PRIMARY EFFLUENT FILTRATION

FINAL REPORT 05 -08
APRIL 2005

NEW YORK STATE
ENERGY RESEARCH AND
DEVELOPMENT AUTHORITY

NYSERDA



The New York State Energy Research and Development Authority (NYSERDA) is a public benefit corporation created in 1975 by the New York State Legislature. NYSERDA's responsibilities include:

- Conducting a multifaceted energy and environmental research and development program to meet New York State's diverse economic needs.
- Administering the **New York Energy \$mart**sm program, a Statewide public benefit R&D, energy efficiency, and environmental protection program.
- Making energy more affordable for residential and low-income households.
- Helping industries, schools, hospitals, municipalities, not-for-profits, and the residential sector, including low-income residents, implement energy-efficiency measures.
- Providing objective, credible, and useful energy analysis and planning to guide decisions made by major energy stakeholders in the private and public sectors.
- Managing the Western New York Nuclear Service Center at West Valley, including: (1) overseeing the State's interests and share of costs at the West Valley Demonstration Project, a federal/State radioactive waste clean-up effort, and (2) managing wastes and maintaining facilities at the shut-down State-Licensed Disposal Area.
- Coordinating the State's activities on energy emergencies and nuclear regulatory matters, and monitoring low-level radioactive waste generation and management in the State.
- Financing energy-related projects, reducing costs for ratepayers.

NYSERDA administers the **New York Energy \$mart**sm program, which is designed to support certain public benefit programs during the transition to a more competitive electricity market. Some 2,700 projects in 40 programs are funded by a charge on the electricity transmitted and distributed by the State's investor-owned utilities. The **New York Energy \$mart**sm program provides energy efficiency services, including those directed at the low-income sector, research and development, and environmental protection activities.

NYSERDA derives its basic research revenues from an assessment on the intrastate sales of New York State's investor-owned electric and gas utilities, and voluntary annual contributions by the New York Power Authority and the Long Island Power Authority. Additional research dollars come from limited corporate funds. Some 400 NYSERDA research projects help the State's businesses and municipalities with their energy and environmental problems. Since 1990, NYSERDA has successfully developed and brought into use more than 170 innovative, energy-efficient, and environmentally beneficial products, processes, and services. These contributions to the State's economic growth and environmental protection are made at a cost of about \$.70 per New York resident per year.

Federally funded, the Energy Efficiency Services program is working with more than 540 businesses, schools, and municipalities to identify existing technologies and equipment to reduce their energy costs.

For more information, contact the Communications unit, NYSERDA, 17 Columbia Circle, Albany, New York 12203-6399; toll-free 1-866-NYSERDA, locally (518) 862-1090, ext. 3250; or on the web at www.nyserda.org

STATE OF NEW YORK George E. Pataki Governor ENERGY RESEARCH AND DEVELOPMENT AUTHORITY Vincent A. DeIorio, Esq., Chairman Peter R. Smith, President

PRIMARY EFFLUENT FILTRATION

FINAL REPORT

Prepared for the

NEW YORK STATE ENERGY RESEARCH AND DEVELOPMENT AUTHORITY

Albany, NY www.nyserda.org

Gregory Lampman, PE Project Manager

and

NIAGAGA COUNTY SEWER DISTRICT NO.1

Niagara Falls, NY

Frank A. Nerone, PE Project Manager

Prepared by

WENDEL DUCHSCHERER ARCHITECTS & ENGINEERS, PC

Amherst, NY www.wd-ae.com

Jeffrey D. Telecky Project Manager

NOTICE

This report was prepared by Wendel Duchscherer Architects & Engineers, PC in the course of performing work contracted for and sponsored by the New York State Energy Research and Development Authority, and the Niagara County Sewer District No. 1, (hereafter the "Sponsors"). The opinions expressed in this report do not necessarily reflect those of the Sponsors or the State of New York, and reference to any specific product, service, process, or method does not constitute an implied or expressed recommendation or endorsement of it. Further, the Sponsors and the State of New York make no warranties or representations, expressed or implied, as to the fitness for particular purpose or merchantability of any product, apparatus, or service, or the usefulness, completeness, or accuracy of any processes, methods, or other information contained, described, disclosed, or referred to in this report. The Sponsors, the State of New York, and the contractor make no representation that the use of any product, apparatus, process, method, or other information will not infringe on privately owned rights and will assume no liability for any loss, injury, or damage resulting from, or occurring in connection with, the use of information contained, described, disclosed, or referred to in this report.

ABSTRACT

A demonstration project was performed at the Niagara County Sewer District No.1, evaluating the use of coarse, mono-media filtration for the treatment of primary and CSO/SSO type wastewater. A secondary objective of the project was to quantify the benefits of mono-media filtration compared to mixed-media filtration with regard to wet weather hydraulic capacity, solids removal efficiency, energy use and operational costs. An evaluation of coarse mono-media filtration versus standard mixed-media filtration was performed and a mono-media filtration system was installed. In a second phase of the project, additional piping was installed to allow the District to directly filter primary treated and CSO/SSO type wastewater. The demonstration project revealed several significant benefits of coarse, mono-media filtration, including the following:

- The hydraulic capabilities of the filters were increased with the capability to treat a peak hydraulic loading of 10 gpm/sf with mono-media filtration compared to 3.8 gpm/sf with mixed-media filtration.
- The mono-media filtration system was shown to save approximately 184,662 kWh per year based on an average flow of 6.8 MGD.
- The mono-media filtration system has reduced effluent TSS and BOD discharge levels by 55% and 21% respectively.
- The mono-media filtration system was shown to enhance the performance of the existing liquid chlorine disinfection system. The 7 and 30-day effluent fecal coliform levels have been reduced by 55% and 26%, respectively.
- The mono-media filtration system was also shown to increase wet weather treatment capacity while
 minimizing capital costs compared to the elimination of wet weather flow by rehab and repair
 measures in the collection system.
- Mono-media filtration was shown to be a viable treatment option for primary treated wastewater with a 75% TSS removal rate at a filtration rate of 4.13 gpm/sf.
- Mono-media filtration was shown to be a viable treatment option for SSO/CSO with a 77% TSS removal rate of 4.89 gpm/sf.

Keywords: Mono-media, deep bed filtration, sand filters, filter backwash, tertiary filtration, wet weather treatment

TABLE OF CONTENTS

SEC.	TION	PAGE
SUM	IMARY	S-1
1	INTRODUCTION	1-1
2	MIXED-MEDIA VERSUS MONO-MEDIA FILTRATION	2-1
3	PROJECT CONSTRUCTION	3-1
4	ANALYSIS OF PROJECT RESULTS Filter Comparison CSO / SSO Results	4-1
5	ENERGY, ECONOMIC AND ENVIRONMENTAL BENEFITS Energy Savings Chlorine Reduction Environmental Benefits	5-1 5-2
6	PROJECTED RESULTS VERSUS ACTUAL RESULTS	6-1
7	DEMONSTRATION PROJECT SUMMARY AND CONCLUSIONS	7-1
Appe	endix A Cost Analysis of Wet Weather Treatment vs Removal	A-1
Appe	endix B Total Suspended Solids Summary	A-2
Appe	endix C Fecal Coliform Summary	A-3
Appe	endix D Treatment Plant Summary Reports	A-4
Anne	endix F. Phosphorus Summary	A-5

FIGURES

<u>Figur</u>	<u>PAGE</u>	4
1	Niagara County Sewer District No. 1 – Treatment Plant	
2	Previous Filter-Media	
3	Clay Underdrain Tile	
4	Comparison of Mono-Media versus Anthracite	
5	Comparison of Effluent Total Suspended Solids	
6	Effluent Total Suspended Solids During Wet Weather Events	

TABLES

<u>Table</u>	2	PAGE
1	Comparison of Filter-Media	2-4
2	Filter Hydraulic Loading Rates and Run Times	4-1
3	Filter Effluent Comparison	4-2
4	Niagara County Sewer District No. 1 - Demonstration Project Results	4-4
5	Filter Backwash Energy Comparison	5-2
6	Total Suspended Solids Removal Cost Comparison	5-3
7	Inflow/Infiltration Management Options	5-5
8	Cost Per Pound of TSS Removed	5-5
9	Projected versus Actual Results	6-1
10	Summary of Results	7-1

SUMMARY

The Niagara County Sewer District No. 1 (NCSD No.1) operates an activated sludge treatment plant (with tertiary filtration facilities) that was designed for an average daily flow rate of 14 MGD. In 1998, the Niagara County Sewer District No. 1 decided to initiate an upgrade of its existing gravity sand filters. The District proceeded to replace its existing mixed-media sand filters with deep bed, mono-media sand filters. Under this demonstration project, co-founded by the New York State Energy Research and Development Authority (NYSERDA), the District proceeded to install bypass piping to allow for the filtration of primary and combined sewer overflow/sanitary sewer overflow (CSO/SSO) type wastewater during wet weather storm events.

Operational data collected since the startup of the new filter system has highlighted that the mono-media system provided longer filter run times, improved effort quality, reduced energy consumption, reduced backwash flow rates, and reduced bleach use for disinfection. It was therefore desired to quantify the performance of mono-media filtration versus mixed-media filtration during the demonstration project for the following items:

- Hydraulic capacities during wet weather events
- Energy use related to the filtration and backwash process
- Effluent quality and receiving body impact
- Performance of existing disinfection systems.

The following objectives were also evaluated for mono-media filtration:

- Show the opportunity to increase wet weather capacity while minimizing capital investment
- Show treatability of primary wastewater utilizing mono-media filtration
- Show treatability of CSO/SSO type wastewater utilizing mono-media filtration.

The demonstration project was a success, quantifying the increased hydraulic capacity and treatment performance of mono-media filtration as well as highlighting the potential for mono-media filtration to provide advanced treatment of CSO and SSO type wastewater. Table S-1, presented on the following page provides a summary of the results obtained during the demonstration project.

Table S-1 Summary of Results

Item	Mixed-Media	Mono-Media
Peak Hydraulic Loading	3.8 gpm/sf	10 gpm/sf
Backwash Energy Savings of Mono- Media vs Mixed-Media	_	142,548 kW-hrs per year
Energy Savings of Dry/Wet Weather Control System		42,114 kW-hrs per year
Effluent TSS	6.24 mg/L	2.81 mg/L
Chlorine for Disinfection	52,200 gal per year	43,475 gal per year
Effluent Fecal Coliform (7 Day Avg)	143 CFU / 100 ml	63 CFU / 100 ml
TSS Removal (Primary Wastewater)	-	75 Percent
TSS Removal (CSO/SSO Wastewater)	-	77 Percent
Total Operational & Energy Savings (Compared to Mixed-Media System)	-	\$27,420 per year
Cost per lb TSS Removed	\$0.358	\$0.175

As highlighted in Table S-1, the mono-media filtration system outperformed traditional mixed-media filters related both to treatment performance and to operational costs. Mono-media filtration was also shown to remove 75 to 77% of total suspended solids (TSS) for primary treated or "CSO/SSO type wastewater" highlighting its promise as an advanced treatment technology.

The total operational cost savings of approximately \$27,420 per year, results in a payback of approximately 13 years for the added cost of the mono-media conversion compared to replacement with mixed-media. The mono-media filtration system removed substantially more suspended solids than the previous mixed-media filtration system resulting in significantly lower cost per lb of TSS removed. The mono-media filtration system has been in operation for 6 years and removed approximately 96,310 lbs of TSS per year. Basing savings on both filter systems removing 96,310 lbs of TSS over one year, the mono-media filtration system would save approximately \$43,460 resulting in a payback of 7.5 years.

The following conclusions are made based on the results of this demonstration project:

- Mono-media filtration is an excellent option for wastewater treatment plants that have capacity
 problems related to wet weather flows. The operational and energy savings when compared to
 traditional mixed-media filtration can help offset the capital cost of the upgrade.
- Mono-media filtration is a cost effective and energy-efficient process for treating CSO and SSO type wastewater.
- Mono-media filtration removes TSS at a substantially cheaper cost per lb. than mixed-media filtration
 and therefore should be considered for all new wastewater treatment plants as well as rehabilitating
 existing treatment plants.
- Mono-media filtration is an effective tool to help increase the efficiency of existing liquid bleach disinfection systems.

INTRODUCTION

All wastewater treatment plants are challenged to meet capacity requirements related to infiltration and inflow events which cause degradation of effluent discharges to receiving streams, and limits plant capacities. Most sanitary sewer systems tributary to these areas have overflow points in the collection system that bypass sewage to adjacent water streams resulting in negative impacts on the environment. The United States Environmental Protection Agency (USEPA) has pending Sanitary Sewer Overflow (SSO) regulations to address these overflows on a national basis.

The Niagara County Sewer District No. 1 (NCSD No.1) operates an activated sludge treatment plant (Figure 1) with tertiary filtration facilities that were designed for an average daily flow rate of 14 MGD. The treatment plant was originally constructed in 1978 and is manned by 18 employees. The plant currently treats about 50% of its design flow on an annual average but experiences significant storm related peak flows up to approximately 32 MGD.



FIGURE 1 – Niagara County Sewer District No.1 Treatment Plant

The NCSD No.1 facility completed a tertiary filter upgrade utilizing mono-media sand and deep bed filtering technology that was recognized statewide with a design excellence award from the New York Association of Consulting Engineers, Inc. Operational data collected since the startup of the new filter system indicated that the mono-media system is capable of successfully filtering primary wastewater and wastewater similar to that discharged from sanitary sewer overflows. In addition, filter performance data

has shown longer filter run times, improved effluent quality, reduced bleach use for disinfection, reduced energy consumption due to longer filter run times, and reduced backwash flow rates.

The outstanding performance of the upgraded filter system has led the NCSD No.1 to believe that additional opportunities exist for use of mono-media filters in the treatment of wastewater discharged during sanitary and combined sewer overflows. The NCSD No.1 decided to undertake a demonstration project with the New York State Energy Research and Development Authority to evaluate the use of monomedia filters for treating primary wastewater, sanitary sewer overflow (SSO) and combined sewer overflow (CSO) type wastewater. The objectives of this demonstration project are as follows:

Comparison of Mono-Media versus Mixed-Media Filtration System

- Quantify increased treatment capabilities within existing facilities
- Quantify energy savings related to filtration process
- Quantify improved effluent quality and receiving water body impact
- Quantify improvement of liquid bleach disinfection system performance
- Show opportunity to increase wet weather treatment capacity while minimizing capital investment.

Demonstration of Mono-Media Filtration for Treatment of Primary and SSO/CSO Type Wastewater

- Show treatability of primary wastewater utilizing mono-media filtration
- Show treatability of SSO/CSO type wastewater using mono-media filtration.

Successful completion of this project would prove to be significant to New York State. A June 1992 NYSDEC publication identifies 152 wastewater treatment plants in New York State with tertiary filters. Most were built in the 1970's with USEPA construction grant funds and they are at, or beyond, their projected service life. All are subject to wet weather flow events from infiltration/inflow with the related operational and treatability problems. Pending SSO regulation will result in large future capital outlays to either treat at SSO points, build interceptors to convey SSO flows to the wastewater treatment plants, and/or increase WWTP capacities. This demonstration project provides an opportunity for a full-scale pilot study to address all of these issues, minimize capital investment, save energy, and improve the environment in the process.

MIXED-MEDIA VERSUS MONO-MEDIA FILTRATION

MIXED-MEDIA FILTER SYSTEM

Like most wastewater treatment plants constructed in the 1970s, the NCSD No.1 plant was equipped with mixed-media sand filters. These filters were shown to function adequately during average day loading and flow conditions but failed to provide the level of treatment needed during wet weather, high-flow and high-loading events.

The filtration process at the District treatment plant consisted of three identical mixed-media, gravity sand filters. The three filters are further broken down into two individual cells each for a total of six filter cells. Each filter cell is 31' 9" by 10' 9" for a total filtration area of 2,048 square feet.

The filters boxes were constructed of concrete and housed an underdrain system made of dual lateral, clay tile blocks and three levels of various sized media. This media consisted of:

- a bottom layer of 12-inches of silica gravel for support
- an intermediate layer of 24-inches of silica sand
- a top layer of 12-inches of anthracite coal.

The top layer of anthracite coal was larger than the intermediate layer of silica sand. In theory, the anthracite coal would remove the largest particles in the filter influent while the silica sand would remove the smaller particles that passed through the top layer. In practice, the top layer of anthracite would become blinded during a high-flow event and the filters would need to be taken out of service for cleaning by running a backwash cycle.



FIGURE 2 – Previous Filter Media



FIGURE 3 - Clay Underdrain Tile

The previous filter system was equipped with a water only backwash system with surface wash facilities which used large volumes of water during the backwash cycle and provided limited agitation to the upper media layers during this cleaning process. The large volumes of water resulted in the backwash holding

tanks becoming completely full during a high flow event within an hour. Therefore, the filters had to be taken off-line and bypassed.

ANALYSIS OF ALTERNATIVES

The problem that needed to be addressed was how to equip the NCSD No.1 treatment plant to treat high flow, high-loading conditions in an economical manner. The following three alternatives were evaluated:

- Option 1 Rehabilitate the existing filters in kind with minor modifications to media size and depth while adding air backwash capabilities
- Option 2 Construct additional filter beds to provide more treatment capacity
- Option 3 Modify the existing filters and utilize deep bed, coarse mono-media with simultaneous air and water backwash facilities.

Option 1 - Mixed-Media with Air/Water Backwash

Rehabilitating the existing filters with minor modifications to the media while adding air and water backwash facilities was not selected. This rehabilitation option would have had the following advantages and disadvantages:

Advantages

- Reduced water required for backwash
- Improved cleaning of filter beds

Disadvantages

- Increased potential for loss of media
- No improvement on filter run times
- No improvement of peak loading capacity
- Incorporation of air supply blowers for air backwash cycle.

Option 2 – Additional Mixed-Media Filters with Water Backwash

Construction of additional filters to provide more treatment capacity was not selected. This option had the following advantages and disadvantages:

Advantages

• Improved total flow and treatment capacity due to additional filter surface area

• Elimination of need for air supply blowers (no air and water backwash cycle)

Disadvantages

- Construction of new building required (high capital cost)
- No improvement on filter run times
- Increased total water required for backwash cycles.

Option 3 – Deep Bed Mono-Media with Air/Water Backwash

Modification of the existing filters to deep bed mono-media was selected as the most cost-effective solution to the District's wet weather treatment problems. This option has the following advantages and disadvantages:

Advantages

- Higher peak loading capacity
- Reuse of existing filter footprints
- Reduced water required for backwash
- Elimination of potential for media loss during backwash
- Longer filter run times
- Improved total flow and treatment capacity
- Reduced chlorine for effluent disinfection

Disadvantages

- Incorporation of air supply blowers for air backwash cycle
- Limited experience in New York State.

Option Three was selected as the most cost effective solution. It provided the advantages of higher filtering capacities with longer filter run times while utilizing the same filter footprints. The reduced use of chlorine for disinfection made up for the additional electrical costs of the air supply blowers. The numerous installations of deep bed, coarse mono-media filters in other areas of the Country provided adequate justification for this treatment system despite the limited operating record in New York State.

ADVANTAGES OF MONO-MEDIA SYSTEM

The key to the design of the deep bed, mono-media filtration system was the large diameter media. Table 1 presented below provides a comparison of the characteristics of the mono-media sand versus the anthracite and silica sand in the previous mixed-media system. The large diameter media allows for deeper

penetration of solids into the filter bed providing for utilization of the whole filter volume instead of just the top layers. The deeper bed and the spherocity of media provide more volume for storage of trapped solids, allowing for higher filtration rates and longer run times. Figure 4 highlights the size difference between the large diameter sand and the anthracite from the previous filter system.

Table 1 Comparison of Filter Media

CHARACTERISTIC	MONO-MEDIA	ANTHRACITE	SILICA SAND
Filtration System	New	Previous	Previous
Effective Size	2.5 mm	1.0 mm	0.5mm
Uniformity Coefficient	< 1.35	< 1.8	< 1.8
Specific Gravity	2.65	1.55	2.65
Spherocity	0.9	0.5	0.7
MOH Hardness	6	2.7	6



FIGURE 4 - Comparison of Mono-Media vs Anthracite

The deep bed, mono-media system that was selected for the NCSD No.1 plant included plastic underdrain that interlock eliminating the need for grouting blocks together. The plastic underdrain block also does not contain orifices that plug over time. The filter media consisted of 54 inches of 2.5-mm silica sand and support gravel. The use of only one filter media eliminates the potential of media layers intermixing as was experienced with the previous filter system.

The spherocity of the coarse, mono-media sand allows the filter to be cleaned at lower water and air backwash rates because the round media gyrates and spins against one another causing scraping and scouring action that removes accumulated solids out of the filter bed. The lower water and air backwash rates result in energy savings due to decreased pumping requirements. The coarseness and high density of the mono-media sand makes fluidization of the filter bed impossible at feasible backwash rates. Despite this lack of fluidization during the backwash cycle, the spherocity of the media and the scouring action achieved during the simultaneous air-water backwash provide thorough cleaning without fluidization of the

filter bed. This scouring and scraping action during backwash does lead to higher levels of erosion and decay of soft filter media. This made the selection of a hard, durable filter media an important design characteristic.

There are several advantages to not fluidizing the filter bed during the backwash cycle. First, no media is washed out of the filters during a backwash as was experienced with mixed-media filtration system.

Second, without fluidization of the filter bed, no intermixing of the media and gravel layers take place. The lack of fluidization also allows a deeper layer of media to be utilized because the freeboard between the top of the media and the wash water troughs can be minimized.

The layer of anthracite in the mixed-media filters eroded away over a period of time. The fine particles were either washed away or made their way into the underdrain laterals. Over the course of several years, the fine anthracite particles started to plug the laterals in portions of the underdrain. These plugged areas would cause localized areas of high velocity currents during a backwash leading to increased intermixing and upset of filter media layers. These problems led to the selection of silica sand, with a MOH hardness of six, which has virtually eliminated the erosion of the media.

Another shortcoming of the previous filtration system that was addressed during the course of the design was that it was no longer required to only backwash one filter cell at a time. With the previous system, the backwash facilities were only sized to backwash one filter cell at a time causing one filter, made up of two cells, to be out of service for a longer time period than would otherwise be necessary. This situation provided additional stress on the two on-line filters during a backwash. The goal to backwash two filter cells at one time was an additional reason that a simultaneous air-water backwash system was desirable. The simultaneous air-water backwash system cleans the filter media with water rates in the neighborhood of 6 gpm/sf instead of 20 gpm/sf as was required with the previous filter system.

Due to the aforementioned limitations of the previous backwash system and the concerns about the underdrain age, a complete retrofit, including replacement of the underdrain and incorporation of an airwater backwash system was selected. HDPE underdrain block replaced the clay tile underdrain. This HDPE jacketed underdrain is specifically designed for wastewater, unlike the previous clay tile underdrain that is utilized in both water and wastewater applications. The underdrain selected is shaped to ensure uniform distribution of air during a backwash and does not contain any orifices to plug with solids or biological growth. The underdrain also interlocks together, eliminating the need for grouting between the individual blocks and associated future maintenance issues.

The existing relay/drum timer filter control system was also upgraded as part of the project to a PC/PLC driven automated control system. The new automated control system provides increased flexibility while

requiring less operator attention. The filter control system allows each filter to be controlled by level or flow of water through the filters by modulating the effluent valves. The control system also automatically limits the number of filter feed pumps that are running during a backwash to keep from overwhelming the remaining online filters.

Backwashing is initiated either automatically, through headloss, time of day, and effluent valve position, or manually by operator initiation. The most energy efficient backwashing event happens automatically and is initiated by effluent valve position. This scenario maximizes the filtering capability of the equipment. The control system and piping layout allow either one or two filter cells to be backwashed simultaneously. Backwashing of one filter cell instead of two is not the standard operating procedure, but is beneficial if it is desired to increase the water backwash rate on filters that are extremely dirty. Backwashing only one filter cell at a time also allows the filters to be backwashed if one air supply blower is out of service. Two blowers are needed if both cells are backwashed simultaneously.

DRY WEATHER / WET WEATHER CONTROL SCHEME

In order to reduce energy usage from pumping during low-flow conditions, a two-mode operational control scheme was developed. The filter control system was designed to operate in either dry weather or wet weather mode. In the dry weather mode, the operating levels of the filters are reduced and the filter feed wet well is run at a higher level. These two factors decrease the amount of static lift that the filter feed pumps provide, thereby reducing pumping energy costs. In wet weather mode, one of the keys to the operation of the filtration system is that all water receives tertiary treatment. In order to ensure that all water receives tertiary treatment, the filters are operated at a higher level while the filter-feed wet-well level is dropped to a lower elevation reducing the threat that bypassing of the filters will occur. The filter-feed wet-well is operated at a lower water level because it overflows to the filter effluent channel at high levels.

PIPING UPGRADES

A second phase of construction was undertaken, as part of this NYSERDA Demonstration Project, that allowed the District to isolate primary treated effluent, which is similar to CSO/SSO type wastewater, directly to the filters while bypassing the filters with the biologically treated effluent. The two treatment trains were then blended and all received disinfection with liquid chlorine before discharge to the Niagara River.

The piping upgrades required to allow the District to isolate the primary treated effluent included construction of approximately 360 linear feet of 36 -inch cement lined ductile iron pipe, two 36" by 36" slide gates, and modifications to the existing high flow channels and filter-feed wet-wells.

PROJECT CONSTRUCTION

PHASE 1 – FILTER UPGRADE

The first construction phase of the project started in June of 1998. Wendel Duchscherer performed the design and prepared contract documents including plans and specifications to convert the existing mixed-media filters to deep bed, coarse mono media filters at the Niagara County Sewer District No.1 treatment plant. The project consisted of General Construction and Electrical Construction contracts. The contracts consisted of the following:

1. General Construction Contract

- Demolition of the existing filter underdrain system and the existing surface wash system
- Extension of six existing filter gullet walls and raise twenty-four existing filter weir troughs
- Sandblast and paint filter internals for six filter cells
- Furnish and install 18" of silica sand support gravel for six filter cells
- Furnish and install 54" of silica sand for six filter cells
- Furnish and install air/water underdrain block for six filter cells
- Construct concrete structural sump in six filter cells
- Furnish and install one filter air backwash system
- Furnish and install two 60 horsepower air supply blowers
- Furnish and install stainless steel air supply piping connecting the blowers to the air backwash distribution system
- Furnish and install six air valves and electric actuators
- Furnish and install one PLC based filter control system, three differential pressure transmitters and two ultrasonic level transmitters.

2. Electrical Construction Contract

- Demolition of three local control panels and one main control panel
- Provide three new local control panels and one main control panel
- Provide wiring to all electrical devices.

The contract for the General Construction work was awarded to Kohl Construction, Inc. of Alden, New York for \$565,000. The coarse mono-media filtration system was supplied by Severn Trent (Tetra Technologies) as a sub-contractor to Kohl Construction, Inc. The contract for Electrical Construction was awarded to O'Connell Electric, Inc. of Lancaster, New York for \$30,900.

Construction of the project commenced in May of 1999 and was completed in October of 1999.

Phase 2

The second phase of the project started in June of 2002 with Wendel Duchscherer providing design services including preparation of contract documents, which consisted of drawings and specifications. The project consisted of a General Construction Contract including the following components:

- Provide and install 360 linear feet of 36" cement lined ductile iron gravity sewer piping and five manholes
- Provide and install two new slide gates with electric actuators
- Perform core drilling in the existing concrete walls to allow for connection of piping into the existing filter feed wet well and the high flow routing chamber.

The contract for the General Construction work was awarded to Yarussi Construction, Inc of Niagara Falls, NY for approximately \$140,000. Construction of the project commenced in May of 2003 and was completed in July of 2004.

ANALYSIS OF PROJECT RESULTS

The results of the demonstration project and the evaluation of coarse mono-media filtration for treatment of primary treated effluent and SSO/CSO type wastewater at the Niagara County Sewer District No. 1 Water Pollution Control Facility are presented in this section. This includes a comparison of the effectiveness of the mixed-media filters versus the mono-media filters for the following parameters:

Comparison of Mono-Media versus Mixed-Media Filtration System

- Quantify increased treatment capabilities within existing facilities
- Quantify energy savings related to filtration process
- Quantify improved effluent quality and receiving water body impact
- Quantify improvement of liquid bleach disinfection system performance
- Show opportunity to increase wet weather treatment capacity while minimizing capital investment.

Demonstration of Mono-Media Filtration for Treatment of Primary and SSO/CSO Type Wastewater

- Show treatability of primary wastewater utilizing mono-media filtration
- Show treatability of SSO/CSO type wastewater using mono-media filtration.

FILTER COMPARISON

The performance of the mono-media filtration system has been superior to the mixed-media filtration system. The District has experienced increased filtering capacity without sacrificing filter performance. The tertiary filters now treat approximately 2.5 times more water between backwashes while being able to handle a peak hydraulic loading rate that is 2.6 times higher than the previous filter system. As a result of this project, the plant now performs half as many backwashes while filtering more water. Filter bypassing has been virtually eliminated. Table 2 below provides filtering rates and run times for dry weather, wet weather and peak flow, hydraulic loading conditions.

Table 2 Filter Hydraulic Loading Rates and Run Times

	Mixed-Media Filters		Mono-Media Filters	
Flow Scenario	Flow Rate	Run Time	Flow Rate	Run Time
	(gpm/sq. ft.)	(hours)	(gpm/sq. ft.)	(hours)
Dry Weather	1.7	20	2.3	38
Wet Weather	2.8	10	5.3	24
Peak Flow	3.8	2	10	8

The District has also experienced the added benefit of increased levels of treatment since startup of the new filter system. Table 3 highlights the enhanced treatment performance of the mono-media filter system. Effluent total suspended solids concentrations have been reduced by 44%, effluent phosphorus concentrations have reduced by 40% and fecal coliform levels in the effluent have been reduced 55% and 26% respectively for 7 day and 30 day averages. The turbidity of the effluent discharged from the treatment plant was enhanced with the upgrade to the mono-media filtration system. The effluent turbidity after the filter improvements was typically 2 Nephelometric Turbidity Units (NTUs) with minimum values of 0.3 NTUs.

In addition to the enhanced performance of the filtration process, the efficiency of the plant's existing disinfection system has increased. The District uses liquid bleach for disinfection, which loses effectiveness when high solids levels are present because the bleach is soaked up by the solids. With lower levels of solids, a larger percentage of the individual bacteria and bacteria in small clumps are destroyed. The reduced suspended solids levels in the filter effluent have resulted in the District utilizing less bleach for disinfection per million gallon of water treated.

Table 3 Filter Effluent Comparison

Effluent Characteristics	Mono-Media	Mixed-Media
Total Suspended Solids	3.49 mg/L	6.24 mg/L
Total Phosphorous	0.21 mg/L	0.35 mg/L
Fecal Coliform (7 day avg)	63 CFU/100 ml	143 CFU/100 ml
Liquid Bleach Used	3623 gallons/month	4350 gallons/month

The average influent total suspended solids (TSS) loading to the mono-media filters has been 18.2 mg/L with a maximum loading of 44.8 mg/L. With an average filter effluent total suspended solids concentration of 3.49 mg/L the mono-media filters are removing approximately 80% of solids entering the filters. The District is removing greater than 95% of the plant influent total suspended solids. Figure 5 graphically highlights the improved total suspended solids removal performance of the deep bed, mono-media filtration system.

2003-04 mono media 9.58 4.02 2001-02 mono 96.9 3.64 1999-00 Plant Flow & Effluent Total Suspended Solids mono media 6.61 2.81 1997-98 mixed 5.57 4.76 1995-96 mixed 7.31 7.36 mixed 1994 9.52 6.61 (J\gm) sbilo& babnaqsu& lstoT Plant Flow TSS

Plant Flow (MGD)

FIGURE 5 Comparison of Effluent Total Suspended Solids

As one of the primary goals of the project was to enhance the performance of the tertiary filters during high flow events, it was necessary to compare the performance of the deep bed, mono-media filtration system against the previous mixed-media filtration system for flows greater than 10 MGD. The comparison data set included 146 days with flow greater than 10 MGD for the mono-media filtration system and 101 days with flows greater than 10 MGD for the mixed-media filtration system. The effluent quality produced by the mono-media filtration system was substantially better than the effluent produced by the mixed-media system during high flow wet weather conditions. The average flow and effluent TSS concentration for the mono-media filtration system was 13.27 MGD and 5.87 mg/L, respectively, while the maximum total suspended solids concentration was 16 mg/l. The average flow and effluent TSS concentration for the mixed-media filtration system was 13.84 MGD and 16.45 mg/L, respectively, while the maximum total suspended solids concentration was 65 mg/L. Figure 6 entitled "Wet Weather Effluent Total Suspended Solids", presented on the following page, plots effluent total suspended solids concentrations versus flow for the mono-media and mixed-media filtration systems during wet weather flow conditions.

26

Figure 6 Effluent TSS During Wet Weather Events

CSO/SSO RESULTS

As part of the demonstration project the District installed high flow piping and an inline filter influent sampler that allowed primary and SSO/CSO type wastewater to be sent to the filters directly and the filter influent to be sampled for TSS levels. These improvements allowed the District to evaluate the monomedia filters for their ability to treat primary wastewater and SSO/CSO type wastewater. The influent to the District treatment plant during a wet weather event is similar to an SSO/CSO type wastewater. The 2004 EPA Report to Congress presents sampling data which reports the median municipal Wet Weather SSO TSS concentration at 91 mg/L and the median municipal CSO TSS concentration at 127 mg/L. The wastewater strength is diluted by storm water that makes it way into the sewer system through inflow and infiltration.

During the performance of this demonstration project, a high flow event was considered to be a sampled day when the average daily flow for the NCSD No. 1 WPCC was above 10.0 MGD. There were 78 high flow events evaluated during the six-month demonstration project from January through June of 2004. For the purpose of this demonstration project, filter influent for days when flow was above 10.0 MGD and the filter influent TSS concentration was above 30 mg/L most closely resembled CSO/SSO TSS values and was considered to be "CSO/SSO type wastewater." Filter influent for days when flow was above 10 MGD and the influent TSS concentration was below 30 mg/L was considered to be primary type wastewater.

Table 4 NCSD No.1 Demonstration Project Results

Wastewater Type	Influent TSS (mg/L)	Effluent TSS (mg / L)	Percent TSS Removal
"CSO/SSO"	41.8	9.4	77 %
Primary	20.0	4.9	75 %
Dry Weather	17.6	3.3	81%

As shown in Table 4, the mono-media filters are effective filtering both primary and CSO/SSO type wastewater. The influent to the NCSD No.1 WPCC during wet weather events is similar to SSO type wastewater. Based on TSS removal levels experienced by the District, an effluent TSS concentration of 20.9 mg/L is projected when utilizing mono-media filtration on SSO type wastewater with a TSS concentration of 91.0 mg/L. These results show that deep bed mono-media filters are an effective technique for the treatment of SSO and CSO type wastewater whether used in combination with primary treatment or as a standalone process.

Additional sampling on the removal of Phosphorus was performed during the demonstration project. Samples were collected on eight days with plant influent Phosphorus averaging 9.17 mg/L, filter influent Phosphorus averaging 0.43 mg/L and effluent Phosphorus averaging 0.26 mg/L. The data collected is presented in the appendices of this report.

ENERGY, ECONOMIC AND ENVIRONMENTAL BENEFITS

The demonstration project highlighted that the NCSD No. 1 has experienced significant energy and economics savings and environmental benefits through the installation of deep-bed, mono-media filters. The energy savings experienced have been from the reduction of filter backwashes, which has resulted in a reduction of backwash water pumping, a decrease in the operation of wash water pumps, and a reduction of the volume of wash water recycled to the headwork of the treatment plant. Additional energy savings have also been seen due to the use of the dry weather/wet weather operating scheme that reduces pumping heads.

ENERGY SAVINGS

The mono-media filtration system has been shown to reduce the amount of energy used for cleaning of the filters during backwash. The reduced energy savings are due to the following changes in the operation of the backwash operation:

- Decrease in the duration of a backwash cycle reducing water use
- Decrease in the frequency of filter backwash
- Decrease in the rate of water per square foot for a filter backwash
- Decrease in the volume of water recycled to the front end of the plant
- Decrease in energy use due to the dry weather / wet weather control system
- Energy reduction during high flow events due to the use of the dual treatment trains.

Table 5 below compares the energy usage related to filter backwash on an annual basis of the previous mixed-media filtration system versus a deep-bed, mono-media filtration system. The additional solids storage capacity of the deep-bed, mono-media filters has resulted in a 75% reduction in the number of backwashes performed per year. This reduction in the number of backwash events, along with the 70% reduction in the volume of water used per filter backwash, has resulted in a decreased energy usage of approximately 142,548 kW-hrs per year. This energy savings is due to the reduction in pumping of backwash water and recycling of wash water to the front of the treatment plant. Due to typical operation during high flow events, no demand reduction is expected.

Table 5 Filter Backwash Energy Usage

Filter System	Backwashes Per Year	Backwash Step	kWhrs per Backwash	Annual Energy Use (kWhrs per year)
Mixed-Media	2190	Water Backwash*	66.7	146,073
		Water Pumping	36.3	79,497
Deep-Bed Mono-Media	548	Water Backwash*	10.7	58,636
		Air Scour Cleaning	23.5	12,878
		Water Pumping	21.0	11,508
Total Yearly Savings				142,548

^{*} These water backwash values are based on the NCSD No.1 filling their elevated storage tank by pumping.

The use of a dry weather/wet weather operating control mode has allowed the District to achieve further energy savings. By operating with lower operating levels in the filters and higher operating water levels in the filter feed wet well, the District reduces the head that the filter feed pumps must overcome by approximately 10 feet. Over the course of one year, assuming that the district is in dry weather mode approximately 50% of the time, 42,114 kW-hrs are saved.

Table 6 Total Annual Energy Savings

Item	Cost Savings
Filter Backwash Energy Savings	\$14,250
Dry Weather/Wet Weather Operating Scheme	\$4,420
Total Savings	\$18,670

CHLORINE REDUCTION FOR DISINFECTION

The Sewer District utilizes liquid bleach for disinfection, which loses effectiveness when elevated suspended solids levels are present because the liquid bleach is soaked up by the clumps of solids and does not reach the bacteria organisms. With lower solids levels, a larger percentage of the individual bacteria and bacteria in small clumps are destroyed. The decreased levels of suspended solids in the filter effluent has resulted in the Sewer District utilizing less bleach for disinfection per million gallon of water treated.

The District has experienced a 17% reduction in the use of liquid bleach due to the enhanced removal of effluent suspended solids, which results in an annual savings of approximately \$8,750.

ENVIRONMENTAL BENEFITS

Numerous environmental benefits were demonstrated during the project. They included improving the effluent quality to the Niagara River through reduced effluent TSS, effluent Phosphorous and effluent Fecal Coliform. The reduction of the above mentioned parameters is as follows:

- Effluent Total Suspended Solids concentrations were reduced by 55% which results in the elimination of the discharge of approximately 45 tons of solids to the Niagara River over the course of one year.
- Effluent Phosphorous concentrations were reduced by 40% which results in the elimination of the discharge of 2,690 pounds of phosphorous to the Niagara River over the course of one year.
- Effluent Fecal Coliform concentrations were reduced by 55% which results in a substantial reduction in the Colony Forming Units of Fecal Coliform discharged to the Niagara River. This reduction helps to make the river safer for fishing, boating, water skiing and other forms of water surface recreation.
- Chlorine utilized for disinfection was reduced 17%, which will help reduce the formation of chlorine disinfection by-products in the wastewater effluent. The reduction of chlorine disinfection by-products will help the impact to Niagara River aquatic population.

ECONOMIC BENEFITS

Several parameters were selected at the onset of the project for verification of the cost effectiveness of deep-bed, coarse mono-media filtration. These parameters included the following:

- Treatment performance required filter square footage versus loading rate. As shown in Table 2, the mono-media filters can treat a peak hydraulic loading of 10 gpm/sf while the mixed-media filters were shown to only treat a peak hydraulic loading of 3.8 gpm/sf. Based on this flow to area relationship, approximately 2.5 square feet of mixed-media filter area is needed for every 1 square foot of mono-media filter area.
- Disinfection system efficiency comparison of chlorine usage and cost. The mono-media filters were shown to utilize 17% less chlorine for disinfection resulting in annual savings of \$8,750.
- Treatment cost versus inflow and infiltration elimination in collection system. The concerns that have been expressed by the Environmental Protection Agency and other regulatory agencies in the proposed SSO regulations leads one to ponder the cost effectiveness of sewer system repair work to eliminate inflow and infiltration versus the cost of treatment. As part of the demonstration project, the cost of treatment versus removal was evaluated based on the specific conditions experienced by the NCSD No. 1.

In order to provide a thorough and realistic economic evaluation comparing the costs of treating Inflow/Infiltration (I/I) versus locating and eliminating I/I, the Hamlet of Bergholtz, a small sub-area of the NCSD No.1 collection system, was selected for evaluation. Bergholtz was selected because it is a known problem area, with previously measured I/I rates, and a small enough system in size to allow for a reasonable projection of rehabilitation costs.

An evaluation of the NCSD's cost of treatment for a peak day flow was performed. The additional incremental cost of treating a peak flow of 26 MGD was calculated. The following items were used as the basis of the District's increased treatment costs on a peak flow day:

- Increased pumping costs at the remote stations
- Increased pumping costs at the WPCC influent station
- Increased aeration (air supply blower) costs of the activated sludge system
- Increased filter feed pumping costs
- Increased backwash air scour blower costs
- · Increased backwash holding tank pumping
- Increased disinfection costs.

The analysis showed that the peak flow event resulted in an additional cost of approximately \$2000 per day for a flow of 26 MGD versus an average-flow of approximately 6.6 MGD. (See Appendix A for peak flow versus average day treatment costs). In order to compare the cost of treating the additional flow versus eliminating it in the distribution system, two I/I control measures were evaluated based on the financial impact to the district. The scenarios were evaluated as follows:

- Utilize the WPCC's existing capacity to treat all incoming flows
- Perform infrastructure and rehabilitation work in the collection system to attempt to eliminate I/I.

An analysis was performed on the Hamlet of Bergholtz sub-area because flow rates and repair costs were readily available. The following assumptions were made:

- The calculation to determine the total I/I for Bergholtz for one year was based on the peak I/I of 7500 gpd/in.mi., or 0.345 MGD, being experienced 365 days a year to determine the treatment cost of the additional flow
- A \$650,000 capital cost was identified for repair costs (See capital cost estimate in appendices)
- The reduction of flow by I/I capital work was based on a 50% effectiveness, meaning a removal of 0.173 MGD and treatment of the remaining 0.173 MGD

The results are of the evaluation are summarized below in Table 7.

Table 7 Inflow/Infiltration Management Options

	Flow		Capital	Total Annual
Scenario	Treated	Treatment Cost	Improvement Costs	Cost
	(MGD)			
Utilize Existing Plant				
Capacity	0.345	\$12,595 per year	\$0 per year	\$12,595
Perform				
Infrastructure Work	0.173	\$6,300 per year	\$65,000 per year*	\$71,300

^{*}The capital improvements costs were based on the District bonding the \$650,000 project over 20 years with a 6% annual interest rate with \$65,000 being the first year repayment amount.

Through utilization of the treatment plant's existing capacity, greatly increased by recent capital projects at the plant, the District can treat all additional wet weather flow at a cost of approximately \$100/MGD. The \$100/MGD was calculated based on the difference in treatment costs for an average day versus a peak day loading condition and is based on the assumption that the fixed costs of the District remain constant while the cost to dewater sludge also remains constant. Utilizing the Bergholtz area as an example, the District can treat all additional flow for \$12,595 per year instead of the \$71,300 per year cost to attempt to eliminate the I/I. Additional information on the calculations utilized during the evaluation can be found in Appendix B.

TSS REMOVAL COSTS

The mono-media filtration system was also shown to remove TSS at half the cost per pound than the mixed-media filtration system. A summary of the removal cost is presented in Table 8 below.

Table 8 Cost Per Pound of TSS Removed

Filter System	Backwash Energy	Disinfection Costs	Daily Cost / lb
	Costs per Year	Per Year	TSS Removed
Mixed-Media	\$22,550	\$52,220	\$0.358
Deep-Bed Mono-Media	\$8,300	\$43,470	\$0.173
Total Savings	\$14,250	\$8,750	\$0.183

PROJECTED RESULTS VERSUS ACTUAL RESULTS

In the proposal submitted for this project, several performance goals were provided based on projected performance of the mono-media filtration system. Table 9 below provides a summary of the projected results versus the actual results obtained from the demonstration project.

Table 9 Projected versus Actual Results

Item	Projected Result	Actual Result
Reduced Water per Backwash	40%	70%
Backwashes per Year	1095	548
Reduction in Disinfection Bleach	20%	17%
Number of High Flow Events (Flow Greater than 10 MGD)	10	78

As highlighted in Table 9, the mono-media filtration system reduced both the number of backwashes per year and the water per backwash significantly more than the projected values. The reduction of bleach utilized for disinfection was slightly less than projected. The amount of bleach added to the effluent has both a manual and an automatic adjustment component. The component of the bleach setpoint that is manually adjusted can effect the amount of bleach added and appears to be the reason the bleach reduction was slightly less than projected.

Other project goals were stated in the proposal but did not include a projected performance level. A summary of the results of these project goals were as follows:

- The hydraulic capabilities of the existing filters were increased with the capability to treat peak hydraulic loadings of 10 gpm/sf versus 3.8 gpm/sf with the previous mixed-media filtration system.
- The mono-media filtration system was shown to save approximately 184,662 kW-hrs per year compared to the mixed-media filtration system.
- Effluent TSS and BOD from the plant were reduced 44% and 21% respectively.
- The mono-media filtration system was shown to enhance the performance of the existing disinfection system. The 7 and 30-day effluent fecal coliform levels were reduced 55% and 26% respectively.
- The mono-media filtration system was also shown to increase wet weather treatment capacity while
 minimizing capital costs instead of the elimination of wet weather flow by rehab and repair measures
 in the collection system.

- Mono-media filtration was shown to be a viable treatment option for primary treated wastewater with a 75% TSS removal rate.
- Mono-media filtration was shown to be a viable treatment option for SSO/CSO with a 77% TSS removal rate.

DEMONSTRATION PROJECT SUMMARY AND CONCLUSIONS

The demonstration project was a success, quantifying the increased hydraulic capacity and treatment performance of mono-media filtration, as well as highlighting the potential for mono-media filtration to provide advanced treatment of CSO and SSO type wastewater. Table 10 provides a summary of results obtained during the demonstration project.

Table 10 Summary of Results

Item	Mixed-media	Mono-media
Peak Hydraulic Loading	3.8 gpm/sf	10 gpm/sf
Energy Savings	-	142,548 kW-hrs per year
Effluent TSS	6.24 mg/L	2.81 mg/L
Chlorine for Disinfection	52,200 gal per year	43,475 gal per year
Effluent Fecal Coliform (7 Day Avg)	143 CFU / 100 ml	63 CFU / 100 ml
TSS Removal (Primary Wastewater)	-	75 Percent
TSS Removal (CSO/SSO Wastewater)	-	77 Percent
Total Operational & Energy Savings	-	\$23,000 per year
Operating Cost per lb TSS Removed*	\$124.63	\$51.78

^{*} The cost per lb. of TSS removed was based on the energy savings due to reduced backwash requirements and the operation of the dry/wet weather control scheme. Other factors in the treatment process were assumed to remain the same.

As highlighted in Table 10, the mono-media filtration system outperformed traditional mixed-media filters related both to treatment performance and operational costs. Mono-media filtration was also shown to be a promising advanced treatment technology for TSS removal related to both primary treated wastewater and CSO/SSO wastewater.

The following conclusions are made based on the results of this demonstration project:

Mono-media filtration is an excellent option for wastewater treatment plants that have capacity
problems related to wet weather flows. The operational and energy savings when compared to
traditional mixed-media filtration can help offset the capital cost of the upgrade.

- Mono-media filtration is a cost-effective and energy-efficient process for treating CSO and SSO type wastewater.
- Mono-media filtration removes TSS at approximately half the cost per lb than mixed-media filtration
 and therefore should be considered for all new wastewater treatment plants as well as rehabilitating
 existing treatment plants.
- Mono-media filtration is an effective tool to help increase the efficiency of existing liquid bleach disinfection systems.
- A dry weather/wet weather control scheme is an effective tool to optimize energy efficiency of a filter system and should be investigated for all filtration systems.
- The treatment of wet weather inflow and infiltration was shown to be substantially cheaper than the
 elimination of inflow and infiltration by collection system repair work. For the pilot area, the cost of
 treatment of wet weather flow was shown to be \$100 / MGD versus the cost of \$205,000 per MGD for
 the collection system repair work.

Appendix A Cost Evaluation of Wet Weather Treatment vs Removal

Bergholz I/I Reduction Costs

Street	Length of 8" Sewer	Number of Manholes	Service Connects
Stoelting Street	2700	10	35
Washington Street	2600	12	29
Niagara Street (N)	4450	· 21 ·· · · · · · · · · · · · · · · · ·	52
Niagara Street (S)	4550	26	34
Cayuga Street "	2100	11	43
Wurl Street	1000	3	13
Sy Road	1400	6	23
Reynolds Street	450	2	11
Luther Street	2300	7	29
Sylvan Place	400	2	17
Old Falls Blvd	2950	14	- 22
Shultz Street	1900	2	19
Rohr Street	2300	3 .	11
Hunt Street	1500	3	17
Totals	30600	122	355

Smoke Testing and CCTV Co	sts	Lateral Repairs	
Percentage of length to test:	50%	% of service laterals to repair:	75%
Cost per LF for smoke testing:	\$0.20	Cost per lateral to repair:	\$1,000.00
Smoke Testing Cost:	\$3,060.00	Lateral Repair Cost:	\$266,250.00
Percentage of length to TV: Cost per LF for TV:	50% of line smoked \$1.50	Manhole Recoating	
	•	% of manholes to repair:	50%
TV Cost (Includes Cleaning):	\$11,475.00	Estimated manhole depth:	8 feet
	•	Cost per LF to repair:	\$140.00
Slip Lining of 8" Sewer			
	•	Cost for repairs:	\$68,320.00
Percentage of length to repair:	50% of line TV'd		
Cost per LF of repair	\$25.00		
•		Total Repair Costs	
Cost for slip lining (w/o laterals)	\$95,625.00	Smoke Testing	\$3,060.00
•		CCTV	\$11,475.00
		Slip Lining	\$95,625.00
		Lateral Repairs	\$266,250.00
·		Manhole Recoating	\$68,320.00
		Sub Total	\$444,730.00
		Contingency	\$75,270.00
		ELA	\$130,000.00
		Total Repair Costs	\$650,000.00

NCSD No.1 Peak Flow vs Average Day Treatment Costs

Conveyance/Treatment Item		Average	Peak		
		Cost Per Day		Cost Per Day	
Remote Pump Stations					
Shawnee	\$	4.5	6 \$	35:77	
Mapleton	\$	9.23	3 \$	47.56	
Moyer	\$	3.34		15.22	
East Canal	\$	46.94		334.71	
Townline	\$	26.19	1 '	204.38	
Tonawanda	\$	17.13	3 \$	73.21	
	\$	107.39	\$	710.85	
Influent Raw Pumps		٠ .			
Influent Raw Pumps	\$	133.63	\$	445.63	
Aeration System					
Air Supply Blowers	\$	190.00	\$	337.73	
Filtration System					
ilter Feed Pumps	\$	44.56	\$	200.32	
ackwash Air Scour Blowers	\$	5.57	\$	48.72	
ackwash Holding Tank Pumps	\$	2.55	\$	10.44	
ewatering Costs					
entrifuging, Polymer, etc		Negligible		Negligible	
isinfection					
each Use		\$60		\$110	
otal Cost	\$	651.09	\$	2,574.54	

Appendix B Total Suspended Solids Summary (Demonstration Project Sampling Results) JAN

2004

DATE	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS Removal
1	21.700	168,00	23.2	2.00	91
2	12,005	216.00	16.0	3.20	80
3	13.610	180.00	18.8	2.00	89
4	10.966	108.00	15.6	1.60	90
5	11.168	112.00	14.8	5,20	65
6	9.500	140,00	13.6	2,60	81
7	8.237	176,00	13.6	2.20	84
8	8.867	116.00	8.4	1.80	79
9	7.120	340.00	8.0	2,00	75
10	7.818	328,00	8.4	2.20	74
11	8.473	80,00	9.2	2.20	76
12	7.825	88,00	20.0	1.80	91
13	7.173	120,00	18.8	2.20	88
14	7.781	136.00	18.8	2.10	89
15	7.371	60.00	20.4	2.80	86
16	7.082	80.00	12.0	2.20	82
17	6.808	248.00	3.6	1.20	67
18	6,886	324.00	24.0	1.60	93
19	6.134	188.00	16.0	2.00	88
20	7.627	344.00	14.4	2.00	86
21	6.083	208,00	16.0	2.40	· 85
22	6.821	260.00	16,0	1.70	89
23	6.744	232.00	16.8	1.40	92
24	6.668	272.00	12.8	1.70	87
25	6.594	284.00	15.6	1.80	- 88
26	6.572	252.00	16.8	1.70	90
27	6.532	244.00	12.8	1.90	85
28	6.447	212.00	10.4	1.60	85
29	6,882	268.00	17.5	2.20	87
30	6.412	260.00	14.8	2.80	81
31	6.753	176.00	16.4	1.40	91
Totals_	8.28	200.65	14.95	2.11	86

CSO/SSO Type Events	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS, Removal
0	0.0	0.0	0.0	0.0	. 0

	Primary Type Events	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS, Removal
i	5	13.9	156.8	17.7	2.8	84

FEB 2004

DATE	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS Removal
1	6.557	184.00	15.2	2	87
2	6.761	220.00	14.4	2.8	81
3	8,095	212.00	27.3	2.8	90
4	9,550	136.00	14.5	3.8	74
5	9.052	68.00	17.2	6	65
6	9.762	80.00	13.5	4	70
7	11.512	104.00	19.5	4	79
8	10,545	124,00	23.5	6.25	73
9	10.836	104.00	55.5	8.25	85
10	8.920	188.00	18.5	6,8	63
11	10.258	116.00	18.0	6.8	62
12	10.548	120.00	22.0	7.4	66
13	7.867	80.00	21.6	5.2	76
14	9.050	96.00	22,4	4.4	80
15	7.191	76.00	18.0	5.6	69
16	7.932	64.00	16.4	5.6	66
17	7.526	84.00	18.0	4.4	76
18	6.971	44.00	14.8	4	73
19	11.068	88.00	14.4	3.8	74
20	8,355	80.00	15.2	4.4	71
21	13.104	72.00	25.3	7.5	70
22	11.916	36.00	20.0	. 7	65
23	11.635	24.00	20.0	8.4	58
24	11.098	96.00	19.6	7.2	63
25	10.672	112.00	33.3	9.5	71
26	10.114	176.00	23.6	9.4	60
27	10.200	112.00	26.0	9.8	62
28	10.235	104.00	25.6	9.6	63
29	12.128	68.00	25.6	8	69
Totals	9.64	105.79	21.34	6.02	72

CSO/SSO Type Events	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS, Removal
2	10.8	108.0	44.4	8.9	80

	Primary Type Events	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS, Removal
L	13	11.1	95.4	21.8	7.3	67

MARCH

2004

DATE	FLOW	INF,SS	FILT, INF SS		% TSS Removal
1 .	15.462	60.00	31.6	8.80	72
2	26,302	188,00	35.0	12.60	64
3	21.515	116.00	24.0	5.60	77
4	17.711	96,00	30.0	7.00	77
5	20.730	92,00	15.2	7.50	51
6	19.670	72.00	21.0	5.00	76
7	13.890	132.00	15.2	6.40	58
8	13.825	124.00	15.6	6.20	60
9	13.747	40.00	14.4	4.20	71
10	11.390	100.00	14.8	6.00	59
11	11.974	116.00	16.4	6,40	61
12	10.244	88.00	18.4	6.20	66
13	11.552	88.00	18.0	6.80	62
14	8.322	68.00	19.6	5.40	72
15	9.375	96.00	19.2	6,80	65
16	8.968	60,00	27.6	5.75	79
17	9.746	20.00	20.5	5.40	74
18	8.879	108.00	21.0	4.50	79
19	9.385	76.00	14.0	6.20	56
20	12.043	36.00	24.5	3.50	86
21	18,463	96.00	25.5	10.50	59
22	13.055	56.00	20.5	9.25	55
23	10.473	68.00	27.5	9.00	67
24	11.645	52.00	20.4	8.75	57
25	14.204	92.00	21.6	9.25	57
26	15.388	36.00	20.6	7.25	65
27	18.379	72.00	43.0	15.50	64
28	14.456	52.00	19.0	8.80	54
29	12.060	52.00	34.8	7.20	79
30	11.501	80.00	23.0	9.20	60
31	10.120	124.00	27.0	8.40	69
Totals	13.69	82.45	22.55	7.40	67

CSO/SSO Type Events	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS, Removal
5	18.0	93.6	34.9	10.2	71

Primary Type Events	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS, Removal
20	14.0	83.0	20.1	7.2	64

APRIL 2004

DATE	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS Removal
1	11.437	40.00	29.0	4.40	85
2	16.276	32.00	17.0	11.00	35
3	15.853	40.00	20.0	5.60	. 72
4	17.424	36.00	26,0	4.80	82
5	16.231	36.00	16.0	5.20	68
6	13.429	40.00	13.0	4.60	65
7	13.387	88.00	20.0	6.00	70
8	12.192	44.00	11.2	3.20	71
9	11.403	68.00	14.0	3.20	77
10	9.657	20.00	19.2	3.60	81
11	8,568	20.00	14.4	4.00	72
12	9.122	28.00	20.0	3.00	85
13	12.031	40.00	19.5	3.60	82
14	20.212	628.00	41.0	12.40	70
15	13.966	20.00	18.5	5.40	71
16	12.584	16.00	18.5	2.20	88
17	11.485	88.00	16.5	3.00	82
18	13.007	124.00	42.7	2.20	95
19	14.711	280.00	22.0	8.60	61
20	12.275	40.00	21.0	15.40	27
21	11.538	40.00	23.0	2.40	90
22	14.063	40.00	26.0	4.40	83
23	12.063	60.00	21.0	1.80	91
24	10.928	48.00	31.0	4.00	87
25	10.529	44.00	29.0	3.20	89
26	12.847	28.00	25.0	4.60	82
27	10.944	12.00	25.0	5.20	79
28	9.049	64.00	27.5	3.40	88
29	9.655	48.00	26.0	3.20	88
30	8.390	88.00	24.0	3.40	86
Totals	12.50853	73.33333	22.6	4.9	78

CSO/SSO Type Events	FLOW	INF,SS	FILT, INF SS	EFF,SS	% TSS, Removal
3	14.8	266.7	38.2	6.2	84

Primary Type Events	FLOW	INF,SS	FILT, INF SS	EFF.SS	% TSS, Removal
21	13.2	53.9	20.5	5.1	75

MAY 2004

19175 1	2004				
DATE	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS Removal
1	8,753	72.00	17.0	2.60	85
2	10,297	40.00	36.0	2,20	94
3	11.387	448.00	12.0	2.20	82
4	9.918	40.00	14.0	3.00	79
5	9,831	44.00	26.0	2.80	89
6	9.120	32.00	20.0	4.40	78
7	8,658	52.00	12.0	4.00	67
8	8.606	40.00	26.0	3.40	87
9	10.271	76.00	22.0	3.60	84
10	9.980	84.00	26.0	5.00	81
11	9.187	56.00	31.0	4.80	85
12	8,578	112.00	13.0	1.40	89
13 .	8.300	72.00	13.6	4.40	68
14	7.896	24,00	11.6	2.20	81
15	7.994	40.00	15.0	2.00	87
16	7.773	36.00	8.4	2.30	73
17	7.698	31,00	10.4	1.40	87
18	8.144	172.00	3.6	1.00	72
19	7.723	204.00	6.8	1.80	74
20	7.229	416.00	6.8	1.20	82
21	7.258	340.00	9.6	3.40	65
22	7.624	380.00	8.4	1.00	88
23	11.015	484.00	12.0	2.60	78
24	21.327	792.00	42.0	14.40	66
25	15.121	188.00	18.0	8.40	53
26	12.726	116.00	22.0	3.80	83
27	10.684	116.00	26.0	3.80	85
28	10.546	108.00	31.0	2.00	94
29	8.855	164.00	24.0	4.20	83
30	8.123	108.00	11.0	1.90	83
31	10.126	124.00	11.0	2.20	80
Totals	9.70	161.6	17.6	3.3	81

			· · · · · · · · · · · · · · · · · · ·		
CSO/SSO Type Events	FLOW	I INF.SS	FILT INF SS	FFF SS	% TSS, Removal
			11.1-1,	211,00	70 100, Kelliovai
1 3	14.1	313.3	36.3	6.2	83
		0.0.0		0.2	1 00 1

Primary Type Events	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS, Removal
7	11.6	221.7	17.6	3.8	78

JUNE 2004 DATE **FLOW** INF,SS FILT, INF SS EFF,SS % TSS, Removal 1 13.850 248.00 9.2 2.8 70 2 10.783 120,00 6.8 2.0 71 3 9.651 240,00 4.8 1.4 71 4 240.00 8.640 6.8 2,2 68 5 8.075 428.00 6.8 2.0 71 6 7.765 380,00 16.0 2,4 85 7 7.968 280.00 6.0 1.8 70 8 7.666 324.00 4.0 2.2 45 9 7.340 260.00 5.2 1.5 71 10 8.776 256,00 2.0 0.5 75 11 7.284 212,00 3.8 1.4 63 12 7.137 184.00 3.6 0.7 81 13 7.040 184.00 3,6 0.9 75 14 7.177 256.00 5.6 0.5 91 15 7.740 364.00 4.4 1.3 70 16 7.097 308.00 5.8 1.8 69 17 7.526 304.00 5.6 1.6 71 18 7.500 244.00 6.0 0.6 90 19 7.069 228.00 10.8 2.2 80 20 7.038 224.00 4.4 0.2 95 21 7.000 268.00 3.6 0.2 94 22 7.216 340.00 4.4 2.6 41 23 7.076 332.00 4.4 8.0 82 24 7.044 252.00 4.4 8.0 82 25 7.543 252.00 6.0 1.2 80 26 6.968 204.00 10.8 1.2 89 27 6.577 244.00 4.8 1.9 60 28 6.593 248.00 4.0 1.3 68 29 6.514 360.00 5.0 1.7 66 30 6.527 336.00 2.0 2.0 0 Totals 7.7 270.7 5.69 1.46 74

Primary Type Events	FLOW	INF,SS	FILT,INF SS	EFF,SS	% TSS, Removal
2	12.317	184.000	8.0	2.4	70

Appendix C Fecal Coliform Summary (Demonstration Project Sampling Results)

NIAGARA COUNTY SEWER DISTRICT #1 SECONDARY CLARIFIER FECAL COLIFORM SUMMARY 2004

<u> </u>		
DATE	SEC CLAR FECAL	SEC CLAR FECAL
	1st Sample	2nd Sample
04/00/04	10.000	
01/02/04	12,000	10,000
01/09/04	11,000	18,000
01/11/04	9,000	12,000
01/16/04	14,000	10,000
01/23/04	28,000	37,000
02/06/04	35,000	20,000
02/08/04	39,000	45,000
02/13/04	28,000	26,000
02/20/04	46,000	58,000
02/22/04	84,000	95,000
03/05/04	62,000	58,000
03/07/04	42,000	57,000
03/12/04	37,000	35,000
03/20/04	9,000	8,000
03/26/04	7,000	9,000
04/02/04	13,000	9,000
04/04/04	17,000	22,000
04/16/04	8,000	9,000
04/18/04	47,000	44,000
04/29/04	98,000	95,000
05/02/04	28,000	31,000
05/06/04	11,000	9,000
05/14/04	58,000	. 69,000
05/16/04	34,000	39,000
05/23/04	24,000	26,000
06/04/04	25,000	30,000
06/06/04	26,000	31,000
06/11/04	21,000	23,000
06/14/04	68,000	84,000
06/25/04	11,000	15,000
07/02/04	32,000	31,000
07/04/04	29,000	35,000
07/11/04	27,000	40,000
07/16/04	14,000	17,000
07/18/04	25,000	21,000
08/01/04	60,000	52,000
08/06/04	74,000	84,000
08/13/04	35,000	38,000
08/27/04	4,000	5,000
08/28/04	4,000	5,000
08/31/04	8,000	8,000
09/03/04	42,000	55,000
09/10/04	59,000	46,000
09/17/04	116,000	91,000
09/19/04	95,000	89,000

Appendix D Treatment Plant Summary Reports (Demonstration Project Sampling Results)

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Oct-98

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

	SOLIDS	EFF,mg/I	3.6	4,4	22.4	8.8	4.0	0.0	27	116	7.6	7.2	7.6	5.6	10.4		4.8	1.0	1.8	0.00	7.7	5.0	2.6		2.8	5.2	3.2	5.6	3.6	7.2		4.4	4.0	7.2		6.1	194.1
	SHSDS	INF,mg/I	180	164	136	132	152	156		216	208	142	160	184	192		152	212	168	212	212	478	2		168	188	88	232	212	220		252	324	244		188.4	96.7%
	70	EFF,mg/I	3.2	2.0	3.4			***************************************	3.9	3.7	2.5			***************************************		4.1	3.4	12.3	5.8			***************************************	E 2	5.0	5.5	3.7	1.8				7.0	3.2				4.2	138.3
2000		I/BE, TVI	107.5	116.5	141.3				123.3	111.0	124.2					150.5	113.3	182.4	123.3			***************************************	1300	20.00	7.700.7	130.9	148.5				170.1	202.1				138.7	%6.96
OI INC 4HD	בונים,	ErF,III//	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	\$0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	×0.4	100		- 70.	7.00		Q0.1	<0.1 -	<0.1	<0.1	<0.1	<0.1		0.0	тах
SETT SOI	2 2	- 1/111, TVI	2	15.0	14.0	13.0	16.0	15.0	13.0	17.0	12.0	11.5	15.0	20.0	16.0	17.0	15.0	14.0	14.0	16.0	11.0	11.0	14.0	10.01	10.0	77.0	7.0	20.0	0.7.0	70.0	20.0	19.0	18.0	18.0	L	25.0	max
Hu	FEE MAX	_ 1	1.0	2./	1.1	7.7	7.7	7.8	7.7	7.6	7.5	7.6	7.5	7.4	7.5	7.6	7.4	7.1	7.2	7.1	7.1	7.4	8.3	7.6	7.6	7.5	7.5	7:7	7.0	٠. ' ر ۲	5.7	B./	1.1	7.8	C	6,3	max
Hu	FFF MIN	. 1	1.7	7.0	0.7	6.7	7.4	7.5	7.3	7.2	7.1	7.6	7.5	(.1	6.8	6.8	7.3	7.0	6.8	6.9	6.8	6.4	7.4	7.2	7.1	7.2	10	0 8	0.0	7.0		0.0	6.7	7.4	1 3	4.0	min
Ha	INF. MAX	14	1.7	1.7	1.7	5.7	7.3	7.4	7.2	7.2	7.2	7.6	7.7	ρ.α -	7.0	6.8	6.9	7.4	7.4	6.7	7.0	7.2	8.4	7.3	7.2	7.2	7.2	7.0	7.0	7.1	7.0	7.7	5.7	4.7	Va	+	шах
Ha	INF. MIN	7.3	7.1	7.3	5.7	7.7	(.1	7.1	7.0	7.0	6.8	6.9	0.9	0.7	6.7	0.0	6.7	6.9	6.9	6.6	6.7	6.3	7.2	7.2	6.9	7.0	6.8	6.8	6.9	6 9	7.1	7.7	7.7	- · /	6.3		
ATURE,C	EFF	10	193								19.4	19.4	n c		40.7	n c	10.7		18.4		15.8		15.9	15.4	15.2	17.7	18.6	18.7		19.5		17.9		-	18.5	0,6	ave.
TEMPERATUR	INF	17.2		16.9		2.0.0			0.7		7.0.	10.0 18 E	18.7					5.0			10.4		15.8		15.9		15.9			16.3		15.9		• 1	16.4		
	FLOW	4.280	3.602	3.653	3.517	2 817	0.0.0	0.04	5.700	2.500	2 500	3 627	3 300	3 76g	4 039	4 072	3 472	3 578	7.320	4.190	0.77.0	3.470	3.738	3.421	3.551	3.700	3.471	3.857	4.107	4.340	4.116	3.761	3.635		3.816	Monthly	
	DATE	-	2	က	4	rc	9	7	α	0	10	1.	12	13	14	1.5	16	17	α	0 0	000	240	- 20	777	23	24	25	26	27	28	29	30	31		AVERAGE		
	DAY	H-	LL	တ	S	Σ		M	<u></u>	- 1	. σ,	S	Μ	L	M	L		S,	S	Σ	<u> </u>	M	A A	- L	L (y)	S.	∑	-	≥	⊢	L1_	ဟ			****	

NIAGARA COUNTY SEWER DISTRICT #1

COMMENTS	COMMITTER														***************************************																			***************************************		***************************************
	***************************************		******						***************************************		***************************************				***************************************		***************************************		***************************************							***************************************						***************************************		***************************************	l l	, Section 1
							***************************************												-																30 da	7 423
F.COI I	/ 100 ml		28	1 F.		45	***************************************	42		39	105	3	***************************************		0	0		0	707		6		24		16	4		3	3	3		25	45		15.3	55.6
DUAL	AVE ma/I	0.58	0.73	0.69	0.73	0.49	0.62	1.04	96 0	0.76	0.73	0.67	0.62	0.50	0.00	0.00	0.50	000	0.40	0.57	0.61	0.51	0.39	0.46	0.44	0.72	0.66	0.55	0.47	0.65	0.44	0.45	0.44		1.04	
CHLORINE RESIDUAL	MAX.ma/I	0.64	0.76	0.71	0.77	0.72	1.28	1.18	1.13	0.81	0.79	0.80	0.64	0.53	0.68	0.00	0.71	- 2	75.0	0.0	0.72	0.61	0.43	0.54	0.48	0.83	0.70	0.61	0.56	0.70	0.58	0.62	0.64		1.28	
CHLOF	MIN,ma/I MAX.ma/I	0.48	0.70	0.67	0.68	0.32	0.27	0.86	0.87	0.70	0.63	0.58	0.59	0.45	0.57	0.40	0.47	77.0	0.50	0.00	0.48	0.42	0.36	0.40	0.40	0.65	0.62	0.51	0.40	0.59	0.36	0.25	0.25		0.25	
OROUS	EFF,mg/I	0.38	0.31	0.39	0.34	0.42		0.55	0.44	0.61	0.57	0.30	0.32		0.55	0.33	0.28	0.49	0.34	00.0	0.32		0.81	0.35	0.31	0.31	0.39	0.46		0.52	0.43	0.34	0.34	••••	0.42	13.2
PHOSPHOROUS	INF,mg/I	4.13	4.50	3.36	9	4.13		3.36	3.36	8.86	2.63	1.90	8.22		3.32	1.82	4.69	3.12	2.06	4.70	27.5	2 04	10.0	3.85	4.17	5.02	4.81			8.59					4.46	
	FLOW	4.280	3.602	3.653	3.517	3.815	3.941	3.708	5.306	3.977	3.592	3.627	3.300	3.768	4.039	4.072	3.473	3.528	4.190	3 774	3 428	3 728	0.700	3.421	3.551	3.700	3.471	3.857	4.107	4.340	4.116	3.761	3.635		3.816	-
	DATE	7	2	3	4	5	9		8	6	10	11	12	13	14	15	16	17	18	19	20	21	200	777	23	75	72	7.0	2/	228	87	30	31	70000	AVERAGE	~
	DAY	-	ш	ഗ	s :	Σļ	- :	X	-	4	S	S	Σ	<u> </u>	>	<u> </u>	ш.	ဟ	S	∑	L			- -	L C	n u	2	∑ ⊦		<u>}</u> ⊦	- 1	(0			-

NIAGARA COUNTY SEWER DISTRICT #1 Nov-98 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

FRANK A. Nerone, P.E. CERT. 4A

716-693-0001 716-693-8759 FAX

SOLIDS	EFF.ma/I	44	7.2	96		112	7.6	0:0	900	200	100	9.7	10.0	2.0	4.0	2.6	8.8	6.0	7.6	18.1	6.5	10.0	9.0	9.6	5.0	7.4	7.6	14.0	40	00	40	ς Υ		8.1	253.2
SUSP S	INF,mg/I	****	184	260		228	304	220	277	177	308	284	212	232	202	230	380	232	260	240	176	252	224	344	188	276	236	304	204	224	216	184		250.4	96.8%
OD	EFF,mg/I			,	8.5	6.6	7	88				6.9	5.6	5.8	10.5	7.01				10.9	9.1	12.4	12.8				12	8.2	52	4.7				8.2	258.4
CBOD	INF,mg/I				160.6	192.8	187.8	131.8				245.3	147.2	148 G	153.0	2.22				150.4	133.1	124.7	110.9				256.2	236.1	234.8	175.8				171.9	95.2%
SOLIDS,1HR	EFF,mI/I	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	×0.1	<0.1	40.4	- 7	- 10	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		<0.1	<0.1	<0.1		0.0	max
SETT SOI	INF,mI/I	17	18.0	16.0	15.0	16.0	27.0	17.0	20.0	21.0	22.0	28.0	14.0	16.0	25.0	23.0	23.0	0.07	14.0	0.71	14.0	15.0	16.0	17.0	10.0	22.0	20.0	20.0		9.0	12.0	15.0		28.0	тах
Hd	EFF, MAX	7.7	7.6	7.8	7.8	7.4	7.5	7.2	7.2	7.2	7.4	7.4	7.5	7.2	7.2	7.1	7.0	7.8	7.0	0.7	9./	8.2	6.7	8.2	8.0	7.9	7.8	7.7	7.7	7.6	7.6	7.6		8.2	max
рН	Z	(.1	7.2	7.4	7.5	6.8	6.9	7.1	7.2	7.0	6.8	7.3	7.3	7.0	6.9	6.7	7.0	7.2	7.1	- 7	7.7	0.)	0.7	(.2	7.4	7.5	7.7	7.7	7.7	7.2	7.5	7.5		6.7	min
	INF, MAX	<i></i> , . <i></i>	7.4	8.7	7.8	7.1	0.7	7.1	7.2	7.2	7.3	7.3	7.5	7.2	7.2	6.9	7.0	7.6	7.6	0.7	7.0	1.9	F. 7	/:/	G. 1	6.7	7.8	/./	7.7	7.6	7.6	7.5		8.1	max
익!	INF, MIN	0.,0	9.9	7:7	7.1	6.8	7.0	6.7	6.9	6.8	6.9	6.9	7.0	7.0	6.8	6.6	6.9	6.9	7.4	5.7	7.0	0.0	0.0	S. /	4:1	5.7	7.7	7.,	7.2	7.1	7.0	1.1		0.0	mm
1 URE, C	17.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.		10.9		10.0	5.7.	0.71	16.3	16.9	16.5	16.7	16.7	16.4	15.9	16.6	16.5	16.3	16.3	16.2	18.2	18 a	15.6	7 9 7	7 4	10.1		10.1				15.4		707	10.4	ave.
INIT CALORE	45.7		15.7	15.5	10.0	15.2	7.0	0.61	15.4	14.2	15.3	15.1	5.0.	14.3	14.6	14.7	14.8	14.8	14.6	14.2	16.8	15.0	14.0	14.0	150	0.07	14.0	2.7	1.4.4	5.4.0	7.41	S.4-	15.0	0.51	ave.
EI OW	3 800	3 736	3.130	3 300	2.009	3 888	0.000	4.010	0.925	3.002	3.830	4.013	0.004	3.270	3.841	3.796	3.873	4.086	3.637	3.649	4.643	3.879	3.607	3 343	3 341	3 717	3 496	3 400	3 554	2 572	2.212	21.5	3 711	Monthly	() () () ()
DATE	111	2	3 6	Ž	- 10	9	2	- a	0 0	40	2 7	- 07	43	2 7	7 1	0 (16	17	18	19	20	21	22	23	24	25	26	27	78	29	30		AVERAGE		· · · · · · · · · · · · · · · · · · ·
DAY	 -	Ц	S	S	≥	 -	M		- 11		0	ρΣ	-	///	<u>}</u> -	-14	L C	ח	တ	Σ	 -	≯	⊢	F	S	S	Σ	-	W	 -	Ц				

NIAGARA COUNTY SEWER DISTRICT #1

∞
Ó
>
<u>o</u>
Z

	T	T				T		T	7		T		T									Ţ			7	T									
COMMENTS	COMMENTS		***************************************			The second secon	au unificial anne principa de un esta de la compansa de la compansa de la compansa de la compansa de la compan		***************************************					***************************************	***************************************		***************************************						AAAAA TUURAAA	***************************************		***************************************		**************************************						30 day 400m	7 day geom
F.CO[1	/ 100 ml		α		11	-	3	0 00	· · · · · · · · · · · · · · · · · · ·	,		30		3.2	22	777		95	***************************************	D.		က	16		20		72	***************************************	11	14	-	- F F	-	118 30	
DUAL	AVE ma/I	0.64	0.60	0.59	0.58	101	141	108	100	1 04	103	1.27	0.72	1 23	1 15	50.7	20.7	to: 1	1.07	0.87	0.80	0.84	0.85	1.00	0.99	0.92	0.77	0.64	0.68	0.70	0.75	0.62	0.02	141	
CHLORINE RESIDUAL	MIN,mg/I MAX.mg/I AVE mg/I	0.70	0.65	0.62	0.77	1 12	1.50	112	1 12	1 06	1 06	131	0.85	134	1 27	1 10	200	0.20	1.25	00.0	0.82	0.90	0.93	1.06	1.07	1.00	0.82	0.70	0.75	0.72	0.80	0.78		1.50	
CHLOF	MIN.ma/I	0.60	0.54	0.54	0.40	0.94	1.33	1.05	0.92	1.02	1.00	1.24	0.53	1.14	66 0	0.01	0.0		0.80	0.03	0.74	0.77	0.80	0.95	0.90	0.78	0.68	0.56	0.61	0.68	0.67	0.37		0.37	
OROUS	EFF,mg/l	0.44	0.45		0.91	0.47	0.40	0.46		0.38	0.43	0.48	0.74	0.33	0.36	0.55	0.53		000	00.0	0.10	0.39	0.40	0.46	0.52		0.24	0.58	0.44	0.41	0.38	0.51		0.48	14.9
PHOSPHO	INF,mg/I	5.10	4.33		8.46	4.00	3.56	4.21		3.80	4.94	3.88	3.44	6.60	5.14	6.64	1.01		5.02	3 24	13.0	10.0	3.32	2.95	4.37		3.73	4.50	4.62	3.93	4.17	3.75		4.21	
	FLOW	3.899	3.736	3.600	3.309	3.996	3.866	4.016	3.925	3.082	3.935	4.013	3.834	3.276	3.841	3.796	3.873	4 086	3 637	3 649	1 6/3	010.0	0.078	3.507	3.343	3.341	3.71/	3.496	3.409	3.551	3.572	3.401		3.711	
	DATE	-	2	ж К	4	5	9	7	ω	o.	10	11	12	13	14	15	16	17	18	19	20	24	22	77	220	74	07	07	77	28	58	30		AVERAGE	
	DAY	<u> - </u>	L	ഗ	တ	Σ	 -	>	⊢	<u></u>	တ	S	≥	<u> </u>	≥	 	Ľ.	ഗ	S	Σ	<u> </u>	>	1	- 1	_ 0	0	0 2	Σŀ	- 1	X	- 1	_			

FRANK A. NERONE

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Dec-98

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

CBOD SUC. INF,mg/l EFF,mg/l 184 12.0 294.2 7.0 13.0 3.6 10.4 5.2 6.0 7.2 12.1 12.0 12.0 14.0 10.0 12.0 15.0 7.0 6.0 8.5 5.0 4.0 4.0 9.5 5.0 7.3 9.0 96.2% 236.8 132 148 164 176 204 176 184 260 92 232 220 216 300 280 180 756 212 260 256 244 244 152 500 204 208 344.5 11.0 10.8 16.0 9.6 14.3 10.4 12.0 24.5 14.4 19.1 8.0 7.2 10.2 6.8 5.0 3.3 8.7 6.4 175.5 290.0 187.6 144.4 144.4 93.1% 115.5 136.2 140.2 158.2 123.3 155.9 145.7 153.9 158.9 164.7 142.2 154.0 136.7 156.1 SETT SOLIDS,1HR INF,ml/! EFF,ml/! 0.0 тах <0.1 0.0 <0.1 6.6.6.6 \$0.1 40.1 <0.1 <0.1 0.0 0.0.0 0.0 9 9 9 9 Ô Ŏ. 0. 0 0 Ö. ô 16.0 22.0 22.0 22.0 22.0 18.0 16.0 18.0 17.0 32.0 max 14.0 13.5 16.0 15.0 15.0 15.0 19.5 18.5 21.0 15.0 16.0 32.0 18.0 EFF, MAX 8.1 max 7.6 7.5 7.5 7.6 7.8 7.7 7.7 7.9 7.9 8.1 7.8 7.6 7.6 7.6 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.4 Hd EFF, MIN 6.6 min 7.7 7.8 7.5 7.6 7.7 7.7 7.7 7.3 INF, MAX тах 7.5 6.9 7.6 7.5 7.5 7.3 7.3 7.3 7.1 7.4 7.2 7.2 7.4 7.4 7.4 7.2 7.1 7.0 7.2 7.2 7.4 INF, MIN 6.9 6.8 6.8 7.0 6.8 6.8 9.9 7.4 7.3 Ē 7.4 Hd TEMPERATURE,C 16.5 16.6 15.2 15.2 15.4 15.1 16.4 15.5 15.8 15.0 15.5 15.4 14.8 14.6 15.1 15.0 14.0 12.8 13.3 12.9 13.5 16.3 17.6 13.9 13.8 15.0 ave. 13.5 13.5 13.6 12.8 12.8 14.1 14.2 14.4 14.0 13.7 13.7 13.7 13.6 13.6 12.6 13.8 13.8 13.9 13.9 13.4 ave. 3.983 3.552 4.488 3.809 3.501 3.638 3.338 3.868 3.340 4.089 4.066 4.261 4.291 3.948 4.104 4.145 3.820 3.928 3.927 5.501 3.488 4.027 3.837 3.892 3.901 Monthly FLOW AVERAGE DATE 9 Ξ 4 0 ထတ DAY டில்ல யலல≥ တ္တΣ ⋛ ∑⊩ |≥|⊢ ≥ ш ≥ பட ഗ ഗ≥ ≥

NIAGARA COUNTY SEWER DISTRICT #1 Dec-98

COMMENTS	CIMINIEINIS																																		1	моер у
F.COLL	/ 100 ml		22	, to the same of t	150	420	0.71	σ		3		<i>VC</i>	13	2	E			0	000	00	14		_			-	52	20		26		ю			16.2 30 day	
DUAL	AVE.ma/I	0.70	0.60	0.35	0.34	0.21	1 14	1 24	1 58	1 74	1 45	1 10	1.25	1 30	20.1	800		0.30	0.00	3,0	0.72	0.77	0.94	0.82	0.70	0.66	0.73	0.81	0.80	0.76	0.82	0.63	0.72		1.74	
CHLORINE RESIDUAL	MIN,mg/I MAX,mg/I		0.70	0.41	0.48	0.25	1.28	1.40	1 94	1 96	1 69	1.36	137	1.56	1 10	1.04	101	70.0	0.75		0.30	10.0	10.1	1.02	0.83	0.73	0.04	0.00	0.30	0.87	0.93		0.77		1.96	
CHLO	MIN,mg/I	0.67	0.46	0.28	0.20	0.18	0.94	1.16	134	1.47	1.20	102	1.13	122	0.98	0.86	0.71	0.72	0.54	0.0	0.02	0 0	0.00	0.54	0.55	40.0	0.00	0.70	0.70	0.00	0.75	0.52	0.63		0.18	
OROUS	EFF,mg/l		0.60	0.55	0.21	0.38	0.34	0.45	***************************************	0.54	0.50	0.39	0.47	0.34	0.35	0.60	0.52	0.50	0.45	0.43	0.43	2	7.7.0	1.00	67.0	24.0	0.35	0.00 98 0	9	7000	0.07	0.50	0.00		0.44	14.3
PHOSPH	INF,mg/I		4.29	3.28	5.75	6.15	2.26	5.14		3.11	1.30	1.42	4.45	6.97	2.06		11.90	4.70	6.16	4 25	4.50	3.81		2 55	3.20	3.48	5 14	3.38	3 8E	3	1 7		4.81	00,	4.43	
	FLOW	3.998	3.961	4.089	3.672	4.066	4.261	4.291	3.948	3.983	3.552	4.488	3.901	3.809	3.745	4.104	3.501	3.638	3.338	3.868	3.340	4.027	5 501	7.40	3 837	3.820	3 747	3.928	4.010	3 802	2,002	201.00	3.400	2 007	2.261	
	DATE	-	2	3	4	5	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	34		AVERAGE		
	DAY	-	8	-	_	S	တ	Σ	<u> -</u>	8	F	LL.	တ	S	Σ	⊢	M	H	ΙL	ഗ	S	M		X	_	Ц	S	S	Σ		M	<u></u>				

ER DISTRICT #1	Nov-99
VIAGARA COUNTY SEWER	SPDES # NY-0027979

7346 LIBERTY DRIVE

!		SOLIDS	EFF,mg/I	3.5	4.8	15.0	9.5	3.8	4.2	5.6	0.9	1.5		1.0	1.2	2.5	14	13	22		22	24	24	3.0	2.6	3.2		2.4	4.0	2.0	20	3.4	2.8		4.7	250.0
FRANK A. Nerone, P.E. CERT. 4A		// T	<u>/f</u>	312	324	228	164	88	108	120	84	128		40	128	140	140	184	216		688	316	204	212	184	228		320	220	164	100	128	264		195.2	07 60/
FRANK A. CERT. 4A	20	OD.	EFF,mg/I			6.8	23.6	3.7	5.2				3.1	3.3	1.4	1.5				3.0	2.5	1,8	1.9				2.0	2.7	3.0	2.1					5.6	331.3
)01 '59 FAX	מטמט	ואור	I/gm,¬vi			90.2	77.3	114.8	97.3				135.6	116.0	92.7	85.9				197.2	218.7	204.2	32.8				136.2	194.6	132.9	105.9					120.0	95.3%
716-693-0001 716-693-8759 FAX	SOI IDS 1HB	- EEE - 11 11 11 11 11 11 11 11 11 11 11 11 1	LL L 1111/1	<0.1	40.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	max
	SETTSO	INE mil	1/1111, 1811	47	20.0	11.0	8.0	11.0	12.0	12.0	12.0	13.0	15.0	15.0	10.0	10.0	3.0	15.0	7.0	13.0	0.0	22.0	15.0	11.0	10.0	12.0	13.0	18.0	12.0	10.0	7.0	12.0	15.0	0.70	74.0	шах
N YORK	Ha	Ϋ́	7 /	7.7	5,7	1.0	5.7	7.0	7.7		7.1	0.7	6.9	0.9	0.7	0.7	(.1	7.0	7.0	6.7	7.1	7.1	6.8	6.9	7.2	7.3	7.6	7.4	7.5	7.3	7.5	7.5	7.5	7.6	0.1	max
7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	Hd	Z	-	1.7	7.7	7.3	5.0	0.0	0.0	0.0	0 0	5.0	9.0	0 0	0 0	0.0	D. C.	9.0	0.7	6.7	7.0	6.9	6.7	0.0	7.1	7.3	4.7	1.4	4.7	7.7	4.7	4.7	7.1	9	0.0	LIE
NAGARA I	hd	X	-	7.3	7.1	7.0	7.7	7.7	5.7	7.0	0.0	0.0	7.0	7.7	7.7	1.	1.0	0.1	۲.)	9.9	7.2	1.7	4.7	(·.)	7.3	1.,	7.7	7.0	0.7	5.7	5.7	1.4	4.4	7.8	200	HIGY
_	Hd	INF, MIN	7.1	6.7	6.6	0 4	0.0	6.7	200	. u	200	- 4	0.0	2 0	200	2.4	- 0	0.0	0.0	5.0	1 0.8	7.0	0.7	7.0	7.0	7.7	7.7	5.7	5.	7.7	7.7	7.7		6.3	nim	-
66-voN	TURE,C	EFF	20.1	18.7	14.8	14.9	15.9	16.2	150	7.0.0	16.7	17.7	16.7	16.0	16.5	16.0	78.0	- T	5.0	10.4	10.0	16.0	18.0	17.0	17.6	17.7	18.7	16.4	7.0.7	ייים ליי	2 L	- 0	2	16.3	aVe	
	TEMPERATURE,	INF	16.5	16.9	15.4	15.2	15.5	15.9	15.7	15.9	16.1	16.2	15.9	15.7	157	15.9	15.8	15.2	15.2	20.0	15.4	15.0	15.2	150	15.2	15.0	15.1	14.9	14.3	14.3	14.6	14.6	2	15.5	ave.	
SPDES # NY-0027979		FLOW	4.997	8.187	21.379	10.983	8.486	6.968	5.474	4.953	5.341	5.252	5.823	5.438	4.864	5.115	5,171	5.094	4 643	4 425	4 147	5 408	4.419	4 659	4.482	4.476	4.410	6.870	9.628	6.702	5.809	4,689		6.276	Monthly	
SPDES # N		DATE	-	2	က	4	5	9	7	8	0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE		
0,		UAY :	Σ	F	3	⊢	ш	ഗ	တ	Σ	⊢	>	F	ഥ	ဟ	ဟ	Σ	F	*	-		S	S	Σ	 -	×	⊢	LL_	ഗ	S	S	<u> </u>		A		

FRANK A. NERONE

NIAGARA COUNTY SEWER DISTRICT #1

COMMENTS	COMMITTALIS																																			
F.COLI	/ 100 ml			84		26	2 0	2	C	0		0	c	200	3	-			9		6.) (r	2	0	2	6	2	c	2 0	2					4.4	18.7
DUAL	AVE.mg/I	0.56	0.52	0.53	0.33	0.50	0.87	100	280	0.00	080	0.03	0.75	0.70	20.0	0.12	0.58	0.75	0.64	0.75	0.61	0.60	0.00	0.73	0.00	38	20.0	10.0	40.0	2 0	0.43	000	0.42	00,	1.00	
CHLORINE RESIDUAL			0.58	0.73	0.43	0.78	133	1 07	0.1	08.0	0.00	0.00	0.00	2 6	0.00	0.73	0.70	0.83	0.78	0.92	0.68	0.65	0.72	101	0.70	0.18	0.50	030	0.00	0.50	0.00	30.0	0.48	1 22	00.	
CHLOF	MIN,mg/I MAX,mg/I	0.52	0.41	0.39	0.21	0.30	0.19	0.01	0.58	0.72	0.84	0.63	0.70	0.72	0.70	0.10	0.00	0.70	0.41	0.45	0.55	0.57	0.62	0.56	0.56	0.31	0.23	0.25	0.33	030	0.50	200	0.33	0 10	2	
OROUS	EFF,mg/I	0.24		0.40	0.24	0.23	0.21	0.01	0.02		0.05	0.02	90.0	000	0.14	1 2 0	2	i	0.25	0.19	0.23	0.20	0.29	0.21		0.17	0.19	0.21	0.14	0.15	0.19			0.20	10.4	C.U.
PHOSPHOR	/b	5.47		1.70	1.82	2.02	3.56	3.03	1.94		1.86	6.48	2.88	2.67	3.28	4 17		1 77	(.5/	21.34	7.45	3.93	3.32	4.41		5.10	7.49	3.32	2.19	2.27	1.54			3.78		
	FLOW	4.997	8.187	21.379	10.983	8.486	6.968	5.474	4.953	5.341	5.252	5.823	5.438	4.864	5.115	5.171	ת ה	0.00	240.4	4.475	4.147	5.408	4.419	4.659	4.482	4.476	4.410	6.870	9.628	6.702	5.809	4.689		6.276		
	DATE	-	2	က	4	2	9	7	8	6	10	11	12	13	14	15	16	17	- 07	0 5	6	07.	21.	22	23	24	25	26	27	28	29	30		AVERAGE		
	DAY	Σļ	- :	X	_	L	S	တ	∑	Ы	≥	H	ഥ	ဟ	ဟ	Σ	-	M	-	- L	L	ח	v) :	Σ		≥		1	တ	S	∑	<u></u>				

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Dec-99

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

FRANK A. Nerone, P.E. CERT. 4A 716-693-0001 716-693-8759 FAX

	SOLIDS	INF,mg/I EFF,mg/I		8.4	3.4	2.4	10.	7.0		1.8	0	20	o ii	22	30	0.5	5 4	2 6.	1 6.	3.5	1 5	2.5	0.4	-	Ç	7 7	7.0	0 0	0.0	0.0	7.0	30	2.0	6.0	10	101.2
0.10	SUSP	INF,mg/I		216	180	188	184	180	200	132	180	180	156	160	200	108	228	164	192	112	156	132	76		121	140	148	236	232	34R	P	12/	128	03	169 5	98.9%
40	חס	EFF,mg/l	14.8	7.3	7.5	3.2				<u>ر</u>	יר ה	1.5	3.4				6.2	3.2	2.8	3.6				28	7	2.5	3.0				28	24	8.9		3.9	213.6
מטפט	0.5	l/gm, ⊣NI	172.7	192.6	162.7	148.4				127.2	1703	119.7	21.0				133.2	72.6	95.4	105.6				120.2	176.3	147.0	158.8				158.0	180.2	142.2		127.2	%6.96
SOI IDS 1HP	בורל, יוווי	Err,mI/I	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.7	×0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	\$0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	max
SETT SOI	INE	- 1	,	14.0	15.0	11.0	15.0	14.0	11.0	13.0	13.0	16.0	10.0	16.0	14.0	14.0	14.0	7.0	10.0	8.5	14.0	15.0	12.0	15.0	13.0	9.0	13.0	15.0	14.0	11.0	16.0	16.0	14.0		16.0	max
Ha	FEE MAX	7,	4.7	7.3	6.7	7.4	7.5	7.2	7.2	7.2	7.1	7.2	0.7	1.1	0.7		6.9	6.8	0.7	0.7	7.7	7.1	7.3	7.4	7.1	7.2	6.9	6.9	6.9	7.2	7.2	7.1	7.5		7.5	шах
Hd	EF	i	7.7	- 1	6.7	7.3	(.1	7.1	6.7	6.6	6.6	6.9	0.0	0.0	0.0	ρία	0.0	8.0	0.0	10.0	0.7	9.9	7.0	(.3	6.4	6.5	6.8	6.6	9.6	6.8	6.2	7.0	7.4		6.2	uim
Hd	INF, MAX	7.4	7.7	t.7	7.0	۲. کا	5.7	7.1	7.2	7.0	7.2	7.1	1.0	- 0	7.0) a	100	1.	7.7	2.7	7.7	7.7	0.7	7.4	7.2	6.3	0.0	1.0	7.7	1 0	7.7	7.7	4.7	1	4.4	ıııax
ЬH	INF, MIN	7.1	7.1	- 8	9 0	0.0	9.0	9.0	6.6	6.5	0.0	٠. ۵ ۵	0.0	ο α	0 0	B 0.0	0	0 0	0.0	200	2.5	7.1	7.3	0.0	4.0	0.0	7.0	, w	0.0	7 0	7.0	- 1	3.	F 4	i.i	
ATURE,C	EFF	14.7	14.4	15.6	10.0	- 6	20.0	- 10.	0.0	15.4	13.3	14.5	14.3	14.6	14.3	13.8	120	12.5	12.7	12.9	13.3	128	114	77	0 4	7. T	2 4 2 5 4 5	11.5	7 2 2	7 5	12.0	12.0		13.6	aVe	
TEMPERATURE,	HN.	14.5	14.5	14.7	14.8	14.6	150	17.7	t v	14.5	- L	14.0	13.7	14.0	13.9	13.1	12.8	12.4	12.5	12.7	13.0	12.4	12.1	121	- Z	117	11.9	11.8	11.9	11.9	12.0	11.6		13.2	ave.	
	FLOW	4.753	5.353	4.906	5.600	5.339	5.556	5.35.8	2.000	5.830	7.563	7.439	7.264	7.517	8.580	11.839	13.154	11.754	6.147	5.595	5.416	6.950	5.745	4.694	4.313	4.561	5.152	4.848	4.614	5.028	4.903	4.687		6.316	Monthly	
	DAIE	-	2	ဗ	4	IJ	9	7	α	0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		AVERAGE		
747	147	>	-	LL.	ဟ	တ	Σ	 -	3	 -	L	S	တ	∑	F	>	<u>-</u>	ш	S	တ	Σ	H	>	H	ш	Ś	S	Σ	⊢	8	<u>-</u>	LI.				

NIAGARA COUNTY SEWER DISTRICT #1 Dec-99

STNEMMOO																the state of the s								The state of the s											
F.COLI	/ 100 ml	6		٣.	0 (0				e.		с.) (C				25		c	8 4	+				2	77	_ ~	2			0		15	2	5.2	9.8
DUAL	AVE,ma/I	0.46	0.52	0.57	0.33	0.08	0.30	0.39	111	0.94	0.95	0.81	0.72	0.88	0.78	0.46	0.87	20.0	0.79	0.78	2000	20.0	70.0	0.02	0.00	0.70	0.00	0.52	0.02	0.00	0.39	0.28	21.	1.11	
CHLORINE RESIDUAL	MIN,mg/I MAX,mg/I AVE,mg/I	0.55	0.80	0.59	0.38	0.13	0.43	0.85	1.15	0.95	0.97	0.90	0.86	1.05	0.82	0.49	1 15	0.95	0.94	0.83	90.0	2000	0.00	00.0	0.00	0.00	0.52	0.55	0.50	0.48	0.42	0.33		1.15	
CHLOF	MIN,mg/I	0.37	0.38	0.54	0.24	0.05	0.15	0.08	1.08	0.94	0.92	0.72	0.45	0.77	0.70	0.45	0.41	0.68	0.62	0.67	0.64	0.57	0.57	20.07 38	0.00	0.42	0.39	0.46	0.44	0.32	0.36	0.25		0.05	
OROUS	EFF,mg/I	0.26	0.25	0.27	0.19	0.16	0.13		0.19	0.25	0.21	0.17	0.19	0.22		0.30	0.18	0.12	0.13	0.16	0.13		0.18	0.10	0.15	0.17	0.20	0.18		0.17	0.16	0.17		0.19	10.2
PHOSPHC	INF,mg/I	4.94	6.60	4.66	4.86	6.16	5.59		5.71	1.70	7.33	3.68	2.43	3.32		3.40	1.99	2.88	0.69	2.79	3.28		2.06	2 79	3.24	4.94	3.60	3.48		3.89	4.05	1.78		3.65	
	FLOW	4.753	5,353	4.906	5.600	5.339	5.556	5.368	5.540	5.630	7.563	7.439	7.264	7.517	8.580	11.839	13.154	11.754	6.147	5.595	5.416	6.950	5.745	4.694	4.313	4.561	5.152	4.848	4.614	5.028	4.903	4.687		6.316	
	DATE	-	2	8	4	2	9	7	8	0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	10.00	AVERAGE	
	DAY	>	-	ഥ	S	က ု	Σ	-	8		ഥ	တ	တ ြ	Σ		8	<u> -</u>	LL	S	S	Σ	⊢	M	L	ட	တ	တ	∑	 	≥	ı-	iL			

NIAGARA COUNTY SEWER DISTRICT #1 May-01 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-8759 FAX 716-693-0001

INF,mg/I EFF,mg/ 10.0 10.0 SUSP SOLIDS 3.6 3.2 4.6 8.8 9.6 4.0 2.0 4.3 3.3 2.0 5.0 2.8 9.2 5.2 5.2 5.2 FRANK A. Nerone, P.E. CERT. 4A 96.5% 149.1 244 268 308 372 272 272 232 232 42 108 179 179 179 136 146 172 120 188 68 448 72 64 92 93 84 INF,mg/l EFF,mg/l 219.0 10.2 6.3 3.2 3.2 2.7 9.8 4.1 CBOD 263.4 237.5 246.0 269.6 243.9 224.6 246.5 158.9 163.4 180.9 163.6 207.3 97.5% 161.9 113.5 121.0 104.1 88.7 81.3 81.7 EFF,mI/I SETT SOLIDS, 1HR 0.0 тах **0.** 6.6 6.6 0.0 0.0 6.6 0.1 40.1 0.1 <0.1 0.0 6.6.6.6 <u><0.1</u> 0, 0.0 0.1 40.1 0, ô 8 INF, HI 31.0 23.0 26.0 30.0 31.0 4.0 5.0 5.0 3.0 2.5 max 5.0 EFF, MAX max 6.9 7.1 7.2 7.2 7.3 7.3 7.5 6.9 7.0 7.1 7.1 7.3 7.4 7.5 EFF, MIN 6.9 6.8 7.0 7.0 7.0 7.0 7.0 7.0 7.0 6.8 7.2 6.9 6.9 7.2 6.6 min INF, MIN INF, MAX 6.9 7.3 max μd 7.3 7.0 7.5 7.1 7.3 7.2 7.5 7.0 6.5 6.8 6.6 7.0 6.8 6.8 7.0 6.8 7.0 6.9 6.5 min 6.6 6.6 pH TEMPERATURE,C 16.6 16.0 15.7 16.0 16.4 15.7 15.8 16.3 16.4 15.9 16.6 17.0 15.9 15.2 15.7 16.2 15.2 16.6 15.9 16.5 15.1 16.4 14.6 15.2 15.5 15.9 ave. 15.1 10.4 10.9 10.9 10.5 10.6 12.1 12.2 11.4 12.1 12.6 10.4 10.7 11.7 11.7 13.2 12.5 ave. 11.7 4.877 5.716 5.115 5.118 5.243 5.298 6.286 10.188 13.024 8.968 7.758 6.610 4.290 5.333 4.988 5.277 6.364 5.597 5.403 9.219 5.067 4.661 5.782 7.630 4.977 Monthly FLOW AVERAGE DATE ထတ DAY ⊥ w w ≥ $\pi |\omega|\omega|\Xi$ ≥ ≥ L 0 0 ≥ ≥ LL (の (の)≥ ≥ ≥

284.0

NIAGARA COUNTY SEWER DISTRICT #1 May-01

CONMINITALES	COMMENTS																															And the state of t			
F CO1 -	/ 100 ml		8		3000	1020				4		m	l c				520	O. C.	640	7 4 4	2				D C		1	4			6	2		28.1	337.0
DUAL	AVE.mg/I		0.66	0.08	0.61	0.44	0.37	0.36	0.52	0.68	0.47	0.46	0.38	0.39	0.00	0 19	0.29	0.27	0.60	007	20.0	0.00	0.97	0.00	00	0.0	0.00	0.01	- 7.0	20.00	20.0		80.0	76.0	
CHLORINE RESIDUAL	MAX,mg/I	0.39	0.85	0.14	1.06	0.85	0.45	0.39	0.65	0.90	0.51	0.53	0.39	0.40	0.42	0.28	0.32	0.42	75.0	1 12	101	1 10	7 0 0	00.00	280	77.0	0 80	7,00	00	0.00	0.83	1 02	1.02	1.12	
CHLOI	MIN,mg/I	0.23	0.52	0.00	0.12	0.09	0.28	0.31	0.39	0.55	0.41	0.40	0.37	0.37	0.20	0.08	0.27	0.08	0.32	0.74	0.72	0.72	0.72	0.02	0.34	0.39	0.39	0.62	0.05	0.65	0.75	0.73	3	0.00	
OROUS	EFF,mg/I		1.74	1.02	0.85	0.82	0.43	0.54		0.26	0.22	0.20	0.30	0.32	0.30		0.47	0.35	0.34	0.20	0.35	0.41		0.35	0.27	0.28	0.39	0.33	0.16		0.49	0.29	2	0.42	22.6
PHOSPH(INF,mg/I		6.16	7.17	3.69	11.83	1.58	1.46		2.27	3.24	3.52	1.01	3.64	3.81		3.04	0.32	3.04	4.53	2.91	2.34		2.59	1.54	1.62	2.67	1.50	4.78		2.18	2.35		3.13	
	FLOW	5.129	5.296	5.021	4.877	5.178	4.290	5.333	4.988	5.716	5.067	5.277	6.364	5.597	5.403	4.977	5.115	5.118	5.243	4.661	5.298	6.286	10.188	13.024	8.968	7.758	5.782	9.219	12.158	11.520	8.432	7.630		6.610	
	DATE	_	2	3	4	ιΩ	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 ·	25	26	27	28	29	30	31		AVEKAGE	
	DAY		≫			S	S	Σ	<u> </u>	3	_	4	y) (S)	∑	⊢	8	-	ഥ	တ	တ	Σ	⊢	>	-	ш.	ഗ	S	≥	<u> </u>	M	-			

R DISTRICT #1	Jun-01
NIAGARA COUNTY SEWER DIST	SPDES # NY-0027979

	Г	ı	ΞT	_	_			-1	_	1	7	7		7					ļ	ļ			1		Ţ	Γ	ļ		T	T	1	1	 		
иį	9	SOLIDS	Err,mg/	0.4	4.4	3.6	9.6	υ. Σ	0.0	2.4	+ 6	4,7	7	5.8	4.0	3.6	3.8	3.0	2.2	3.0	4.0	3.5	11.6	11.6	5.2	6.8	6.5	11.2	9.2	6.7	5.3	3.7	7.3		5.5
Nerone, P.		S ACOC	INF, mg/I	871	011	1444	717	2	2 2	20	0 1	200	20.	104	208	104	160	212	160	376	252	244	348	372	176	172	128	268	184	212	132	192	152		165.7
FRANK A. Nerone, P.E. CERT. 4A	2	טוט ברד שביוו	EFF,1119/1	0.0	0.2			c	0.0	2.0	c	7.0			J	6.5	12.9	13.0	18.3		-		5.6	9.4	3.4	4.3				1.4	4.1	3.8			6.3
*	0000	INE ma/I	1/8111, 11811	140.4	2			1281	165.1	143.1	1510	•			000	168.2	181.4	319.1	429.0				285.1	171.3	212.8	206.2				148.1	152.1	234.8		0 001	193.8
716-693-0001 716-693-8759 FAX	SOI IDS 1HD	EEE ml/l	1 - 1			- 7		V 0.	, C	\$ 0.1 0.1	40.4	\$0.4	50		- 7	V.U.	<0.1	۲.0>	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0	0.0
•	SETT SOI		יי	2.6	2 2	000	יין ל	5.0	27.0	5.5	45	5.0	כיי	1 7 Y	. t	0.0	0.0	0.0	18.0	25.0	24.0	24.0	35.0	20.0	18.0	18.5	4.5	5.0	4.0	8.5	5.0	12.0	5.5	0 110	0.00
: W YORK	Hu	ΑX	73	7.3	7.0	7.0	7.2	7.3	7.3	7.2	7.2	7.1	7.2	7.0	7.0	7.7	7.7	10	7.7	7.7	0.7	1.1	7.4	7.3	7.4	6.3	- 0	9.9	(.2	7.2		6.9	7.2	7.4	ţ.
7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	H	EFF. MIN	7.3	7.3	7.0	7.0	7.2	7.3	7.3	7.2	7.2	7.1	7.2	7.0	7.2	7.7	7.4	- 1	7.7	7.7	1.0		4.7	1.3	4.7	5.7	- 0	0.0	7.7	7.5		6.9		0	6:5
7346 LIBEI NIAGARA	Ha	INF, MAX	7.3	7.3	7.3	7.4	7.4	7.3	7.4	7.5	7.5	7.3	7.4	7.4	7.2	7.9	7.2	7.7	7.3	3.7	- 0	10.0	5.7	5.7	0.7	5.7	5.7	7.0	7.7	1.7	7.7	6.3	7.2	7.5	2
#1	Hd	INF, MIN	7.2	7.3	7.1	7.0	6.9	7.2	7.2	7.2	7.2	7.2	7.0	6.8	7.0	7.0	88	7.4	7.0	0.0	3.0	7.7	- '- '	7.1	7.1	7.2	1 0	200	9 O	0,0	50 0	0.0	1,1	6.2	
	ATURE,C	EFF	15.6	16.0	16.4	15.9	15.0	17.1	17.5	17.6	17.6	17.8	17.4	16.3	18.3	18.1	18.5	190	10.0	γ υ α υ α	180		10.0	187		180	2007	187	70,0		10.7		18.7	17.9	0,00
EWER D	TEMPERATURE	INF	12.8	12.7	12.6	12.7	12.9	13.1		13.2	13.1	13.4	13.5	15.9	13.5	13.7	13.9	14.1	13.9	13.0	14.2	14.2	14.0	14.5	14.3	14.3	14.2	14.5	15.1	- L		20.0		13.9	۵۷۵
JUNTY S Y-0027979		FLOW	6.838	6.974	6.612	6.370	6.612	7.127	5.600	6.717	5.544	5.913	6.444	6.003	5.925	5.349	5.475	5.072	4.825	5,219	5.024	5.466	5 343	5,399	5.781	5,444	4.995	5.017	4.274	4.631	4616	7 077	F	5.652	Monthly
NIAGARA COUNTY SEWER DISTRICT SPDES#NY-0027979		DATE	-	2	8	4	ro.	9 1	7	∞ (α	D .	2 7		12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
Ż		DAY	_	တ	S)	∑	-	≥ H	- 1	L U		0 2	≥ I	-	>	ı	ш	ဟ	တ	Σ	 -	3	F	L	S	S	Σ	-	3	F	L	S			

NIAGARA COUNTY SEWER DISTRICT #1

COMMENTS	COMMENTS																																	
F.COLI	/ 100 ml	3	, e				65		cr.	4				10	2	6	2 (*					171		1060	55000				3		77	2400	27.7	2151.4
DUAL	AVE,mq/I	0.91	0.80	0.76	0.54	0.63	0.72	0.59	0.59	0.60	0.57	0.47	0.50	0.45	0.47	0.52	0.02	0.45	5,00	0.03	0.27	0.24	0.27	0.24	0.31	0.36	0.22	0.15	0.54	0.48	0.35	0.30	0.91	
CHLORINE RESIDUAL	MAX,mg/I	0.96	1.08	0.94	0.70	0.66	0.76	0.66	0.70	0.70	0.66	0.50	0.52	0.56	0.48	0.63	0.58	0 55	20.0	00.0	0.30	0.29	0.34	0.26	0.50	0.38	0.26	0.18	0.59	0.50	0.40	0.44	1.08	
CHLOR	MIN,mg/I MAX,mg/I AVE,mg/I	0.84	0.64	0.63	0.40	0.56	0.67	0.49	0.51	0.52	0.47	0.42	0.49	0.38	0.45	0.36	0.41	0.34	30	120	2 6	0.0	0.21	0.22	0.18	0.35	0.18	0.10	0.50	0.45	0.28	0.10	0.10	
OROUS	EFF,mg/I	1.	0.24	0.23	0.41		0.24	0.28	0.48	0.35	0.38	0.43		0.34	0.40	0.33	0.38		0.35	0.31	- 6	0.30	7.0	0.34	0.40	0.44	0.67		0.60	0.49	0.44	0.49	0.37	17.2
PHOSPHO	5	2.67	1.22	1.70	3.04		2.23	2.02	2.51	1.66	3.60	3.32		2.67	5.46	8.54	3.84		5.39	3.32	7 45	2 60	0000	3.03	5.7.5	5.83	5.27		5.06	3.97	5.35	5.55	3.64	
	l	6.838	6.974	6.612	6.370	6.612	7.127	5.600	6.717	5.544	5.913	6.444	6.003	5.925	5.349	5.475	5.072	4.825	5.219	5.024	5.466	5 343	0.00	0.088 1704	0.701	0.444	4.985	2.017	4.274	4.631	4.616	4.944	5.652	
	DATE	-	2	8	4	Ω.	9	7	ω	တ	10	11	12	13	14	15	16	17	18	10	20	21	22	273	27	177	52	27	17	28	79	30	AVERAGE	
	DAY	LL	S	S	∑!	-	>	-	ഥ	ဟ	ഗ	Σ	F	8	-	Щ	တ	တ	Σ	<u> </u>	×	Ļ	Ц	_ (<i>U</i> .	O C	2	≥ F-	100	> -	- 1	Τ (S)		

FRANK A. NERONE

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 716-693-8759 FAX

FRANK A. Nerone, P.E. CERT, 4A

	OLIDS	EFF,mg/I	4.0	1.6	3.3		4.6	. K	o u	0.0	0 0	0.0	0.0	5.3	5.0	4.7	8.3	3.7	6.3	o r	2	0 7	4.0	4.5	3.5	4.3	2.6	2.6	5.0	3.6	3.8	3.6	18	12	3.2	7.0	4.4	167.1
9	SUSP SULIDS	INF,mg/I	100	144	80		136	7.6	180	007	0	707	4 5	132	128	128	232	96	112	120	21	400	00	116	124	\$	128	208	144	180	184	164	104	96	192	1	132.7	96.7%
ניס	00	EFF,mg/l				3.0	3.2	3.5	3.0	2			707	4.0	13.0	3.5	15.6				α C	2.5	0.	4.0	3.4					3.5	2.8	5.5					5.9	223.7
90	מטפט "	INF,mg/I				186.6	174.4	200.3	205.2				100 4	120.1	1.8.7	198.3	175.5				181.8	347.5	70.0	0.80	143.8					170.7	176.3	179.1					191.3	%6.96
OI IDS 1HB	בונילים ב	Err,mi/i	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	×0.1	<0.1	<0.1	- C V			<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0 ×	5	- 0	V0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	тах
SETT SOI	2 2	1/111, L	C	9	4	D.	9	5	5.5	5	4.5	4	7.5.5	3	0	ا ۵	7	5.5	7	5	T.	5	T.) (٥	0	4	0	9.5	9	7	6.5	14	9.5	7		14.0	тах
Hu	EEE MAY	-11	1.4	4.7	7.2	7.2	7.2	7.1	7.1	7.0	7.0	7.1	7.4	7.1	7.2	7.7	7.3	7.2	7.3	7.3	7.4	7.5	7.5	2.7	7.7	1.6	(.1	6.0	(.1	7.1	7.1	7.1	7.0	6.9	7.1		7.5	max
Ha	Z	\neg	1		0.7	7.0	7.2	7.0	6.9	6.8	7.0	6.7	7.2	7.1	7.0	1.0		(.1	7.1	7.1	7.4	7.4	7.4	7.2	7.0	0.0	0 0	0.8	1.7	6.9	7.0	9.9	6.9	6.7	6.8		6.7	min
Ha	INF MAX	75	0.1	1.1	4.7	7.7	7.4	7.3	7.3	7.2	7.1	7.3	7.4	7.3	7.2	7.7	5.7	7.7	6.3	7.3	7.4	7.5	7.5	7.2	7.2	7.7	7.7	1.	- 1	7.7	7.7	1.1	7.0	6.9	7.2		7.5	тах
hd	INF. MIN	7.1	7.4	1	1.0	1.0	۲.٦	6.9	6.9	6.8	7.0	6.7	7.1	7.0	7.0	7.7	- 0	500	6.0	6.9	7.3	7.2	7.3	7.0	6.9	8	0.0	0,0	0.0	0.0	0.0	0.0	9.9	6.7	6.8		6.6	mim
ATURE,C	EFF	19.6	180	70.7		0.00		18.5	18.8	18.9	19.5	19.7	19.5	19.2	19.1	187	70,0	1.0.7	6.0	19.8	20.5	20.5	20.8	20.9	21.5	214	21 12	27.7	20.7	20.7	20.0	20.7	20.5	20.5	18.5		6.81	ave.
TEMPERATURE	IN.	14.9	14.9	17.3	оп, Сп,	770	0 7	0.4.0	15.1	15.3	14.9	14.9	15.6	16.0	16.1	15.9	15.4	20.17	2.0.0	13.0	.16.1	16.0	16.0	17.4	17.3	16.3	17.0	17.6	17.5	47.4	- 4	20.0	10.9	71.7	0.7		10.0	ave.
	FLOW	4.139	5.431	3 645	4 067	4.30	1 187	1.10	4.107	4.300	5.533	4.567	4.761	4.675	3.831	4.841	4 018	4 519	2007	1.110	4.311	4.4/4	4.721	4.449	4.376	4.400	4.179	4.550	5 343	4.563	4 485	4 450	A 70B	Lac A	7.70+	1 540	1.010	WIGHTERIN
	DATE	~	2	6	4	rc.	0	0 1	- 0	0 0	ָר אָר	2	11	12	13	14	15	16	17	107	0,7	D C	27	21	22	23	24	25	26	27	28	29	30	31		AVERAGE		
	DAY	S	Σ	H	3	-	LL	. U	0	0 2	≦ ⊦		> F			ഗ	S	Σ	F	1//	\$ -	- 1	L ('n	တ	Σ	<u> </u>	3	 - -	LL	တ	S	Σ	 -				

NIAGARA COUNTY SEWER DISTRICT #1 Jul-01

·	CIMINICIO											Total Control																			and the second s				
F.COLI	/ 100 ml				8	,	.33) m				ď		AR	2 0	2						16	4						33	0 (7	,			4.8	12.0
IDUAL	MIN,mg/I MAX,mg/I AVE,mg/I	0.61	44.0	0.53	0.75	0.87	0.95	0.97	06.0	0.29	0.77	0.82	1.07	0 92	0.78	50.0	0.00	0.02	0.13	0.00	0.60	0.53	0.72	0.40	0.35	0.33	0.22	0.23	0.59	0.54	0.58	0.51	10.0	1.07	
CHLORINE RESIDUAL	MAX,mg/I	0.63	0.58	0.88	0.84	0.94	1.03	0.99	0.93	0.98	0.87	0.95	1.11	1.36	0 96	0.63	0.52	0.53	0.00	2.0	0.61	0.66	1.04	0.49	0.54	0.37	0.28	0.29	0.68	0.57	0.72	0.61	0.60	1.36	
CHLOR	MIN,mg/I	0.59	0.32	0.28	0.64	0.79	0.90	0.94	0.85	0.66	0.58	0.69	1.04	0.47	0.67	0.56	0.60	0.45	2 2 2	0 0	0.08	0.42	0.55	0.34	0.24	0.25	0.14	0.17	0.43	0.51	0.49	0.36	0.48	0.14	
OROUS	EFF,mg/I	0.47	0.48		0.64	0.73	0.91	0.92	0.82	0.71		0.52	0.56	0.52	0.50	0.65	0.82		0.84	0.74	0000	0.00	76.0	0.52	0.44		0.48	0.45	0.45	0.56	0.60	0.61		0.62	23.4
PHOSPH	1/6	2.96	4.25		3.24	3.20	3.24	3.32	2.79	2.88		3.28	4.62	3.60	3.60	4.98	3.97		3.32	3.65	25.0	O. 10	2.00	0.10	7.67		4.13	4.37	3.48	9.51	4.41	28.90		4.85	
	FLOW	4.139	5.431	3.645	4.967	4.430	4.167	4.167	4.300	5.533	4.567	4.761	4.675	3.831	4.841	4.018	4.519	4.446	4.311	4 474	4 721	7770	A 27E	0/0/7	4.400	4.1/9	4.550	5.343	4.563	4.485	4.459	4.706	5.284	4.540	
	DATE	-	2	m	4	ιΩ	9	7	8	6	10	11	12	13	14	15	16	17	18	19	20	23	22	23	27	74	67	07	17.	28	29	30	31	AVERAGE	
	DAY	s);	ΣΙ	-	8	-	Щ	တ	တ	∑	-	>	-	L.	တ	S	Σ	⊢	>	F	止	S	V.	2	<u> </u>	- 1/1	3 -	-	L 0	מ	ומ	≥ 1	H		

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Aug-01

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

SOLIDS	EFF,mq/I)	6.6	1.8	2.8	2.4	3.6	3.0	7.0	3.4	2.0	12	12	3.2	2.2		3.8	1.0	7.0	2,0	144	0.0	2.5	2.0	3.6	2.2	2.0	0.8	14	1.2		2.8	C	2.3
SUSP S	INF,mg/I		316	156	132	162	196	200	104	152	98	312	28	264	196		216	106	200	236	252	232	276	216	440	205	252	204	164	352		212	2000	270.0
20	EFF,mg/I	2.1	2.8	1.7	2.7				3.7	15	2.1	9.1				O.	1.2	2.4	- 6	2			43	4.3	2.0	4.2				3.0	3.4	5.4	40	٠. ٠
CBOD	INF,mg/I	163.1	145.6	. 155.5	132.7				138.6	131.0	169.2	176.8				150.7	149.6	1411	144.1				211.6	158.5	232.8	247.8				236.4	190.6	169.4	160.0	0.80
SOLIDS,1HR	EFF,ml/I	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	00	0
SETT SOL	INF,mI/I	10	18	10	5	8	9	11	7	4.5	7	9.5	9.5	10	7	6.5	80	o,	7	7	7	တ	12	12	19	6	17.5	11	10.5	23	20	10	23.0	60.0
	EFF, MAX	7.2	7.1	7.1	6.9	7.0	7.0	7.2	7.2	6.9	7.0	7.0	6.8	6.8	7.0	7.0	7.1	7.1	7.0	7.1	6.9	7.1	7.0	6.9	7.1	6.9	7.0	6.9	6.9	7.0	7.3	6.8	7.3	2
hД	MIN	6.6	6.9	7.1	6.8	6.9	6.9	6.2	6.9	6.9	6.7	6.9	6.7	6.7	6.8	6.8	6.9	6.9	6.9	6.7	6.8	6.9	6.8	6.8	6.7	6.8	6.7	6.7	6.7	6.7	6.8	6.7	6.2	
Hd	INF, MAX	7.2	7.3	7.3	7.1	7.3	7.1	7.6	7.2	7.3	7.2	7.2	7.0	8.0	7.2	7.6	7.3	7.3	7.2	7.2	7.4	7.3	7.4	7.4	7.5	7.0	7.4	7.3	7.1	7.2	7.3	6.9	8.0	
Н	INF, MIN	6.6	6.9	7.0	6.8	6.9	6.9	6.2	6.8	6.9	6.7	6.9	6.7	6.7	6.8	6.8	6.9	6.9	6.9	6.7	6.8	6.9	6.8	6.8	6.7	6.7	6.7	6.7	6.6	6.6	6.6	6.7	6.2	
ALUKE,C	FFF	21.5	21.3	21.6	21.7	21.3	21.3	22.0	21.2	20.4	21.1	19.4	20.7	20.7	20.9	20.8	20.7	21.3	21.2	21.8	21.3	21.7	21.2	21.8	21.5	21.7	21.8	21.7	21.4	22.0	21.6	22.5	21.3	
ILIVIPERALURE	- L	11.1	17.5	16.9	18.2	16.9	16.7	17.3	17.8	18.0	18.0	1/./	16.9	1/./	17.5	17.2	17.9	18.0	17.4	17.1	17.9	17.9	17.7	17.7	18.2	4.0	78.7	18.0	18.3	18.4	18.9	0.0	17.8	9.60
1	TLOW	4.911	5.044	4.052	3.872	3.775	3.882	4.039	5.284	4.232	3.55/	3.847	4.050	3.844	4.016	3.908	3.977	3.80/	3.678	4.294	4.526	4.067	3.917	4.335	3.787	3.320	0.778	0.048	3.6/5	3.868	400.0	4.639	4.047	Monthly
TAAT	מאוני	- 0	7,0	0	4 1	0	0 1		ω (5	2 7	- 0	72	3 5	7 - 7	0,	10	- (α	J.G	07	17	77	23	74	22	27	77	200	SZ	24	9	AVERAGE	
> ٧ ८	X	≥ F	_ _	LO	0 0	פוס	≅∣⊦	-	≥ +	- L	LO	0 0	2	ž F	14/	S F	-		ממ	מ	≥ ⊦	-	≥ F	- L	L	o U	2	<u> </u>	- 1	> -	- ц	-		

NIAGARA COUNTY SEWER DISTRICT #1 Aug-01

COMMENTS	COMMINICATION																	- Company of the Comp																	
F.COLI	/ 100 ml	15		3	000				c	2	8.) r:				8)	c	2 (7	0						က	30				3200		123	10.0	66.0
DUAL	AVE,mg/l	0.52	0.28	0.19	0.36	0.21	0.20	0.79	0.73	0.72	0.59	0.48	0.24	0.26	0.38	0.60	0 98	0.50	0.77	0.70	0.78	0.03	0.20	0.24	0.18	0.57	0.29	0.40	0.92	0.59	0.23	0.15	0.16	0.98	
CHLORINE RESIDUAL	MAX,mg/I		0.33	0.30	0.40	0.31	0.25	0.96	0.87	0.78	0.64	0.53	0.27	0.35	0.43	0.87	66.0	06:0	0.89	08.0	0.03	3.0	0.20	0.26	0.26	0.94	0.30	0.75	1.36	0.96	0.27	0.20	0.25	1.36	
CHLOF	MIN,mg/I		0.19	0.11	0.31	0.14	0.16	0.59	0.65	0.65	0.53	0.42	0.21	0.12	0.29	0.13	0.97	0.23	0.65	0.65	30.0	3,50	4.0	0.22	0.12	0.09	0.28	0.20	0.65	0.39	0.18	0.09	0.10	0.06	
OROUS	EFF,mg/I	0.55	0.47	0.41	0.45	0.48	0.62		0.44	0.32	0.34	0.27	0.31	0.27		0.35	0.29	0.28	0.33	0.34	0.33	3	77	0.41	0.41	0.43	0.45	0.41	0.36		0.24	0.20	0.21	0.37	12.6
PHOSPHO	_	6.04	7.81	14.82	10.24	6.44	5.35		5.39	3.65	4.86	5.67	7.29	17.44		7.04	5.99	2.31	4.13	6.07	4 49)	5 62	30.02	27.0	4.59	4.84	10.70	20.05		10.60	8.74	3.88	6.78	
	I	4.911	5.044	4.052	3.872	3.716	3.882	4.039	5.284	4.232	3.557	3.947	4.050	3.944	4.016	3.908	3.977	3.867	3.678	4.294	4.526	4.067	3 017	1.00	4.333	3.707	0.020	0,778	0.01	3.6/5	3.868	3.504	4.259	4.047	
	DATE	ν-	2	က	4	2	မ	7	80	6	10	11	12	13	14	15	16	17	18	19	20	21	22	1 2	27	25	300	27	700	87	29	300	31	AVERAGE	
	DAY	8	F	4	Ø	တ	≥	ı-	3		L	တ	တ	∑	 -	3	-	ш	ဟ	ഗ	Σ	ļ.—	3	-	- ப	_ cr.	O	2	- H	-	S F	- L			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Sep-01

7346 LIBERTY DRIVE	NIAGARA FALLS, NEW YORK
--------------------	-------------------------

FRANK A. Nerone, P.E.	CERT, 4A
716-693-0001	716-693-8759 FAX
DRIVE	S,NEW YORK

OLIDS	EFF.ma/I	, C	0.0	7	+ 0	2.0	٦. ۵	2.4	2.0	5.8	0.8		1.1		2.0	1.2	0.8	0.4	0.8	0.6		0.4	0.0	800	0.7	0.0	2.6	i	1.6	12	2.0	1.6		t.
SUSP SOLIDS	INF.ma/I	4—	280	200	250	727	780	208	248	276	232	200	268		372	344	276	216	252	128		168	276	184	144	232	492		292	180	172	236		250.6
60	EFF,mg/I	6.1				7 8	4 6	K.1.3	2.4	3.3				3.2	3.6	3.6	1.8				3.2	2.5	2.1	2.3				6.4	3.8	2.5	2.4			4.6
CBOD	INF,mg/I	366.8				100 0	170 E	0.50	2/8.4	240.5				210.4	257.9	182.3	283.9				221.3	211.5	171.2	230.7				220.1	281.2	128.7	171.5		0 100	227.0
SOLIDS,1HR	EFF,ml/I	<0.1	<0.1	<0.1	207	, C		.0.	- 0	- NO.1	V0.1	- 0	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	c	0.0
SETT SO	INF,m[/]	18	15.0	15.0	180	18.5	19.0	20.00	20.00	40.0	20.0	0.00	24.0	24.0	72.0	29.0	25.0	23.0	15.0	23.0	22.0	24.0	21.0	19.0	28.0	24.0	18.0	18.0	20.0	17.0	16.0	20.0	0.00	23.U
	EFF, MAX	7.1	7.4	7.1	7.2	7.2	7.1	7.1	7.4	7.4	7.4	1.7	7.0	7.1	7.0	, c	9.0	9.0	6.8	6.6	7.0	7.1	7.1	7.1	7.0	7.0	7.1	7.3	7.1	7.1	6.9	6.9	1/2	ţ.
	Z	6.9	6.9	6.7	6.6	6.9	7.0	6.7	0.9	7.0	0.00	0 9	0 0	0.0	- 0	0.0	0.0	0.0	0.7	6.5	6.6	6.9	7.0	6.8	6.9	6.8	6.8	7.0	7.0	6.8	8.9	6.8	5.5	? .
НД	INF, MAX	(.5	7.1	7.3	7.3	7.4	7.3	7.2	7.2	7.2	7.1	7.0	7.1	7.4	7.2	7.4	- 0	10.0	7.0		7.1	6.7	7.4	7.3	7.7	7.3	7.3	7.2	7.3	[:]	1.1	7.7	7.5	2
nd Fig.	INT, WIIN	۲.)	7.0	6.9	7.1	7.1	7.1	7.1	7.2	6.9	6.8	6.9	0.00	0.00	7.0	7.1	- 0	0.0	0.7		500	0.0	7.7	7.1	7.1	7.2	1.7	(.1	1.1	1.0	7.0	0.)	6.7	i.
יו סור	7 7 7	7.12	21.2	21.0	21.9	21.8	21.2	21.6	22.6	22.6	22.3	22.5	22.2	21.8	20.8	213	20.5	20.02	24.0	0.10	0.70	0.17	0.17	70.7	20.0	20.3	4.07	20.00	19.0	0.60	20.1	40.1	21.2	ave
יאם יאיז וווידי	47 p	0.7	0.71	17.6	17.7	17.9	18.3	18.1	17.8	18.3	18.5	18.1	18.4	18.7	18.3	18.1	18.2	184	18.6	7 2 2	727	- 07	10.4	18.7	10.7	0.6.	τ α	20.0	ο. α α	10.0	17.7	+	18.2	ave.
EI OW	4 200	7.200	4.200	4.218	4.324	4.154	4.154	4.429	4.225	3.924	3.927	4.239	4.239	4.089	3.924	3.600	3.850	3.724	3.825	3 469	3 621	4.417	4010	4.007	2002	4 567	5.650	7.050	6.438	4 692	4 333	200	4.318	Monthly
DATE	1 -	- 0	7 0	0	4	5	Q.	7	8	တ	10	-	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
DAY	S	U.	ρĮΣ	≥ ⊦	- 3	≥ F	- 1	1	S	S	≥	-	A	⊢	Щ	S	တ	∑	 -	8	 	LL	S	S	Σ	-	M	-	Ш	S	S			

FRANK A. NERONE

NIAGARA COUNTY SEWER DISTRICT #1 Sep-01

CONMACTION	COMMENIA			The state of the s																															
FCOL	/ 100 ml	540				8		α) (;				ď		99	20.50	7100				က		ε.) (r				rt	2	с.	0 (1	0		10.5	74.5
IDITAL	AVE,mg/I	0.26	0.54	0.63	0.37	0.45	0.88	0.49	0.55	0.60	0.35	0.50	0.43	0.27	0.27	0000	0.29	0.02	0.25	1.05	0.51	0.60	0.61	0.62	0.57	0.59	0.64	0.46	0.51	0.56	0.61	070	0,1	1.05	
CHLORINE RESIDITAL	MAX,mg/I	0.34	0.58	0.79	0.43	0.92	1.12	0.65	0.66	0.67	0.57	0.55	0.50	0.68	0.45	0.77	0.47	0.00	0.52	1.32	0.53	0.65	0.76	0.68	0.60	0.70	0.98	0.54	0.68	0.65	0.67	0.51	3	1.32	
CHLO	MIN,mg/I	0.21	0.52	0.52	0.32	0.00	0.72	0.36	0.39	0.53	0.05	0.46	0.35	0.06	0.15	0.19	2.5	5.0	0.00	0.79	0.49	0.50	0.52	0.58	0.53	0.50	0.33	0.35	0.25	0.44	0.52	0.47		0.00	
OROUS	山	0.21	0.20	0.24		0.38	0.43	0.39	0.44	0.41	0.44		0.42	0.46	0.35	0.31	0.34	+0.0	0.20	100	0.25	0.23	0.24	0.33	0.40	0.35		0.31	0.28	0.19	0.23	0.28		0.32	11.4
PHOSPH(INF,mg/I	7.65	4.29	4.45		5.50	6.08	6.16	6.16	4.57	3.44		1.29	7.24	6.07	5.83	4 86	B 03	0.03	C	5.30	4.53	3.56	6.32	4.57	4.78		4.90	0.57	3.77	1.22	3.73		4.55	
	FLOW	4.200	4.200	4.218	4.324	4.154	4.154	4.429	4.225	3.924	3.927	4.239	4.239	4.089	3.924	3.600	3.850	107.5	2 80E	0.00	0.408	3.621	4.417	4.019	4.007	3.203	4.567	5.650	7.459	6.850	4.692	4.333		4.318	
	DATE	ν-	2	ဗ	4	5	9	7	8	O	19	1	12	13	14	15	16	17	- 82	10	0 0	77	21	22	23	24	25	26	27	28	29	30		AVERAGE	
	DAY	တ	ഗ	Σ	F	3		Щ	S	တ ြ	∑ E		8		L	ဟ	တ	Σ	-	M	: -	-	1-	S	S	Z I	-	M	-	1 (y) (1)	S			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Oct-01

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 716-693-8759 FAX

FRANK A. Nerone, P.E. CERT. 4A

סמו זסמ	SOLIDS	EFF,mg/I	0.	2.4		2.3	2.2	5.8	3.8	0.2	0.7	1.6	2.2	. 1.0	4.0	3.6	4.0	3.2	1	28	20	2.0	1.8	200	1.0	2.2	1.4	1.2	2.0	1.8	1,8	1.4			4.4
CIICD	, yene	INF,mg/I	184	244		180	224	432	292	88	152	184	268	164	136	152	148	156		56	112	80	104	220	136	188	140	92	116	188	120	108		0 007	183.0
CROD	רבי בייו	EFF, mg/I			0	27.8	2.9	14.6				1.5	2.1	1.7	3.0				3.7	16	2.4	0.9				2.9	2.8	2.7	1.5				14.0	C LI	208 4
S	INIC	I/BIII; LINII			0 017	1/3.2	1/4.4	170.9			'	167.7	197.2	142.9	156.8				132.6	92.8	108.0	116.4				147.1	121.2	105.5	124.6				106.9	144.0	96 0%
SOLIDS 1HR	FEE 31/1			- 7	- 7		V0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0	max
SETT SOI	. =	12.00	75.00	12.00	12.00	200	10.00	15.50	9.00	10.50	16.00	6.50	10.50	6.00	5.00	4.50	4.00	4.50	4.00	4.00	4.00	5.00	4.00	4.00	3.50	6.00	5.00	3.00	5.00	4.00	4.00	4.00	4.50	16.0	max
Ha	FFF MAX	i «	7.4	7.7	1.7	7.7	7.7	0.0	9.0	9.8	7.1	7.1	7.2	7.1	7.1	7.1	7.0	7.0	7.0	7.1	7.2	7.1	7.1	7.1	7.2	7.0	7.1	7.0	7.2	7.0	7.1	7.1	7.2	7.4	max
Hd	EFF. MIN	6.7	9	0.0	7.0	7.2	7. 0	0.0	5 0	0.0	6.9	6.9	7.1	0.7	9.9	7.1	6.9	6.9	7.0	7.0	7.0	6.9	7.0	6.9	6.8	6.8	6.9	9.0	0.)	6.9	6.9	6.9	6.9	6.7	min
Hd	INF. MAX	7.1	7.3	7.0	7.4	7.7	7.2	7.7	C. /	1.4	7.3	1.4	4.7	5.7	5.7	7.7	c.)	7.4	7.5	7.5	7.4	7.4	7.3	7.3	7.6	7.3	1.3	4.7	7.4	7.3	(.3	۲.3	7.4	7.7	тах
Hd	INF, MIN	6.9	6.8	6.9	7.3	7.1	7.1	7.1	7.2	7.4	1	s; L	7.7	0.7	7.7	7.7	5.7	7.7	7.0	7.4	7.3	7.3	7.7	7.7	7.0	5.7	5.7	5.7	5.7	7.5	5.7	7.,	7.1	6.8	min
ATURE,C	EFF	20.2	20.7	20.4	20.7	202	18.8	184	τ α τ	18.5	70.0	0.8.0	20.3	20.1	24.0	40.0	0.0	7.81	18.3	18.0	18.5	19.5	0.0	19.4	19.6	9.0	13.7	6.7.		7 0.0			18.5	19.3	ave.
TEMPERATURE	INF	17.8	18.0	18.5	18.3	18.3	17.4	17.6	17.3	17.4	47.7	17.7	17.0	17.7	17E	77.7	7.5	11.0	17.4	17.1	47.4	17.7	17.5	0.71	17.4	17.1	- α	16.0	20.04	10.4	18.7	70.0		17.4	ave.
	FLOW	4.393	4.505	4.286	4.096	5.818	15.901	7.935	6.150	5 381	5 330	5 196	4 937	4 767	4 834	5 624	F 178	0.4.0	0.300	0.402	7.0.0	4.000	5.140	7.201	5.303	6.77B	8 168	5 620	5 383	4 080	4 858	/ 50g	600.	5.865	Monthly
	DATE	_	2	3.	4	3	9	7	8	0	40	1	12	13	14	15	18	17	- 07	2 0	200	27	22	22	27	25	26	27	28	29	30	34		AVERAGE	
	DAY	Σ	⊢	≯	⊢	ഥ	S	တ	Σ	-	>	-	L	ဟ	ဟ	Σ	-	M	: -	- ш	. U.	v.	Σ	-	>		IL	S	S	≥		3			

NIAGARA COUNTY SEWER DISTRICT #1

CHINDRANGO	COMMENTS														The state of the s																					
FCOLI	/ 100 ml			C.	p	c,) (r.)			m		8	m				,	3		3	3				3		c	m.				2800	2000	5.2	13.6
DIJAI	AVE.ma/I	0.83	1 09	0.94	0.89	0.70	0.93	0.77	0.80	0.23	105	0.84	0.80	0.75	0.45	0.0	0.47	700	20.0	1.02	0.75	0.91	1.03	0.82	0.75	0.39	0.63	0.27	0.86	0.80	0.92	0.39	0.24	7.0	1.09	
CHLORINE RESIDITAL	MAX,ma/I AVE.ma/I	1.48	1.14	1.03	1.06	0.99	1.12	0.78	0.95	0.81	1.15	0.99	0.94	0.82	0.77	0.29	1 23	2007	1.00	1.27	0.94	1.00	1.18	1.05	0.80	0.90	0.73	0.55	0.94	0.83	1.06	0.54	0.22	77.0	1.48	
CHLOF	MIN,mg/I		0.99	0.81	0.72	0.50	0.72	0.75	0.71	0.76	0.96	0.60	0.72	0.62	0.24	0.06	0.00	0.73	0.73	00.0	0.58	0.78	0.91	0.58	0.67	0.00	0.57	0.00	0.80	0.78	0.81	0.24	0.20		0.00	
OROUS	EFF,mg/I	0.35		0.41	0.24	0.54	0.34	0.15		0.18	0.25	0.28	0.30	0.39	0.44	0.53		0.84	0.0		0.49	0.42	0.44	0.43		0.41	0.43	0.33	0.33	0.35	0.36		0.36		0.38	18.9
PHOSPH	INF,mg/I	4.29		3.85	2.99	1.58	8.46	2.34		2.22	6.60	16.60	4.65	3.40	3.52	4.09		2.83	202	7 1 0	7.3	6.79	3.32	5.67		4.09	2.71	2.63	2.19	3.97	3.28		2.88		4.25	
	FLOW	4.393	4.505	4.286	4.096	5.818	15.901	7.935	6.150	5.381	5.339	5.196	4.937	4.767	4.834	5.624	5.476	8.560	6.482	T 611	7.000	4.000	5.148	2.25/	5.363	5.713	6.5/8	8.168	5.620	5.383	4.960	4.858	4.596		5.865	
	DATE	~	2	က	4	22	9	7	8	6	10	11	12	13	14	15	16	17	18	10	200	24	7 2	77	23	24	67	56	27	28	29	30	31		AVERAGE	
	DAY	Σ	F	≥	-	ш	တ	တ	Σ	-	≫	 	Щ	S)	တ	Σ	⊢	>	F	L	. U.	0	0 2	5 }		} r	-	L 0	S) (0	n :	Σ	-	8			

Y SEWER DISTRICT #1	Nov-04
NIAGARA COUNTY SEWE	SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	
--	--

							~,-				_,													1	1				_	,	· T	-,		- 	-1	_
Э. С.	ממו וסמ	OLIDS FFF Lan	Err,mg/I	9.0	2	1.6	J. 0	7.	ρ. Ο Ο	2, Z	0 0	2.0	40	2,0	7. a 0	0.0	7	2. 4	ţ.	Σ.	1.6	0.6	1.6	1.4	3.0	1.4	1.2	1.2	2.0	12		0.6	4.0		1.6	73.7
Nerone, P.	CIICD C	רן קי		477	132	148	120	132	401	180	0.70	188 188	224	180	800	202	124	130	132	200	760	220	284	104	344	116	112	168	96	8		98	92		157.4	99.0%
FRANK A. Nerone, P.E. CERT, 4A	מ	EEE ma/I	1/B/11/B/1	0,0	2.0	4.1				2.1	i	0,10	ò			0		0.40	0.70	0.0				6.0	2.5	2.2	2.6				3.2	3.5	5.9		3.7	173.7
FAX	CROB	INE mg/l	1700 -	1186	10.0	100.4			476 J	1787	156 R	238.5				156.9	137.5	150.0	457.0	9.70				152.8	305.2	146.9	141.1				94.7	112.4	56.2		144.0	97.4%
716-693-0001 716-693-8759 FAX	SOI IDS 1HR	FFF ml/I	1		5, 5	7	7.0.			0 0	<0.1	<0.1	<0.1	×0.4	×0.1	×0.4	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	×0.1	5			<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0,0	тах
	SETT SOI	INF HVI	45	S C	7.0	7.0	, r	0 0	77.0	7.5	10.0	13.0	14.0	14.0	10.0	110	80	80	0 9	0.0	2.0.7	0.10	8.0	6.0	9.0	4.0	5.0	4.0	3.0	3.0	4.5	5.0	1.4		14.0	max
N YORK	Ha	X	7.0	7.0	7.1	7.1	7.2	7.7	7.2	7.0	7.0	7.0	7.0	7.0	7.1	7.1	7.2	7.2	7.3	7.7	7.7	0.7	(.1	6.9	7.2	6.9	6.9	6.9	6.9	7.2	7.2	7.2	7.2		7.3	max
7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	Ha	Z	_	6.8	6.9	2 0	6.2	5 9	0.00	6.8	7.0	6.9	6.9	6.8	6.8	7.0	7.0	6.9	7.0	9 9	0 0	9.0	0.0	6.8	6.8	6.6	6.8	6.9	6.8	6.5	7.1	7.1	7.0		6.5	шiп
7346 LIBEI NIAGARA I	Hd	INF, MAX	7.3	7.3	7.3	7.3	7.2	7.2	6.9	7.2	7.4	7.1	7.1	7.1	7.5	7.5	7.3	7.6	7.4	7.3	7.1	7.7	0.7	6.3	6.9	6.6	D. C.	7.0	7.0	7.5	7.3	7.4	7.3		7.6	max
	Hd	INF, MIN	7.2	7.0	7.0	7.1	8.8	6.8	6.8	6.9	6.9	7.1	7.0	7.0	6.9	7.2	7.2	7.3	7.2	6.8	88	2.0	10.7	7.0	0.0	D 0	0.0	0.7	6.9	6.4	7.3	7.3	7.2		6.4	min
ISTRICT Nov-01	TURE,C	出	18.5	18.7	19.1	19.4	18.0	18.1	18.5	19.1	18.8	19.1	18.4	18.1	18.0	18.4	19.1	18.9	17.6	16.6	16.5	Z W	20.0	4.0.	0.0	7 0.0 0.0	0.0	7.01	15.6	17.3	17.7		15.5		17.5	ave.
EWER D	TEMPERATURE,	ΗNI	16.8	17.0	16.7	16.4	16.4	16.3	16.3	16.4	16.2	16.3	15.7	15.8	16.2	16.2	15.8	16.1	16.0	15.5	15.7	15.7	ָ ה מ	0.0 n	20.0	1.0.T	7.0.4	70.7	15.7	13.4	15.5	14.8	14.3		15.8	ave.
SUNTY S Y-0027979		FLOW	4.612	4.642	4.234	4.694	4.841	4.542	4.678	4.686	4.969	4.781	4.616	4.615	4.435	4.495	4.980	4.416	4.519	3.889	4.765	5.056	5 722	7 300	7307	4 400	A A A C A A	0.002	0.1.0	0.000	0.787	9.824	13.223		7320	Monthly
NIAGARA COUNTY SEWER DISTRICT #7 SPDES # NY-0027979		DATE	-	2	3	4	5	9	7	ω	6	10	11	12	13	14	15	16	17	18	19	20	24	22	23	24	25	3 6	27	200	200	82	200	77.10	AVERAGE	
Ž		DAY	-	LL.	တ	ဟ	Σ	-	×	-	1	S) C	<i>y</i>	[≥	-	>	- 1	_	S	တ	Σ	<u> </u>	>	: -	Ш	S	o.	2	<u> </u>	10/	} -	- L	L-			

NIAGARA COUNTY SEWER DISTRICT #1

COMMENTS																																	
F.COLI	/ 100 ml		6.	1				6)	0	2 (4				2	2	,		2				43		8	က				3933		11	7.6
DUAL	AVE,mg/I	0.73	0.93	0.47	0 30	0.00	0.17	0.01	0.75	0.07	2.0 R	100	200	1 23	1 28	5.7	1.13	7.70	1.63	1.34	0.71	0.17	0.29	0.44	0.54	1.42	0.51	0.69	0.25	0.22	0.84	0.68	1.42
CHLORINE RESIDUAL	MAX,mg/I	1.23	1.14	0.68	0.56	0.84	0.70	0 92	0.84	120	1 12	1 40	1.27	1.57	141	1 20	1.50	20.7	00.7	40.5	1.30	0.23	0.44	0.84	1.22	1.52	0.87	0.95	0.36	0.26	1.08	1.12	1.57
CHLOR	MIN,mg/I MAX,mg/I AVE,mg/	0.08	0.73	0.24	0.16	0.66	0.65	0.77	0.61	0.71	0.80	0.85	0.93	100	127	100	3.5	1 17	00.	0.20	0.30	7.0	0.14	0.15	0.18	1.35	0.25	0.46	0.20	0.19	0.70	0.45	0.08
	1/6	<u> </u>	0.32	0.35		0.42	0.34	0.52	0.50	0.44	0.49	0.53	0.35			0.45	0.41	0.40	0 70	08.0	0.0	000	0.30	0.30	0.40	0.00	0.48	0.37		0.38	0.30	0.30	0.40
Ϊŀ	INF,mg/I		3.77	4.25		3.84	3.88	5.50	3.96	4.73	4.09	5.91	6.48			377	4.09	5.95	10.77	41.10	2	000	10.44	1.0.	3.01	0,00	0.0	3.40		3.24	2.31	2.02	5.43
+		4.612				4.841	4.542	4.678	4.686	4.969	4.781	4.616	4.615	4.435	4.495	4.980	4.416	4.519	3.889	4 765	5.056	5 722	5 300	0.000	4.034	A A A A	0.00 8 446	00	0.300	6.291	9.854	13.223	5.367
1	DAIE	-	2	က	4	2	9	7	80	6	10	11	12	13	14	15	16	17	18	19	20	2	22	22	24	25	3,0	276	200	07	87	30	AVERAGE
> 0	LAY	-	_	y)	ഗ	Σ	Н	≥	⊢	ш	တ	တ	≥	 -	≥	<u></u>	ш	S	S	Σ	 -	8	-	. [1	S	S	Z	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	} -	- L	L	

FRANK A. NERONE

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Dec-01

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-8759 FAX CERT. 4A

SUI IOS dSI IS	E ma/l INE ma/l			-	+	-	-	200	108	5.0 7.5	000	-	$\frac{1}{1}$	- 1	7)	108	112	-	184 3.1	90	36		96		204	240 1.1	80		-	788	787	+		-
CROD	INF ma/l	-	1.			1316	1733	400.4	100.1	103.0			7000	170.0	70.0	00.0	9.				86.4	63.1	67.6	62.9				80.9	88.3	63.8	73.0			
SOLIDS.1HR	EFF.ml/I	<0 1	\$ 0.1	\$ V	×0.1	<0.1	V V				20.7	5 0	5 0	- 5	- 7	70.	0,0	- N	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	×0.1	<0.1	<0.1	<0.1	×0.1	<0.1	<0.1	7	 ?
SETT SC		2.00	1.30	3.00	2.00	4.00	7.50	4 00	00.6	3.00	3.50	12.00	800	4 00	20.5	200	20.00	20.7	0.00	2.00	2.00	3.00	3.00	2.00	5.00	2.00	2.00	2.50	3.50	2.00	2.50	7.50	1 50	3.
Hd	出	7.2	7.1	7.2	7.3	7.4	7.3	7.3	7.0	7.1	7.1	7.2	7.1	7.3	7.3	7.2	7.1	7.7	7.7		1.1	7.0	6.9	6.9	7.0	6.9	7.0	7.0	6.9	6.8	7.0	7.1	7.1	
ЬH	EFF, MIN	7.1	7.0	7.1	7.0	7.0	6.8	6.8	6.9	6.9	6.8	7.0	6.8	7.2	7.1	7.1	8 9	0 0	10.0	1 0	0.7	6.7	6.8	6.9	6.8	6.9	6.9	6.8	6.9	6.7	6.9	6.9	6.9	
Hd	INF, MAX	7.4	7.3	7.4	7.2	7.4	7.4	7.6	7.2	7.3	7.3	7.3	7.4	7.5	7.5	7.5	7.4	7.3	7.3	5.7	- 7	7.7	0.0	6.0	7.0	7.3	7.0	7.4	6.9	7.3	7.0	7.2	7.2	
bН	INF, MIN	7.1	7.2	6.7	7.1	7.2	7.2	7.2	6.8	7.0	7.1	7.0	6.6	7.2	7.3	7.3	7.3	7.0	9.9	2.0	0.0	0 0	0.0	0.7	6.8	6.8	0.7	6.9	6.8	6.7	6.8	7.0	7.0	
ATURE,C	EFF	15.3	15.7	16.1	16.1	17.2	16.7	16.4	16.1	16.3	15.9	16.9	16.7	17.0	17.0	15.8	14.5	14.4	13.6	137	170	7.50	20.00	13.0	13.6	13.4	12./	12.5	12.3	12.4	Ni.	~ ∏	11.4	
TEMPERATURE	HN.	14.4	14.4	14.9	14.9	14.8	15.1	14.9	14.5	14.5	14.5	15.0	14.7	14.9	14.9	13.5	13.4	13.6	13.1	13.4	13.3	12.5	5.00	5.00	13.3	13.2	13.2	13.1	13.0		12.9	12.9	12.7	_
7	FLOW	10.065	7.786	9.665	5.889	4.975	5.720	4.847	8.426	4.571	7.857	4.770	4.358	4.803	5.492	9.874	8.280	13.898	14.157	10.673	9.073	0 990	6 194	0.00	7.0014	7.452	200	0.083	7.488	7.022	0.741	0.520	0.583	
	DATE	-	2	5	4	ç	9	7	8	6	19	11	12	13	14	15	16	17	18	19	20	21	22	23	27	25	27	20	17	220	200	24	0	
	DAY	מ	n :	≅ŀ	- 1	S F	_	LL	တ	တ	Σŀ	-	S	-	1	တ	Ø	≥	⊢	≥	 	L	S	v.	2	<u> </u>	1	\$ F	- ⊔	LU	ט	2 2	101	

COMMENTS	COMMENT		, , , , , , , , , , , , , , , , , , , ,		and the state of t																							The state of the s							The state of the s
F.COLI	/ 100 ml	9				ď		780	5 0)			е.)	ď	2 (1	P			6	2	C	3 0	0			ď)	ď	2 "				4.9	24.3
DUAL	AVE,mg/I	0.76	0.94	0 88	0.94	0.0	0.72	0.22	0 70	101	0.84	0.76	1.02	0.46	1 04	0.65	0.68	0.51	2.0	1 13	1 27	1.2.1	4.07	3.5	- t	0.77	1 17	0.82	0.02	0.82	0.68	0.33	3.0	1.31	
CHLORINE RESIDUAL	MAX,mg/I	0.82	1.21	1.30	105	1 20	0.93	0.24	1.06	1.05	0.92	0.81	1.32	0.69	141	0.75	0.82	0.75	0.13	1.55	7 20	δ, τ	7 23	4 A8	134	0.87	1.30	0.97	0.95	66.0	0.71	0.44	5	1.55	
CHLOF	MIN,mg/I MAX,mg/I AVE,mg/I	0.69	0.61	0.65	0.85	0.79	0.43	0.21	0.15	0.98	0.77	0.70	0.81	0.10	0.78	0.51	0.60	0.28	0.56	0.77	2	0.60	0.25	1.18	105	0.64	1.10	0.72	0.80	0.73	0.66	0.18	5	0.10	
OROUS	EFF,mg/I	0.25	0.15	0.24		0.26	0.40	0.38	0.34	0.36	0.43		0.53	0.54	0.62	0.46	0.45	0.42		0.24	0.19	0.18	0.28	0.26	0.35		0.32	0.31	0.22	0.24	0.48	0.46		0.35	22.1
PHOSPHO	l/b	İ	1.70	1.94		2.02	5.38	3.68	2.43	12.63	2.95		6.80	3.61	4.37	2.35	1.01	3.12		1.25	1.38	1.58	1.26	2.35	1.78		1.82	1.90	0.49	5.71	1.45	2.14		2.86	
	FLOW	10.065	7.786	9.665	4.975	5.720	4.847	8.426	4.571	7.857	4.770	4.358	4.803	5.492	9.874	8.280	13.898	14.157	10.673	9.073	9.990	6.194	6.814	7.268	7.153	6.683	7.499	7.022	6.741	6.526	6.593	0.000		7.348	
	DATE	-	2	က	4	Ð	9	7	8	O	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	56	27	28	29	30	31		AVERAGE	
	DAY	y) (S	Σ	⊢	3	⊢	Ľ.	S	S	≅	-	S		Щ	တ	တ	Σ	Н	>	_	ட	ဟ	တ	Σ	-	8	-	11	<i>y</i>	S):	Σ			

7346 LIBERTY DRIVE

716-693-0001

	0	2 2	1,611		_	1.2	.8	0	-	1.6	4.4		8.6	2.3	2.2	2.6	4	2	0	2.2	1.6	1.6	9	2	4		4.8	5.0	3.8	2	3.6	30	14	2		2.9	213.1
o ni	מתו וספ		ŭ	- -	-i ·	-		2	<u>-</u>	- -	<u>-</u>		8.	2	2.	2	2.	2	2	2	-	-	2	2	4	-	4	5	3	2	C.	, c	,	2		7	21
Nerone, I	CIICO	INE ma/	יוון, יוון, יוון	2 6	8	200	136	56	48	26	196		148	48	99	48	88	132	160	128	180	275	160	124	188		272	104	128	8	148	140	177	144		123.7	97.7%
FRAINK A. Nerone, P.E. CERT. 4A	C.	FEE ma/I	1,1	27	1.7	5.	χς,	2.8				4.0	21.2	5.3	5.0				9.7	5.5	7.6	4.5				25.8	8.8	7.1	6.7				4.1	11.1		8.2	645.3
	CROD	INF ma/I	+	07.0	0.10	000.0	92.9	,0,			110	7.761	64.6	51.1	42.0				111.9	108.4	180.8	204.0				126.3	162.6	154.8	81.2				175.0	192.9		112.4	92.7%
716-693-8759 FAX	SOLIDS 1HR	EFF ml/I	<0.1	×0.1	500			- 7	- 70.	V0.1	V0.1	- 0.	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1.	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	max
	SETT SOL		2.00	4.00	3.00	6.00 5.00	200	3.00	00.00	2.00	00.7	9.30	0.00	2.00	2.00	3.00	4.00	9.50	7.50	11.00	12.00	14.00	12.00	14.00	15.00	15.00	12.00	10.00	10.00	14.00	15.00	15.00	18.00	18.00	0	18.0	max
N YORK	Hd	X		7.4	7.2	7.2	7.2	7.7	7.7	7.7	7.2	7.1	7.7	5.7	7.7	7.7	7.3	9.7	7.7	7.3	7.3	7.3	7.3	7.2	7.3	7.3	7.4	7.2	7.2	7.4	7.3	7.3	7.5	7.4	7.7	1:,	шах
NIAGARA FALLS, NEW YORK	Hd	Z		7.3	7.1	7.1	7.1	7.2	7.0	7.7	7.2	7.4	7.7	7.4	1	10	7.7	7.7	1.2	7.1	7.7	1:3	۲.۱	7.0	6.9	7.1	7.3	0.7	7.2	7.3	7.0	7.1	7.2	7.0	a u	0.	ulm ulm
NIAGARA	Hd	INF, MAX	7.2	7.4	7.3。	7.4	7.4	7.4	7.4	7.6	7.4	7.4	7.7	1.7	7.3	7.3	1.7	5.7	6.7	4.7	7.7	5.7	3.1	7.6	(.)	رن)	7.7	7.7	7.3	4.7	(.5	(.3	7.5	7.5	7.6		IIIaX
_	Hd	INF, MIN	6.7	7.2	7.3	7.3	7.3	7.3	7.1	7.1	7.3	7.2	7.3	7.3	7.2	7.7	7.7	7.7	7.7	7.7	7.3	- / /	0.0	0.0	0.0	1 0.8	4.7	10.0	7.7	5.7	1.7	6.3	5.7	5.	6.7		
Jan-02	TURE,C	EFF	11.2	11.7	12.4	13.3	13.5	14.3	13.8	13.0	13.2	12.9	12.4	12.2	α+	12.1	- 4	10.0	4.5	14.0	0.4	117	α, τ,	13.5	10.0	13.0	110	7.1.	- 14.	2, 0	0.0	0.7.0	74.0	9.	12.4	27/0	5
	TEMPERATURE	۲	12.6	12.7	12.9	13.0	12.8	12.7	12.6	12.7	12.6	11.7	11.3	11.2	114	11.55	12.4	117	117	- 2	117	117	170	10.0	118	2.00	10.7	17.1	1,3	117	140	117	- 4	3	11.9	ave	
Y-0027979	\vdash	FLOW	6.365	6.385	6.037	5.961	6.378	6.002	6.933	6.697	5.938	13,151	11.321	21.389	9.630	9.434	11 155	9 853	9 008	7 771	6.611	6.865	6.500	6.980	7.460	13 988	12.761	9.528	9.786	7.880	8 272	7 754	8 232	2:104	8.775	Monthly	,
SPDES # NY-0027979		DAIE	- 0	7	۵.	4	Ω.	9	7	8	0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		AVERAGE		
	2	DAY 1	- 1	∆ F	- L		S) (C)	က (၁)	≥	F	>	-	ш	S	ဟ	Σ	H	>	 -	LL.	S	S	Σ	-	×	F	L	S	S	Σ	-	8	 				

COMMENTS																							10,772					The state of the s							
F.COLI			6		3	6				3		15	333				1333		3		2					m	CT.				ď			8.4	186.3
DUAL	AVE,mg/I	0.24	0.62	0.77	1.01	0.88	0.82	0.77	0.67	0.75	0.29	0.34	0.48	0.58	0.40	0.32	0.21	0.45	79.0	0.81	0.00	0.43	1 40	0.94	1.22	0.88	0.76	0.86	1.00	105	1.07	0.86	1	1.22	
CHLORINE RESIDUAL	MIN,mg/I MAX,mg/I AVE,mg/I	0.38	0.93	0.80	1.12	76.0	0.99	1.01	0.72	0.99	0.54	0.37	0.76	0.69	0.50	0.54	0.32	106	1 10	0.88	0.83	1 22	1.26	101	1.46	0.96	0.83	1.17	1.60	1.19	1.29	1.00		1.60	
CHLOR	MIN,mg/I	0.03	0.05	0.73	0.92	0.80	0.52	0.52	0.59	0.51	0.15	0.30	0.32	0.44	0.23	0.09	0.00	60 0	0.74	0.77	0.30	0.00	100	0.85	0.93	0.74	0.70	0.47	0.63	0.97	0.75	0.75		00.0	
OROUS	EFF,mg/I		0.62	0.60	0.54	0.97	0.77	0.78		0.50	0.48	0.40	0.23	0.32	0.37		0.35	0.36	0.36	0.40	0.46	0.53		0.69	0.49	0.29	0.24	0.32	0.33		0.52	0.62		0.47	35.2
PHOSPH	INF,mg/I		2.26	3.44	4.45	2.35	2.91	1.94		4.29	2.31	1.74	2.55	3.32	3.07		4.33	3.04	6.48	4.54	4.25	4.86		4.90	4.50	3.12	2.59	2.63	3.76		3.32	3.24		3.47	
	FLOW	6.365	6.395	6.037	5.961	6.378	6.002	6.933	6.697	5.938	13.151	11.321	21.389	9.630	9.434	11.155	9.853	9.006	7.771	6.611	6.865	6.500	6.980	7.460	13.988	12.761	9.528	9.786	7.880	8.272	7.754	8.232		8.775	
	DATE	-	2	0	4	D.	9	7	ω	6	10	7	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		AVERAGE	
	DAY	-	>		1	တ	n :	Σ	├	8			S	S)	Σ	-	>	L	LL.	S	ഗ	Σ	F	8		u_	S	တ	Σ	-	8	-			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

OLIDS	FFF ma/I	15.6	13.6	10.0	0.0	4 0	7.8		4.8	1.8	9.4	2.8	7.2	5.0	52	8 10	12.2	6.4	0 7	7	0.	4.8		6.2	10.2	6.0	9.6	4.2	8.0	7.0	9.2		7.4	
SUSP SOLIDS	INF.ma/I	+	26	100	207	† 6	00		244	92	196	120	200	228	196	308	348	392	172	477	7/1	784		180	132	92	224	152	188	224	244		205.7	, , ,
CC	EFF.ma/I	17.4	12.5				0	1 0.1	7.7	4.5	4.6				8.1	10.0	6.3	5.1					0.4	11.8	9.2	12.9				5.3	14.1		9.4	
CBOD		161.5	99.9				181 E	0.4.0	770.0	2.6.0	165.0				146.3	196.1	194.7	87.3				10.7	180.0	183.6	125.1	114.9				195.7	190.0		161.1	20010
SOLIDS,1HR	EFF,mI/I	×0.1	<0.1	<0.1	V0.1	×0.1	5			7.0	0/	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	< 0 < 1	7	70.7	- 0	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	
SETT SO	INF,mI/I	2	7.0	8.0	13.0	110	17.0	18.0	17.0	10.0	0.0	16.0	18.0	15.0	17.0	20.0	21.0	24.0	25.0	21.0	19.0	24.0	22.0	22.0	20.5	18.0	25.0	23.0	20.0	18.0	24.0		25.0	2000
	EFF, MAX	7.5	7.3	7.4	7.3	7.3	7.5	7.4	7.7	5 L	5 .	7.4	4.7	7.5	7.4	7.5	7.4	7.3	7.4	7.3	77	7.4	7.2	3.5	5.7	7.3	(.3	7.5	7.3	7.3	7.3		7.7	Ye m
-	EFF, MIN	7.4	7.2	7.3	7.1	6.8	7.2	7.3	7.4	7.5	1:51	7.5	6.3	(.3	7.3	7.4	7.2	7.2	7.2	7.2	7.2	7.2	7.0	7.7	7.5	7.7	/	7.1	7.2	7.3	7.2		9.9	.E
рн	INF, MAX	7.6	7.4	7.5	7.6	7.6	7.6	7.5	7.5	7.6	7.8	1.0	1.4	6.7	7.5	7.5	7.4	7.4	7.4	7.4	7.7	7.5	7.5	2.7	7.7	1.7	1.0	(.)	6.7	7.4	4.7	1	1.1	max
ph	INF, MIN	7.2	7.2	7.3	7.0	6.7	7.2	7.2	7.4	7.5	7.3	Э П	0.0	5.7	6.3	7.4	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.7	7.2	7.4	1	1.1	7.7		5.8	i i	0.0	E
יו טאט וי	EFF	10.6	9.4	11.3	10.6	11.3	11.3	11.6	12.1	11.4	110	707	2.0.7	- 0.	5.07	10.5	10.9	10.7	10.1	9.8	10.4	11.1	10.4	10.0	10.5	10.5	2.7		0	0.0	10.0	107	7.2	ave.
LINI LINA I UNE	TZ.	10.9	9.5	10.3	10.9	10.9	11.1	11.1	11.0	10.5	10.8	10.2	10.7	7.0.7	- 0	20.00	7.0.7	0.0	9.0	9.7	10.1	10.1	9.6	9.6	9.6	80	10.2	10.4	10.4	5.5	10.2	10.2	0,6	ave.
12 014	rLOw	23.135	16.699	15.066	11.094	9.842	8.875	8.875	9.188	10.504	10,490	14 123	11 644	11 207	0.407	9.033	9.000	12.000	12.023	10.755	9.445	9.634	14.768	12,300	10.248	9.327	90.0	8 803	8 773	27.00	0.44.0	11.327	Monthly	WICH HIS
חאת	מאוש	- c	7 0	2	4	2	9	7	8	6	10	11	12	17	14	r r	5 4	17	- 07	0 9	BL.	20	21	22	23	24	25	26	27	28		AVERAGE		
γVU	בו	LO	20	0 2	≥	- :	8	-	ഥ	တ	(O)	Σ	 	×		- 11	. 0	0 0.	2	≥ F	- :	8	<u>-</u>	ш_	S	တ	≥	-	×	-				

CHILLIAMOO	COININENIS																																		
FOOL	/ 100 ml	1100	70	38				c.	>	2) m	>			7	2		2)	33					2	ď	0 0	0							4.8	13.2
IDITAL	MAX ma/l AVF ma/l	ט מין	0.03	0.63	0.56	0.74	0.60	0.61	0.66	0.23	0.72	0.78	0.0	0.00	0.22	000	0.00	0.07	0.63	0.64	0.64	0.70	0.82	0.02	0.75	0.00	0.03	0.70	0.70	1.02	0.10	0.31		1.16	
CHLORINE RESIDITAL	MAX ma/l	88 0	0.00	0.88	0.80	0.88	0.84	0.67	0.78	100	0.78	06.0	0.20	0.75	0.83	0 88	0.00	0.00	0.00	0.69	0.72	0.88	0.73	1 18	0.77	280	40.00	200	1.30	1.10	÷!	0.57		1.47	
CHLOF	MIN ma/I		3.5	U.Z1	0.42	0.57	0.48	0.56	0.57	0.42	0.68	0.56	0.48	0.55	0.65	0.32	0.02	0.00	0.0	0.59	0.52	0.48	0.56	0.56	0.03	000	0.18	0.52	0.02	0.02	300	0.00	0	0.00	
IOROUS	EFF.ma/I	-	20.0	0.43	0.39	0.36		0.51	0.46	0.38	0.59	0.67	0.66		0.75	0.87	0.83	07.0	0.10	0.56	0.57		0.72	0.76	0.67	0.63		0.64	0.70	0.64	79.0	40.0	29.0	0.00	60.5
PHOSPH	INF,mg/I	4.21	107	10.0	2.51	3.44		2.79	2.47	2.47	3.93	3.40	1.42		4.74	4.21	4.54	4.50	20.	4.20	4.99		4.25	0.94	3.31	3.59		4.68	6.04	4.01	7 80	3	3 63	20.0	
	FLOW	23.136	16 600	7.000	13.000	11.094	9.842	8.875	8.875	9.188	10.504	10.490	14.123	11.644	11.207	9.655	9.858	13,230	10 003	10.750	10.766	9.445	9.634	14.768	12.300	10.248	9.327	9.086	8.893	8.773	8 420	2: :2	11.327	170	
	DATE	-	2	1 0	2	4 1	C I	9	7	8	6	10	11	12	13	14	15	16	17	- 07	0 9	9	20	21	22	23	24	25	26	27	28		AVERAGE		
	DAY	ഥ	S	U) 2	ŽΙΗ	-	8	-	ш	S	တ	∑	-	8	⊢	Ш	တ	v.		ž F	- :	8	⊢	ш	S	S	Σ	-	3	H				

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Mar-02

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

CBOD SUSP SOLIDS INF,mg/l EFF,mg/

0.01
14.00 30.00 25.00 15.00 7.00 14.00
7.4 7.3 7.4 7.5 7.3
7.3 7.3 7.3 6.9 6.9
4.7 7.3 7.3 7.3 7.5 7.5 7.7 7.5
7.3 7.4 7.5 7.7 7.5 7.7 7.5 7.7 7.5 7.7 7.5 7.7 7.5 7.5
10.7 10.5 9.6 10.0
10.3
7.608
1
1 74CW

0.15 2900 0.17 0.17 0.70 0.84 3 0.77 0.77 3 1.05 3 0.15 3 0.15 3 0.15 3 0.15 3 0.15 3 0.15 3 0.15 3 0.15 3 0.17 3 0.18 3 0.19 3 0.10 3 0.1	
	_

作の大田藤

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Apr-02

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

30.10	OCLIDS FFF	Err,mg/I		8.6			3.0	6.8	4.4	62	6.5	3.4	4.6	4.0	8.0	11.6	6.4	αυ	2.0	2.5	2.0	0.7	3.4	2.0	44	4.2	5.0	2.6	5.8	5.4	9.0	5.8		5.6	527.9
201100 00110	, 1000	INF, mg/I	228	188			532	206	144	100	136	64	108	191	428	152	90	136	8	124	100	220	168	332	296	356	.452	100	232	616	376	240		217.0	97.4%
CBOD		rr,mg/l			12.9		9.7	8.3				9.6	7.6	3.3	5.8				8.5	r.	5.0	6.3				8.8	12.8	4.5	16.4					8.6	762.2
2	INE mail	וואן יוואן			196.2		6.76	80.2				118.0	123.4	87.5	316.8				150.3	156.4	184.4	178.2				308.5	419.0	138.5	224.9				10,	185.8	95.4%
SOLIDS 1HR	EEE mill	,	0,0	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	max
SETT SO	INF		0.0	10.0	14.0		14.0	5.0	6.0	4.5	4.5	4.0	5.0	3.0	31.0	14.0	14.0	17.0	13.0	12.5	23.0	25.0	30.0	37.0	28.0	38.0	37.0	20.0	20.0	55.0	32.0	25.0	C LL	0.00	max
Ha	EFF. MAX	7.1	7.3	٠ د د	7.7	4.7	7.2	7.3	7.2	7.2	7.2	7.3	7.3	7.2	7.2	7.3	7.5	7.2	7.2	7.1	7.2	7.3	7.2	7.0	6.9	7.3	7.2	7.3	7.4	7.2	7.2	7.3	7 7	C.,	шах
Hd	EFF. MIN	7.1	5.7	7.7	10	7.7	6.9	7.0	7.1	6.8	6.8	7.3	7.1	7.0	7.0	7.2	7.2	7.0	7.0	6.9	7.0	6.9	6.8	6.9	6.6	7.0	7.2	7.0	7.2	7.2	6.8	9.9	y y	2.	E E
H	INF, MAX	73	7.0	7.1	- ' '	7.7	1.1	7.3	7.7	7.1	7.4	C.)	7.4	ť.)	7.3	7.2	7.2	7.4	7.1	7.2	7.0	7.2	7.0	7.6	7.9	7.5	5.7	¢.,	7.4	7.2	5.7	(.3	7.9	?	шах
Ha	INF, MIN	7.2		6.7	- 1	2.0	6.0	7.0	0.7	5.0	0.0	7./	1.7	7.1	1.7	0.7	6.9	6.9	7.0	6.8	7.0	7.2	6.9	0.7	0.7	6.7	7.7	7.4	1.1	1.7	10.1		6.7		
ATURE,C	EFF	11.0	10.6	80	40.5	10.4	0.0	10.9	7 0.0		14.3	3.0	25 - 5	1001	7.0	J. 6	0.1	13.2	12.8	13.0	14.1	14.0	13.6	12.7	177	13.0	13.7	4.0.4	13.0	4.7	12.1	17.1	12.3	0/10	ava.
I EMPERATURE,	INF	10.0	10.6	9.2	9 6	0.0	10.0	10.0	10.0	10.7	10.0	107	10.4	700	2 C	2.0.	† C	7.1.7	0.17	Ç.	5.1.5	υ.	0 1	7		12.0	11.0	0.77	0.1.	7.0	5	ţ.	10.9	ave	
	FLOW	11.284	14.360	9.930	13.911	12.509	11 339	9.459	23 730	10.707	7,674	6 782	13 05B	17.708	17 002	10.360	10.369	0.500	9.930	12.733	19.343	0.752	0.733	7.007	A 578	7.010	7.356	6 003	0.000	13 285	12 038	200	11.322	Monthly	
	DAIE	-	2	8	4	5	G	7	80	o	9	4-1	12	13	14	15	1,00	17	- α	2 0	200	27	22	23	24	25	26	27	28	29	30		AVERAGE		
	DAY:	Σ	-	>	⊢	Ш	S	S	Σ	F	M	 	L	S	S	Σ	-	· >	: -	- 14	. 0.	O.	2		×	: -	LL	S	S	Σ	 -			•	

COMMENTS	Civiliano																																
F.COI I	/ 100 m	200		2	5	ď) (r)			ď	>		7.4		,		C	0	C	3 6	7			c)	7) m	>			5.2	14.9
DUAL	AVF ma/I	0.68	0.35	1 02	1 17	0.89	134	2 2	5 5	1.22	1.76	1 20	0.42	107	0.48	1 30	1.03	200	0.92	08.0	0.00	0.03	0.42	000	0.88	0.80	760	0.78	0.77	121	0.67	1.43	
CHLORINE RESIDUAL	MIN.mg/I MAX.mg/I AVE mg/I	0.80	0.45	1.58	1.43	1.55	1.50	127	105	140	1.41	151	0.64	188	1 13	1.50	1,60	1.24	1 22	35.5	77.0	0.74	107	118	1 10	1.02	1.12	121	96.0	1.32	1.21	1.88	
CHLO	MIN.ma/I	0.60	0.26	0.66	0.94	0.00	1.08	0.87	0.98	0.94	1.02	1.02	0.30	0.25	0.10	118	1.28	0.64	0.77	0.61	0.53	22.0	41.0	0.53	0.63	0.51	0.71	0.52	0.48	1.12	0.00	0.00	
OROUS	EFF,mg/I	0.36	0.55	09.0		0.40	0.63	0.48	0.67		0.50	0.54	0.56	0.64	0.51	0.42	!	0.47	0.43	0.42	0.43	0.45	0.62		0.55	0.53	0.59	0.63	0.62	0.60		0.53	50.5
PHOSPHO	INF,mg/I	1.48	3.66	2.92		19.23	7.33	4.02	1.99		0.66	2.61	2.96	6.24	2.46	2.03		2.65	230	4.21	2.38	5.69	4.75		10.10	10.18	3.04	3.98	3.59	5.07		4.49	
	FLOW	11.284	14.360	9.930	13.911	12.509	11.339	9.459	23.730	10,404	7.674	6.782	13.958	17.298	17.902	10.369	10.368	9.936	12.753	19.345	10.657	8.753	8.067	7.063	6.576	7.019	7.356	6.003	9.526	13.285	12.038	11.322	
	DATE	-	2	ဇ	4	5	မ	7	8	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	AVERAGE	
	DAY	∑	-	X	-	LL	တ	တ	Σ	F	≥		щ	S	S	Σ		>	-	L	S	တ	Σ	—	≯	 -	4-	S	S :	ΣΙ			_

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 May-02

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

INF, MIN INF, MAX EFF, MIN IFF, MIN INF, MIN	CLOW NF EFF INF, MIN INF, MIN EFF MIN INF, MIN EFF MIN INF, MIN EFF MIN				TEMPERATURE	ATURE.C	Ha	He	1	7	COLLEG	001				
8 564 11.6 13.1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8 564 1.6 1.3 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.2 </th <th>DA</th> <th>TE</th> <th> </th> <th>H.</th> <th></th> <th>MIN</th> <th>INE MANY</th> <th>EEE MIN</th> <th>ביין</th> <th>1110</th> <th>LIDS,1HR</th> <th>CB</th> <th>go</th> <th>SUSPS</th> <th>OLIDS</th>	DA	TE		H.		MIN	INE MANY	EEE MIN	ביין	1110	LIDS,1HR	CB	go	SUSPS	OLIDS
4657 146 134 6.9 7.4 7.7 7.2 2.200 6.01 12.7 2.80 8.809 1.1 1.2 7.2 7.3 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 3.00 4.01 284.8 7.4 4.0 7.089 1.2 1.2 7.2 7.2 7.0 6.1 284.8 7.4 4.0 7.089 1.2 1.2 7.2 1.40 6.0 7.4 4.0 6.0 7.4 4.0 7.03 1.2 1.4 7.7 7.2 7.0 7.2 1.40 6.0 7.4 7.0 7.2 1.40 6.0 7.0 2.2 7.0 7.2 1.40 6.0 7.0 7.2 1.40 6.0 7.0 7.0 7.2 1.40 6.0 7.0 7.2 7.4 7.4 7.2	4 657 146 134 6.2 7.4 7.5 2.200 6.01 155,4 1.2.7 2.50 8.0839 1.1.6 1.28 7.2 7.3 7.2 7.3 2.00 6.01 207.2 3.4 1.0 9.023 1.2.0 1.3.6 7.1 7.2 7.0 7.2 14.00 6.01 207.2 3.4 1.0 9.023 1.2.0 1.3.6 7.1 7.2 1.400 6.01 207.2 3.4 1.0 7.038 1.2.0 1.3.6 7.1 7.2 1.400 6.01 207.2 3.4 1.0 1.1.088 1.2.2 1.4.7 6.0 7.2 1.400 6.01 207.2 3.0 1.1.1.288 1.2.2 1.4.5 7.0 7.2 7.2 1.400 6.01 3.0 3.2 1.0 1.1.1.288 1.2.0 1.2.1 1.2.2 1.4.00 6.01 2.0 1.0 1.0 2.0 1.0	-	-	8.564	11.6	13.1	0 9	7.2	NIIIA	Err, MAX	- 1	EFF,mI/I	INF,mg/I	EFF,mg/I	INF,mg/I	EFF,mg/I
BER09 11.6 12.8 7.2 7.4 7.1 7.4 2.300 <0.1 20.3 1.2 1.9 1.0 7.1 7.2 2.300 <0.01 237.2 3.4 4.08 9.02 4.01 237.2 3.4 4.08 9.02 4.00 4.01 237.2 4.00 2.01 237.2 3.4 4.08 3.0 4.01 2.02 4.00 4.01 2.00 4.01 2.00 4.01 2.02 4.00 3.2 4.00 2.01 2.00 4.01 2.00<	BEORG T.G. T.G. <t< td=""><td></td><td>2</td><td>4 657</td><td>146</td><td>137</td><td>0.0</td><td>7.7</td><td>0.7</td><td>7.7</td><td>22.00</td><td><0.1</td><td>155.4</td><td>12.7</td><td>280</td><td>5.6</td></t<>		2	4 657	146	137	0.0	7.7	0.7	7.7	22.00	<0.1	155.4	12.7	280	5.6
7.683 11.7 12.2 7.4 7.2 7.3 7.4 7.3 7.4 7.3 7.4 7.3 7.4 7.2 14,00 c0.1 227.2 3.4 112 7.68 1.2.0 1.36 7.1 7.3 7.0 7.2 14,00 c0.1 224.8 7.4 408 7.68 1.2.2 14.7 6.6 7.0 6.7 7.1 37.00 c0.1 224.8 7.4 408 8.828 1.2.2 14.7 6.6 7.0 6.7 7.1 37.00 c0.1 284.8 4.5 6.0 1.0.08 1.2.2 14.3 7.0 7.2 14.00 c0.1 342.3 10.9 320 1.0.08 1.2.2 14.3 7.0 7.2 14.00 c0.1 342.3 10.9 320 1.0.08 1.2.2 14.3 7.0 7.2 14.00 c0.1 342.3 10.9 320 1.0.08 1.2.2 <td>7.883 1.1.7 1.2. 7.2 7.3 7.0 7.0 4.01 254.0 4.01 254.0 7.1 4.08 8.023 12.2 1.36 7.1 7.2 7.0 4.0 264.8 7.4 4.08 8.023 12.2 14.7 6.6 7.0 7.2 14.00 4.01 264.8 7.4 320 7.703 12.2 14.7 6.6 7.0 7.2 14.00 4.01 264.8 7.4 320 1.0368 12.2 14.2 7.0 7.2 7.2 14.00 4.01 26.9 6.8 7.2 34.00 4.01 320 4.6 6.8 7.2 34.00 4.01 4.6 6.8 7.2 34.00 4.01 32.0 4.0 6.8 8.0 1.0 30.0 4.0 8.0 8.0 1.0 30.0 4.0 8.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 <td< td=""><td>(4)</td><td>3</td><td>8.809</td><td>11.6</td><td>10.4</td><td>7.0</td><td>4.7</td><td>1.1</td><td>7.4</td><td>23.00</td><td><0.1</td><td>300.3</td><td>12.8</td><td>196</td><td>3.0</td></td<></td>	7.883 1.1.7 1.2. 7.2 7.3 7.0 7.0 4.01 254.0 4.01 254.0 7.1 4.08 8.023 12.2 1.36 7.1 7.2 7.0 4.0 264.8 7.4 4.08 8.023 12.2 14.7 6.6 7.0 7.2 14.00 4.01 264.8 7.4 320 7.703 12.2 14.7 6.6 7.0 7.2 14.00 4.01 264.8 7.4 320 1.0368 12.2 14.2 7.0 7.2 7.2 14.00 4.01 26.9 6.8 7.2 34.00 4.01 320 4.6 6.8 7.2 34.00 4.01 4.6 6.8 7.2 34.00 4.01 32.0 4.0 6.8 8.0 1.0 30.0 4.0 8.0 8.0 1.0 30.0 4.0 8.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 <td< td=""><td>(4)</td><td>3</td><td>8.809</td><td>11.6</td><td>10.4</td><td>7.0</td><td>4.7</td><td>1.1</td><td>7.4</td><td>23.00</td><td><0.1</td><td>300.3</td><td>12.8</td><td>196</td><td>3.0</td></td<>	(4)	3	8.809	11.6	10.4	7.0	4.7	1.1	7.4	23.00	<0.1	300.3	12.8	196	3.0
9.023 1.20 1.31 7.3 7.0 7.2 14,00 <0.1 264.8 7.4 409 7.688 1.22 14.1 6.7 7.2 7.0 7.2 14.00 <0.1	9.023 1.20 1.31 7.1 7.2 14.00 <0.1 224.8 7.4 409 7.688 1.20 1.41 6.7 7.2 7.0 7.2 14.00 <0.1 22.8 7.4 409 7.688 1.22 1.41 6.7 7.2 7.0 7.2 14.00 <0.1 342.3 10.9 328 7.788 1.22 1.45 6.6 7.0 6.7 7.2 14.00 <0.1 342.3 10.9 328 1.0086 1.22 1.45 7.0 7.4 7.2 1.2 14.00 <0.1 342.3 10.9 328 1.0086 1.20 7.2 7.2 1.20 7.2 3400 <0.1 342.3 10.9 328 1.077 1.24 1.2 7.2 7.2 1.2 1.2 1.0 32.3 1.2 1.0 32.2 1.078 1.2 1.2 1.2 1.2 1.2 <t< td=""><td>4</td><td>+</td><td>7 893</td><td>117</td><td>12.0</td><td>7.7</td><td>3.</td><td>7.7</td><td>7.3</td><td>24.00</td><td><0.1</td><td>237.2</td><td>3.4</td><td>112</td><td>4.2</td></t<>	4	+	7 893	117	12.0	7.7	3.	7.7	7.3	24.00	<0.1	237.2	3.4	112	4.2
7,686 1,22 1,41 7,2 32,00 <0,1 320 7,703 1,23 14,1 6,6 7,2 7,0 7,2 14,0 <0,1	7.088 1.2.2 1.4.1 7.3 7.1 7.2 1.4.0 co.1 32.0 co.1 <t< td=""><td>14)</td><td>10</td><td>9 023</td><td>12.0</td><td>13.E</td><td>7.1</td><td>1.3</td><td>0.7</td><td>7.2</td><td>14.00</td><td><0.1</td><td>264.8</td><td>7.4</td><td>408</td><td>8.4</td></t<>	14)	10	9 023	12.0	13.E	7.1	1.3	0.7	7.2	14.00	<0.1	264.8	7.4	408	8.4
7,703 1,23 1,7-7 6,7 7,0 7,1 4,0 6,0 8,828 1,22 14,2 7,0 6,7 7,2 14,00 6,0 1,0 8,0 1,0,08 1,22 14,2 7,0 7,2 7,2 14,0 601 34,2 6,0 1,0,08 1,22 14,3 7,0 7,4 6,9 7,2 15,00 6,0 1,0 30,2 10,9 37,2 1,0,08 1,22 14,3 7,0 7,1 6,9 7,2 24,00 6,0 7,1 10,9 37,2 10,9 37,2 10,9 37,2 10,9 37,2 10,0 30,2 10,0 37,2 10,0 30,0 10,0 37,2 10,0 30,0<	7.703 1.23 1.4.7 6.7 7.2 7.0 6.7 7.1 7.0 6.7 7.1 7.00 6.0 6.0 6.0 6.0 6.0 6.0 7.0 7.2 1.4 0.0 6.0 6.0 7.0 7.2 1.4 0.0 6.0 7.2 1.4 0.0 6.0 6.0 6.0 7.0 7.2 1.4 0.0 6.0 4.5 0.0 6.0 6.0 1.0 6.0 7.0 3.0 6.0 7.0 6.0 6.0 7.0 3.0 6.0 7.0 6.0 6.0 7.0 7.2 1.4 0.0 6.0 7.0 6.0 6.0 7.0 6.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6.0 7.0 6	9	3	7.688	12.2	14.1	7.7	5.7	7.7	7.2	32.00	<0.1			320	5.8
8.828 1.22 1.45 7.0 7.1 37.00 <0.1 4.5 9.88 11.28e 1.22 1.45 7.0 7.4 7.2 1.40 <0.1	8.828 1.22 1.42 7.0 7.1 37.00 <0.1 342.3 4.5 32.8 1.1.286 1.22 1.45 7.0 7.2 14.00 <0.1	7	7	7.703	123	14.7		7.7	0.7	7.7	14.00	<0.1			284	3.8
11.268 12.2 14.3 7.2 7.4 7.2 14.00 <0.1 34.3 4.5 6.9 7.2 14.00 <0.1 34.3 4.5 6.9 7.2 14.00 <0.1 30.7 6.9 37.2 14.00 <0.1 30.7 6.9 37.2 34.00 <0.1 30.7 6.9 37.2 34.00 <0.1 30.7 6.9 37.2 34.00 <0.1 30.7 6.9 37.2 34.00 <0.1 30.7 7.8 6.9 7.2 24.00 <0.1 30.7 7.2 7.2 34.00 <0.1 30.7 7.2 32.0 <0.1 30.7 7.2 30.7 7.2 30.7 7.2 30.7 7.2 30.7 7.2 7.0 25.00 <0.1 30.7 7.2 30.0 <0.1 30.7 7.2 30.0 <0.1 30.7 7.2 30.0 <0.1 30.2 30.0 30.1 30.2 <0.1 30.2 30.0 30.1	11.268 12.2 14.5 7.0 7.4 7.0 7.2 7.4 7.0 7.0 4.5 6.0 7.1 4.0 4.	8	3	8.828	12.2	14.2	7.0	7.7	7.0	1.7	37.00	<0.1			328	3.8
10.098 12.0 14.3 7.2 7.4 6.9 7.2 34.0 <0.1 342.3 10.9 372 7.648 12.2 14.3 7.0 7.1 6.9 7.2 34.00 <0.1	10.098 12.0 14.3 7.2 7.3 6.9 7.2 15.00 <0.1 240.3 10.9 372 7.648 12.2 14.3 7.2 7.3 6.9 7.2 24.00 <0.1	C)	0	11.268	12.2	1	7.0	7.1	7.7	7.2	14.00	<0.1		4.5	809	5.8
7,648 12.2 14.3 7.0 7.3 6.9 7.2 34.00 <0.1 20.9 7.5 19.0 10,177 12.3 13.9 6.8 7.2 6.8 7.3 18.00 <0.1	7,648 12.2 14.3 7.2 3.4,00 <0.1 20.9 7.5 34,00 <0.1 340,5 4.6 320 10,177 12.3 13.9 6.8 7.2 24,00 <0.1	<u>-</u>	0	10.098	12.0	14.3	7.2	7.3	0.4	7.7	15.00	×0.1	342.3	10.9	372	5.0
10.177 12.3 13.9 6.8 7.2 6.8 7.2 24.00 <0,1 340.5 4.6 320 21.770 12.4 13.9 6.8 7.0 6.8 7.0 25.00 <0,1	10.177 12.3 13.9 6.8 7.1 6.8 7.2 24.00 <0.1 340.5 4.6 320 21.770 12.4 13.9 6.7 7.0 6.6 7.0 25.00 <0.1	+	_	7.648	12.2	14.3	7.0	5.7	200	7.7	34.00	<0.1	209.7	6.7	190	3.8
21,770 12.4 13.9 6.7 7.0 6.6 7.0 25.00 <0.1 728 31,769 12.1 12.2 6.6 7.5 6.6 7.0 25.00 <0.1	21,770 12,4 13.9 6.7 7.2 6.5 7.3 18.00 <0,1 728 31,766 12,1 12,2 6.6 7.5 6.5 7.2 15.00 <0,1	1,	2	10.177	12.3	13.9	0, 00	7.2	0.0	7.7	24.00	<0.1	340,5	4.6	320	3.6
31.76g 12.1 12.2 6.6 7.5 6.5 7.0 25.00 <0.1 25.00 <0.1 376 18.776 11.7 12.4 7.2 7.5 7.3 7.4 12.00 <0.1	31.769 12.1 12.2 6.6 7.5 6.5 7.2 5.00 <0.1 25.00 <0.1 25.00 <0.1 376 376 376 376 18.7 7.2 1.5 0.0 7.2 15.00 <0.1 12.8 8.9 146 28.4 18.00 <0.1 17.8 8.9 146 18.0 18.0 <0.1 17.8 8.9 17.8 18.0 <0.1 17.8 8.9 18.0 18.0 <0.1 18.0 <0.1 18.0 <0.1 18.0 <0.1 18.0 <0.1 18.0 <0.1 18.0 <0.1 18.0 <0.0 18.0 <0.0 18.0 <0.0 <0.0 18.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0 <0.0	1,	8	21.770	12.4	13.9	2.0	7.7	0.0	5.7	18.00	<0.1			728	4.2
18.776 11.7 12.4 7.2 7.5 7.3 7.4 15.00 <0.1 82.9 8.9 146 13.641 12.1 13.3 7.2 7.5 7.3 7.4 7.2 6.9 8.9 146 13.641 12.1 13.3 7.4 7.2 7.3 7.3 24.00 <0.1 128.6 6.2 96 12.636 12.1 13.2 7.2 7.4 7.2 7.3 24.00 <0.1 128.6 6.2 96 12.68 12.1 13.1 7.2 7.4 7.2 7.3 24.00 <0.1 217.3 6.0 6.0 9.266 12.3 13.2 7.4 7.4 7.2 7.2 7.0 <0.1 217.3 6.0 6.0 9.266 12.5 13.7 7.4 7.2 7.2 7.2 7.0 <0.1 217.3 6.0 10.323 12.5 13.2 12.0 <0.1 2	18.776 11.7 12.4 7.2 7.5 6.9 7.2 15.00 <0.1 82.9 8.9 116 13.641 12.1 13.3 7.2 7.5 7.3 12.00 <0.1	1	4	31.769	12.1	12.2	0	7.5	0.0	1.0	25.00	<0.1			376	9.0
13.641 12.1 13.3 7.2 7.4 7.2 7.4 12.00 <0.1 82.9 8.9 116 13.949 12.1 13.3 7.4 7.2 7.3 24.00 <0.1	13.641 12.1 13.3 7.2 7.3 7.4 12.00 <0.1 82.9 8.9 116 13.949 12.1 13.3 7.4 7.4 7.2 7.3 24.00 <0.1	1	5	18.776	11.7	124	7.0	7.5	0.0	7.7	15.00	<0.1			264	14.4
13.949 12.1 13.3 7.4 7.4 7.2 7.3 18.00 <0.1 128.6 6.2 96 12.636 12.1 13.2 7.4 7.4 7.3 7.3 24.00 <0.1	13.949 12.1 13.2 7.4 7.2 7.3 18.00 <0.1 128.6 6.2 96 12.636 12.1 13.2 7.4 7.4 7.2 7.3 24.00 <0.1	16	9	13.641	121	13.3	7.7	7.0	1.3	7.4	12.00	<0.1	82.9	8.9	116	14.5
12.636 12.1 13.2 7.2 7.4 7.3 7.3 24.00 <0.1 91.7 4.0 180 11.346 12.1 13.2 7.2 7.4 6.9 7.2 7.3 6.0 6.0 6.0 6.0 9.266 12.3 13.2 7.0 7.3 7.0 7.2 7.4 6.9 7.2 7.0 6.0	12.636 12.1 13.2 7.4 7.3 7.3 24.00 <0.1 91.7 4.0 180 11.346 12.1 13.2 7.2 7.4 7.2 7.3 23.00 <0.1	1.	7	13.949	12.1	2.5.5	7.7	1.4	7.7	7.3	18.00	<0.1	128.6	6.2	96	4.3
11.346 12.1 13.2 13.2 13.2 13.2 13.2 13.1 13.1 13.2 <	11.346 12.1 13.2 7.2 7.3 7.3 23.00 <0.1 217.3 6.0 60 60 9.266 12.3 13.1 7.2 7.4 6.9 7.2 70.00 <0.1	132	8	12.636	12.1	3.5	1.1	4.7	6.3	7.3	24.00	<0.1	91.7	4.0	180	4.2
9.266 12.3 13.1 7.2 7.4 6.9 7.2 32.00 <0.1 260 10.323 12.3 13.2 7.0 7.3 7.0 7.2 7.0 7.2 7.0 224 8.266 12.5 13.7 7.4 7.4 7.2 7.3 65.00 <0.1	9.266 1.23 1.32 1.34 1.32 1.30 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.34 1.32 1.32 1.34 1.32 1.32 1.34 1.34 1.32 1.32 1.34 1.32 1.32 1.34 1.32 1.32 1.34 <t< td=""><td>15</td><td>6</td><td>11.346</td><td>12.1</td><td>13.4</td><td>7.7</td><td>1.4</td><td>7.1</td><td>7.3</td><td>23.00</td><td><0.1</td><td>217.3</td><td>0.9</td><td>9</td><td>1.0</td></t<>	15	6	11.346	12.1	13.4	7.7	1.4	7.1	7.3	23.00	<0.1	217.3	0.9	9	1.0
10.323 1.25 1.3 1.3 1.0 7.2 7000 <0.1 224 8.266 12.5 13.5 7.1 7.4 7.2 7.4 7000 <0.1	10.323 1.2. 1.3. 1.0 7.2 7.0 7.2 7.0 7.2 7.0 4.0 2.24 8.266 1.2. 13.5 7.1 7.4 7.2 7.4 7.0 7.3 460 7.725 12.6 14.5 7.3 7.3 7.2 7.2 7.3 65.00 <0.1	20	0	9.266	103	13.0	7.7	1.4	9.9	7.2	32.00	<0.1			260	2.5
8.266 12.5 13.7 7.4 7.2 7.3 65.00 <0.1 348.2 7.3 460 7.725 12.5 13.7 7.4 7.2 7.2 7.2 65.00 <0.1	8.266 12.5 13.7 7.4 7.2 7.3 65.00 <0.1 348.2 7.3 460 7.725 12.6 13.7 7.4 7.2 7.2 7.3 65.00 <0.1 348.2 7.3 480 6.913 12.6 14.2 7.3 7.2 7.2 7.3 65.00 <0.1 368.9 6.4 440 6.204 12.5 14.5 7.2 7.2 7.3 52.00 <0.1 214.9 5.6 412 6.803 12.5 14.7 7.3 7.4 7.2 7.3 17.00 <0.1 214.9 5.6 440 6.803 12.5 14.7 7.3 7.4 7.2 7.3 17.00 <0.1 155.2 5.7 264 6.803 12.5 14.3 7.3 7.4 7.1 7.2 27.00 <0.1 155.2 5.7 240 6.021 12.9 14.3 7.3 7.4	21	-	10.323	123	13.5	7.7	7.3	7.0	7.2	70.00	<0.1			224	3.9
7.725 12.6 12.7 12.4 12.4 12.7 12.7 12.6 14.2 12.7 12.4 12.7 12.7 12.6 14.2 12.3 12.3 12.2 14.2 12.3 12.3 12.2 12.4 12.4 12.4 12.4 12.4 12.4 12.4 12.4 12.4 12.2 14.2 12.2 12.2 14.2 12.2 12.2 14.2 12.2 12.4 12.2 14.2 12.2 14.2 12.2 14.2 12.2 14.2 12.2 14.2 12.2 14.2 12.2 12.2 12.4 12.2 12.2 12.4 12.2 12.2 12.4 12.2 <t< td=""><td>7.725 12.6 13.1 1.4 1.2 7.3 65.00 <0.1 348.2 7.3 480 6.913 12.6 14.2 7.3 7.2 7.2 60.00 <0.1</td> 368.9 6.4 440 6.913 12.6 14.5 7.2 7.2 7.3 52.00 <0.1</t<>	7.725 12.6 13.1 1.4 1.2 7.3 65.00 <0.1 348.2 7.3 480 6.913 12.6 14.2 7.3 7.2 7.2 60.00 <0.1	22	2	8 266	12.5	12.0	7.1	1.4.	7.2	7.4	70.00	<0.1			460	2.6
6.913 12.6 14.5 7.2 7.5 7.2 60.00 <0.1 368.9 6.4 440 6.204 12.5 14.7 7.3 7.4 7.2 7.3 52.00 <0.1 214.9 5.6 412 6.803 12.5 14.2 7.2 7.4 7.2 7.3 17.00 <0.1 155.2 5.7 264 6.803 12.5 14.2 7.2 7.4 7.2 7.2 27.00 <0.1 155.2 5.7 264 6.803 12.5 14.3 7.4 7.1 7.2 27.00 <0.1 24.9 5.6 20 6.220 12.5 14.3 7.4 7.1 7.2 27.00 <0.1 247.6 3.9 276 6.021 12.9 14.3 6.9 7.4 7.1 7.1 34.00 <0.1 247.6 3.9 276 6.021 12.9 15.2 7.3 7.4 7.1 7.1 34.00 <0.1 247.6 3.9 276 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 272.9 8.6 204 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 223.9 3.2 376 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2	6.913 12.6 14.5 7.3 7.3 7.2 7.2 60.00 <0.1 368.9 6.4 440 6.204 12.6 14.5 7.2 7.3 7.3 52.00 <0.1	23	3	7 725	12.6	5 5	4:7	4.7	1.2	7.3	65.00	<0.1	348.2	7.3	480	5.0
6.204 12.5 14.7 7.3 7.4 7.2 7.3 17.00 <0.1 214.9 5.6 412 6.803 12.5 14.7 7.3 7.4 7.2 7.2 9.00 <0.1 155.2 5.7 264 6.803 12.5 14.2 7.2 7.4 7.1 7.2 27.00 <0.1 155.2 5.7 264 6.803 12.5 14.3 7.3 7.4 7.1 7.2 27.00 <0.1 247.6 88 6.220 12.5 14.3 6.9 7.4 7.1 7.1 34.00 <0.1 247.6 3.9 276 6.021 12.9 14.3 6.9 7.4 7.1 7.1 34.00 <0.1 272.9 8.6 204 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 223.9 3.2 376 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2	6 204 12.5 1.2 7.3 7.2 7.3 7.2 7.3 7.4 7.2 7.3 7.0 <0.1 214.9 5.6 412 6.803 12.5 14.7 7.3 7.4 7.2 7.3 17.00 <0.1	24	-	6.913	12 B	14.7	7.3	5.7	7.2	7.2	00.09	<0.1	368.9	6.4	044	3.8
6.803 12.5 14.2 7.2 7.4 7.2 7.2 9.00 <0.1 155.2 5.7 264 5.949 12.4 13.8 7.3 7.4 7.1 7.2 27.00 <0.1 6.220 12.5 14.3 7.3 7.4 7.1 32.00 <0.1 6.021 12.9 14.3 6.9 7.4 7.1 34.00 <0.1 6.021 12.9 14.3 6.9 7.4 7.1 24.00 <0.1 7.1 34.00 <0.1 272.9 8.6 204 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 223.9 3.2 376 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2	6.803 12.5 14.2 1.3 1.4 1.2 1.3 17.00 <0.1 155.2 5.7 264 5.949 12.4 13.8 7.3 7.4 7.2 7.2 9.00 <0.1	25	15	6.204	12.5	747	7.7	0.7	7.5	7.3	52.00	<0.1	214.9	5.6	412	2.8
5.949 12.4 1.2 1.4 1.2 1.2 9.00 <0.1 88 6.220 12.4 13.8 7.3 7.4 7.1 7.2 27.00 <0.1	5.949 12.4 1.2 1.4 1.2 1.2 9.00 <0.1 88 88 6.220 12.4 13.8 7.3 7.4 7.1 7.2 27.00 <0.1	26	3	6.803	12.5	14.2	5.7	1.4	7.7	6.3	17.00	<0.1	155.2	5.7	264	3.2
6.220 12.5 14.3 7.3 7.4 7.0 7.1 32.00 <0.1 247.6 240 6.021 12.9 14.3 6.9 7.4 7.1 32.00 <0.1 247.6 3.9 240 5.572 13.0 15.2 7.3 7.4 7.1 7.2 34.00 <0.1 247.6 3.9 276 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 223.9 8.6 204 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2	6.220 12.5 14.3 7.3 7.4 7.0 7.1 32.00 <0.1 247.6 240 6.021 12.9 14.3 6.9 7.4 7.1 7.1 34.00 <0.1	27	7	5.949	12.4	13.8	7.3	4.7	7.7	7.2	9.00	<0.1			88	2.2
6.021 12.9 14.3 6.9 7.4 7.1 32.00 <0.1 247.6 3.9 240 5.572 13.0 15.2 7.3 7.4 7.1 7.2 34.00 <0.1 247.6 3.9 276 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 272.9 8.6 204 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2	6.021 12.9 14.3 6.9 7.4 7.1 32.00 <0.1 247.6 3.9 240 5.572 13.0 15.2 7.3 7.4 7.1 7.2 34.00 <0.1 272.9 8.6 204 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 272.9 8.6 204 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min max max max 96.9% 522.6 98.0%	28	8	6.220	12.5	14.3	5.7	1.4	- 1	7.7	27.00	<0.1			260	2.6
5.572 13.0 15.2 7.3 7.4 7.1 34.00 <0.1 247.6 3.9 276 9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 223.9 3.2 376 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min	5.572 13.0 15.2 7.3 7.4 7.1 7.2 34.00 <0.1 247.6 3.9 276 9.346 13.1 15.2 7.3 6.9 7.1 24.00 <0.1	29	6	6.021	12.9		3.7	1.4	7.0	7.1	32.00	<0.1			240	2.2
9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 272.9 8.6 204 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max	9.346 13.1 15.6 7.2 7.3 6.9 7.1 24.00 <0.1 272.9 8.6 204 10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min max max max 96.9% 522.6 98.0%	30		5.572			7.3	1.4	1.1	7.7	34.00	<0.1	247.6	3.9	276	3.2
10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max mi	10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min max min max max 96.9% 522.6 98.0%	31		9.346	13.1		1.5	1.4	- 0	7.7	34.00	<0.1	272.9	8.6	204	5.0
10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min max	10.156 12.3 13.8 6.6 7.5 6.5 7.4 70.0 0.0 214.9 6.7 290.2 Monthly ave. ave. min max min max max 96.9% 522.6 98.0%					2	7.1	3.		1.7	24.00	<0.1	223.9	3.2	376	1.4
ave. ave. min max min may 214.3	ave. ave. min max min max max 96.9% 522.6 98.0%	AVER	1 1	10.156	.12.3	13.8	9.9	7.5	6.5	7.4	70.0	C	244.0	7.3	2000	C
				Monthly	ave.	ave.	min	max	E C	200	2.5	2.	214.3	0.7	730.7	5.9

	COMMENIS																																				
1001	1.00E	111001	00		က	3				0	>				Ľ	>	000	707	·	200	2				3		8	е				14		3		5.0	
IAIIG	AVF ma/I	0.67	200	1.28	1.22	1.08	1.31	1.26	1 16	130	0.58	0.56	79.0	0.98	1 10	0.47	4	200	4 47	7.07	40.	1.07	1.08	0.87	1.25	1.14	1.06	0.98	0.60	0.47	0.55	0.30	1,41	1.57		1.57	
CHLORINE RESIDITAL	MAX ma/l	1 20	175	0.73	1.40	1.15	1.41	1,44	1.38	151	0.64	0.67	1.32	1.35	142	0.62	1 33	121	1 63	1.03	t C.	70.1	1.33	0.97	1.47	1.21	1.16	1.16	1.04	1.30	0.73	0.50	1.52	1.80		1.80	+
CHLOR	MIN.mg/l MAX.mg/l AVE mg/l	0.40	140	54.0	1.03	0.95	1.20	1.12	1.00	1.08	0.48	0.50	0.45	0.73	0.81	0.24	0 73	0.55	135	200	200	0.00	0.79	0.80	0.95	1.08	0.86	0.84	0.32	0.00	0.35	0.19	1.21	1.45		0.00	-
OROUS	EFF,mg/l	0.46	0.73	5 0	64.0	0.57	0.75	09.0		0.62	0.65	0.57	0.52	0.63	0.62		0.51	0.31	0.45	0.30	0.57	20.0	ţ.	01	0.79	46.0	1.05	0.97	1.05	1.13		1.28	1.24	0.99		0.69	המה
PHOSPH(INF,mg/I	+	3.63	8.70	2 6	3.82	7.02	6.63		4.76	7.33	6.86	7.02	5.89	6.98		4.17	6.75	2.42	2.18	5 92	6 27	0.21	1007	12.01	7.88	2.88	5.18	3.39	4.76		6.55	4.84	6.83		6.04	
	FLOW	8.564	4.657	8 800	7 000	7.093	9.023	7.688	7.703	8.828	11.268	10.098	7.648	10.177	21.770	31.769	18.776	13,641	13.949	12.636	11,346	9.266	10 323	0 200	7 725	6,1.7	0.913	0.204	5.8U3	5.949	6.220	6.021	5.572	9.346		10.156	
	DATE	-	2	3	A	1	o o	9	<u> </u>	8	6	10	11	12	13	14	15	16	17	18	19	20	23	22	23	200	75	67	07	17	87	67	300	5	A1177	AVEKAGE	
	DAY	≥	—	Ш	U,	U	2	≥	-	Μ	L	1 (y)	S	2	-	}	-	ш.	S	ഗ	Σ	-	\ <u>\</u>	: -	- L	_ 0	0	2	ΣF	- 8	^^ F	- L	L			•

NIAGARA COUNTY SEWER DISTRICT #1 7346 LIBEI SPDES # NY-0027979 Jun-02 NIAGARA

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

-		7		I EIMPERATORE,C	Ę	E	H	ī		SOI IDS 1HP	0	0000	נונונו	000
DAY	DATE	FLOW	HN.	EFF	INF. MIN	INF MAX	H	FEE MAY	ING	בונים, וווא	ב בו	200	S ASDS	
S	-	7.610	12.5	16.2	7.4	74		7.7	ı	ErF,min	INF, mg/I	EFF,mg/I	INF,mg/I	出
တ	7	6.173	12.4	15.0	73	1	1.1	7.7	3	<0.1	285.3	5.4	464	2.2
Σ	0	5.430	12.5	146	7.5	1.1	1.0	1.1	24.0	<0.1			340	1.4
 -	4	6 432	128	0.4	1.7	4.7	0.7	(.1	24.0	<0.1			340	0.8
	ιΩ	10 582	42.7	3.5	1.0	9./	7.0	7.4	33.0	<0.1			300	20
-	9	8 837	128	70.0	7.3	7.4	7.1	7.2	34.0	<0.1	295.7	4.2	388	3.4
ш	7	6 782	120	10.1	7.2	7.4	7.0	7.1	28.0	<0.1	267.0	3.3	244	30
v.	. α	5070	0 2	1.0	7.7	7.4	7.2	7.2	28.0	¢0.1	146.2	3.0	200	ν α
S	0	5.073	77.0	16.6	7.2	7.3	7.1	7.2	30.0	<0.1	197.4	06	256	3.5
Z	3	7.301	27.9	16.4	7.0	7.3	7.0	7.1	34.0	<0.1			284	7.0
	2 7	4.0.4	13.0	16.8	7.1	7.4	6.9	7.1	14.0	×0.1			200	7 0
- >	12	6.307	13.3	17.6	7.2	7.4	7.2	7.3	28.0	<0.1			218	7.7
-	45	4.730	13.1	18.2	7.4	7.4	7.1	7.3	10.0	<0.1	173.0	27	450	0.0
-	2	4.979	13.0	17.7	7.3	7.3	7.1	7.2	27.0	<0 ×	161.0	000	700	0.0
_ 0	‡ L	5.184	12.9	17.2	7.1	7.3	7.1	7.1	33.0	× 0.3	218 8	2.0	477	Σ.
0 0	Ω (5.699	12.9	17.1	7.1	7.3	7.0	72	30.0	5 6	250.0	4,1	727	0.1
0	9!	5.702	12.8	17.0	7.1	7.2	7.1	7.4	22.0		203.0	1.)	877	1.2
≥ }	\[\frac{1}{1}\]	11.085	12.9	16.4	6.8	7.1	6.9	7.2	37.5				215	1.2
- - :	18	12.743	12.6	14.6	6.9	74	7.0	7.0	27.7	7			388	10.4
<u>-</u>	19	8.632	13.3	16.6	7.1	73	7.0	7.1	2.5	70,1			216	10.5
 	20	8.567	13.8	17.2	7.2	7.2	7.7	- 01	21.0	<0.1	147.1	5.1	196	8.3
ш	21	6.316	13.9	17.5	4 0	7.3	- '	7.7	23.0	<0.1	145.8	1.7	228	9.0
S	22	7.310	13.4	18.3	7.0	S. 7	0.0	6.7	26.0	<0.1	197.9	2.0	360	1.4
S	23	5.997	13.6	1000	200	7.0	0.7	7.0	35.0	<0.1	250.5	22.8	268	2.2
Y	24	5,155	14.1	78.0	0.0	0.7	0.0	0.7	34.0	<0.1			228	9.0
-	25	5.658	14.1	18.5	0.6	4.7	0.7	7.1	21.0	<0.1			120	2.6
3	26	4.801	14.5	10.7	7.7	7.7	0.7	7.3	35.0	<0.1			348	5.0
<u> </u>	27	5 729	45.4	707	7.7	7.5		7.7	35.0	<0.1	249.9	15.6	340	2.4
 	28	7 090	17.3	10.7	- 0	۶۰,۱	/.1	7.3	21.0	<0.1	221.5	19.4	252	3.0
S	29	5 066	17.5	0.0	6.0	7.7	7.0	7.1	24.0	<0.1	164.6	4.1	168	6.0
S	30	4 282	17.0		1.	5.7	6.9	7.2	20.0	<0.1			212	3.2
		707:	P. F.	(3.0	0./	4./	7.0	7.2	23.0	<0.1			216	2.0
A	AVERAGE	6.657	13.4	17.2	6.8	7.6	6.6	7.4	35.0	c	0.050	1		
		Monthly	ave.	ave	3.			•	0.00	0.0	7.13.0	? .	266.9	3.6
										-			The state of the s	

California	COMMENS																																		
1001	/ 100 ml	200	>			3)	4	2 "	>			44	•	C.	2 (4	2					m	124	-				41		2)	33			9.9	38.4
IDIIAI	MIN.mg/I MAX.mg/I AVE mg/I	163	140	1.56	1.62	1 22	101	1.18	2 7	1.26	1 17	0 04	0.48	0.93	1 13	800	0.50	0.00	- 0.0	0.93	1.07	1.06	0.75	0.22	0.66	0.93	1.13	0.32	0.18	14.	1.14	0.46		1.63	
CHI ORINE RESIDITAL	MAX.ma/l	191	150	181	1 73	1.35	130	140	1.50	1.58	139	0.98	0.91	1.10	72	1.25	06.0	1 13	101	1.2.1	1.0.1	1.23	1.5.1	0.24	0	0	10.0	0.00	0.27	4.55	50.1	0.57		2.28	
CHIO	MIN,mg/I	1.45	1.30	1.36	147	111	0.67	26.0	0.58	0.94	1.01	0.92	0.06	0.73	0.86	0.66	0.83	0.62	0.87	00.0	0.90	10.00	5.0	0.20	0.20	0.70	0 0	3 6	0.00	0.13	0.0	0.40		0.00	
IOROUS	EFF,mg/I	0.80	0.68	1.05		0.87	0.50	0.38	0.50	0.56	0.67		1.17	1.21	0.91	0.66	0.52	0.61		0.45	0.48	0.40	70.7	0.70	0.10 58	3	0.84	0.01	0.00	0.45	0,00	0.40	1	0.67	36.3
PHOSPH	INF,mg/I	10.18	3.20	8.77		8.81	3.78	4.41	2.93	3.86	6.66		5.53	3.59	4.13	10.14	3.54	7.44		2.37	2.53	7.56	257	15.99	3 97		4 09	4 60	3.82	4.57	377	t	E 40	5.0	
	FLOW	7.610	6.173	5.430	6.432	10.582	8.837	6.782	5.873	5.981	4.974	6.307	4.730	4.979	5.184	5.699	5.702	11.085	12.743	8.632	8.567	6.316	7310	5.997	5,155	5.658	4.801	5.729	7.090	5.066	4 282	707:	E 657	100.0	
	DATE	-	2	က	4	2	9	7	80	o,	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	3	
	DAY	S	တ	Σ	⊢	8	⊢	LL	S	တ	Σ	-	3		LL	S	S	Σ	<u>-</u>	>	F	ш	S	S	Σ	 	≥	⊢	ட	S	S				

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-8759 FAX CERT. 4A

			TEMPERATURE	ATURE,C	Hd	Ha	Ha	Ha	SETT SO	SOI IDS 1HR	Cao	00	0 0010	001 100
DAY:	DATE	FLOW	INF	EFF	INF, MIN	INF, MAX	EFF, MIN	EFF, MIN EFF, MAX	1 1	EFF.ml/I	INF ma/I	FFF mu/I	INF ma/I	FEE ma/l
2		4.670	14.7	19.4	7.1	7.3	6.7	7.3	25.00	\$0.4	,		220	200
- :	2	4.363	14.7	20.1	7.2	7.3	7.1	7.3	24 00	<0.1			17E	2.0
≥	m	4.428	15.0	20.0	7.1	7.3	7.2	7.4	24.00	×0.1	2072	7.0	277	17.0
_ _	4	4.211	15.1	20.6	7.2	7.2	7.4	7.4	22.00	<0.1	266.8	0.8	224	46
_ C	Ω	4.293	16.4	20.0	7.2	7.4	7.3	7.5	21.00	<0.1	223.0	6.0	352	2.0
n c	1 0	3.812	16.1	20.2	7.1	7.3	7.4	7.5	16.00	<0.1	215.3	20	184	200
0		4.278	16.1	19.8	7.0	7.2	7.0	7.4	17.00	<0.1			144	7 10
Σŀ	0	4.905	16.1	21.8	7.0	7.1	6.8	7.3	14.00	\$0.1			27R	ο
	δ ,	3.903	16.4	19.9	6.9	7.4	7.1	7.5	13.00	\$0.1			124	2.4
> F	10	4.197	16.3	19.8	7.3	7.4	7.2	7.5	21.00	<0.1	237.5	27	256	2.7
- L	11	4.490	16.4	20.4	7.0	7.3	7.2	7.4	21.00	¢0.1	253.4	2	256	1 6
۲ (12	4.905	16.1	19.8	7.2	7.3	7.1	7.3	21.00	\$0.1	226.4	43	208	2, 4
ח	13	4.613	15.4	19.8	7.0	7.1	7.1	7.2	25.00	<0.1)	240	0.0
s) :	14	4.584	15.7	20.1	6.9	7.2	7.0	7.2	26.00	\$0.1			252	2.4
ΣΙ	15	4.901	15.9	20.1	6.8	7.1	7.0	7.1	23.00	\$0.4			180	7.0
-	16	4.715	16.4	20.1	7.0	7.1	6.5	7.1	24.00	¢0.1			244	ן ע
≥	1/	4.929	16.4	20.9	6.9	7.1	6.6	7.1	18.00	<0.1	183.9	2.0	208	2.5
- 1	18	4.342	16.7	23.2	6.4	7.4	6.8	7.1	15.00	V0 1			316	3.2
1 0	19	4.191	18.1	21.7	7.0	7.2	6.6	7.1	17.00	<0.1	184.2	7.6	2,00	2.6
S	20	4.102	18.1	21.3	6.8	7.1	6.9	7.1	14.00	<0.1	191.0	ָר ל. ד	196	ο α α
S)	21	4.122	17.1	21.0	6.5	7.0	66	7.0	13.00	20.4	2:10	-	25.0	0.0
Σ	22	4.550	17.4	21.0	7.0	7.4	6.9	7.2	28.00	100			727	4. 4
-	23	5.664	17.4	21.4	6.5	6.7	6.5	99	21.00	0,00			047	7.4
8	24	4.927	17.4	20.7	6.7	7.3	89	7.1	28.00	7	277.E	17.0	107	0,0
-	25	8.959	17.4	20.6	7.2	7.3	7.0	7.2	14.00	\$ C	174.0	0.1.0	220	7.0
т (26	4.652	17.1	20.9	7.1	7.3	7.0	7.2	21 00	\$0.1	255.4	2.2	180	0.0
מי	27	5.021	17.1	21.4	7.3	7.3	6.8	73	17.50	<0.1	1007	2,7	270	0.7
S	28	5.591	17.4	21.5	7.2	7.4	7.1	7.3	24 00	5 0	200	t l	180	5.2
2	29	7.132	17.1	21.6	7.1	7.3	6.7	7.1	24.00	×0.1			24.0	t o
-	30	6.723	17.2	21.1	7.1	7.2		7.1	24.50	\$ 0			212	2.4
>	31	5.497	17.1	20.7	6.8	7.1	69	7.1	19.00	¢0.1	158.1	17	248	
	ALUTDA												2	-
	AVERAGE	- 1	16.5	20.7	6.4	7.4	6.5	7.5	28.0	0.0	206.7	4.7	227.7	3.4
		Monthly	ave.	ave.	min	тах	min	max	max	тах	97.7%	191.4	98.5%	134.5

COMMENTS	STATISTICS																													The state of the s						
F.COI I	/ 100 ml	111001		7)				m		Cr.	0 60	>					0	0	3				3		33	က				3		3.2	
DUAL	AVF ma/I	0.33	0.22	0.46	0.24	0.49	0.30	0.34	0.45	0.82	1.19	117	1 16	1 16	1.16	1 44	107	080	0.03	200	0.22	0.50	0.44	0.27	0.30	0.73	7.07	1.10	1.20	1.24	1.25	1.09	1.18		1.44	
CHLORINE RESIDUAL	MIN.mg/I MAX mg/II AVE mg/I	0.51	0.45	0.68	0.57	0.73	0.47	0.45	0.95	1.02	1.82	1.38	1.21	131	136	165	120	0.07	25.0	220	0.0	0.70	0.50	0.32	0.07	4. 6	60.1	77.1	1.33	1.35	1.36	1.18	1.30		1.82	
CHLOF	MIN.ma/I	0.07	00.0	0.29	0.00	0.15	0.07	0.17	0.20	0.72	0.74	1.05	1.10	1.05	0.82	1.26	0.94	0.76	0.70	0.12	1 6	2 5	0.40	0.20	0.20	30.00	10.92	- 1	1.05	1.09	1.12	1.02	1.06		0.00	
OROUS	EFF.ma/l	0.39		0.75	0.51	0.63	0.80	0.82	0.76		0.67	0.66	0.61	1.34	0.92	0.79		0.87	0.86	0.81	08.0	0.00	0.10	0.0	0.67	0.07	0.00	0.00	0.65	0.83	0.93		0.73		0.75	
PHOSPH	INF,mg/I			3.59	6.40	8.66	3.78	27.26	5.03		12.51	4.60	4.80	6.08	4.21	4.17		4.79	4.79	9.43	4.68	3.20	503	3	176	4.17	4.10	7 70	0,70	3.35	4.72		4.79		6.01	٠.
	FLOW	4.670	4.363	4.428	4.211	4.293	3.812	4.278	4.905	3.903	4.197	4.490	4.905	4.613	4.584	4.901	4.715	4.929	4.342	4.191	4 102	4 122	4 550	5.664	4 027	8 959	4 652	700 Y	3.021	0.081	7.132	6.723	5,497		4.893	_
	DATE	-	2	က	4	3	9	7	6 0	6	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	07	67	30	31		AVERAGE	•
	DAY	Σ	⊢	≯	F	ш.	S	S	Σ	-	>	-	ш	S	တ	Σ		>	F	上	S	S	Σ	-	M	-	Ш	U.	U) 2	Σŀ	-	A		1	

Mary Websel

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Aug-02

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

FRANK A. Nerone, P.E. CERT. 4A 716-693-0001 716-693-8759 FAX

3	4		TEMPERATURE	ATURE,C	ЬH	hd	Hd	Hd	SETT SOI	SOLIDS,1HR	CB	CBOD	SUSP	SOLIDS
LAY.	DAIE	FLOW	본	EFF	INF, MIN	INF, MAX	EFF, MIN	出	INF,n	EFF,m//	INF,ma/I	EFF.ma/l	INF.ma/I	EFF ma/l
- -		4.273	18.1	21.1	6.8	7.3	6.8		17.00	<0.1	213.5	15.2	177	24
L C	7	5.186	17.7	21.4	6.6	7.2	6.7	7.1	19.00	<0.1	258.9	0.0	396	
0	v) <	4.030	17.7	21.3	6.7	6.9	6.5	6.8	19.00	<0.1	177.4	1.0	248	2.0
0 2	1 և	3.646	18.1	21.3	6.8	7.1	6.6	6.8	23.00	<0.1			260	5.4
Ĕŀ	0 4	4.221	18.4	21.8	6.6	7.0	6.7	7.0	25.00	<0.1			228	1.0
- }	7 0	3.534	17.9	21.1	7.0	7.8	7.1	7.6	25.00	<0.1			192	18
} ⊦		3.543	18.1	21.5	7.3	7.7	7.0	7.6	26.00	<0.1			268	24
_ L	ρ	3.477		21.3	7.2	7.3	7.0	7.1	28.00	<0.1	296.6	23	296	24
_ 0	co Ç	3.619		21.5	7.0	7.4	7.0	7.2	19.00	<0.1	250.7	1.6	236	46
0	2	3.052		21.5	6.9	7.2	7.0	7.1	19.00	<0.1	327.7	3.5	224	28
0 2	- 0	4.258	18.4	21.9	7.0	7.3	6.8	6.9	30.00	<0.1		1.7	204	1.8
Σ Γ	7 0	3.0/3		22.5	7.1	7.3	6.9	7.1	25.00	<0.1			208	2.8
- 2	2	4.238		21.7	6.9	7.3	7.1	7.2	18.00	<0.1			244	14
> F	14	3.9/6	[21.4	7.1	7.2	6.9	7.1	24.00	<0.1			220	0.6
- L	0	3.892		21.5	7.3	7.4	6.9	7.1	19.00	<0.1	331.8	3.4	228	16
LO	10	3.597		22.2.	7.3	7.4	7.0	7.1	21.00	<0.1	226.4	2.6	216	5.2
0	707	3.711		22.1	7.4	7.5	7.1	7.2	21.00	<0.1	224.7	3.3	204	1.2
2	0 5	3.340	1	21.9	7.0	7.2	6.9	7.0	29.00	<0.1			240	0.4
≅ ⊦	2 6	3.976		21.3	7.1	7.2	6.8	7.0	31.00	<0.1			220	0.8
-	22	3.262		20.9	6.8	7.2	7.0	7.3	22.00	<0.1			196	2.4
> -	7 20	3.327		20.9	7.1	7.2	7.0	7.4	21.00	<0.1	209.8	2.5	152	1,6
_	77	3.003	1	21.6	7.1	7.3	7.0	7.2	26.00	<0.1	217.9	3.1	236	3.2
_ 0	200	3.000	18.5	21.8	7.1	7.3	7.1	7.1	26.00	<0.1	209.8	4.9	216	1.4
ט כ	25	3.919		22.4	7.3	7.5	6.9	7.2	29.50	<0.1	136.9	11.8	228	2.2
>	30	2.003		21.0	5.7	7.4	7.0	7.1	32.00	<0.1			256	1.8
<u> </u>	27	0.470	10.7	21.8	.:	7.3	7.0	7.3	24.00	<0.1			256	2.6
M	780	3.007	0.0	21.4	6.8	7.3	7.0	7.2	31.00	<0.1			284	2.0
}	700	7.730	18./	21.4	7.2	7.3	7.0	7.2	24.00	<0.1	185.2	0.8	228	2.0
- 1	200	3.542	18.	21.4	7.2	7.5	7.0	7.1	29.00	<0.1	251.1	2.0	244	2.4
_ 0	00	3.170	18.4	21.7	7.1	7.3	6.9	7.1	21.00	<0.1	432.5	3.7	276	2.8
0	0	3.208	18.4	22.4	7.2	7.3	7.1	7.1	28.00	<0.1	241.8		260	9.8
	AVERAGE	2 600	70.0	2										
	שארואפור	0.030	10.3	21.6	6.6	7.8	6.5	7.6	32.0	0.0	243.7	3.9	236.6	2.5
		Monthly	ave.	ave.	mim.	шах	min	шах	тах	max	98.4%	120.7	98.9%	7.77

<u>5.</u>	2																	the state of the s													The state of the s		
STNEWMOO																			-						4444						100000000000000000000000000000000000000		
F.COLI	/ 100 ml		141	3200						3	6				3		3	3				3		3	8				3		3	2300	
JUAL	AVE ma/I	1 15	0.57	0.51	1.21	0.91	1.79	1.55	1.61	1.21	1.59	1.28	1.32	1.28	1.20	1.52	1.20	0.58	0.27	0.29	0.43	1.23	1.29	1.13	96.0	1.19	1.17	26.0	0.86	0.91	0.95	0.78	
CHLORINE RESIDUAL	MAX.ma/I	1.26	0.80	0.84	1.34	0.98	2.35	2.04	1.86	1.45	1.76	1.54	1.51	1.60	1.37	1.62	1.40	0.98	0.34	0.39	1.10	1.33	1.37	1.31	1.15	1.37	1.30	1.05	0.94	1.01	1.05	0.97	L
CHLOR	MIN.mg/ MAX.mg/ AVF mg/	1.03	0.25	0.09	1.00	0.82	1.05	1.29	1.32	0.93	1.49	0.85	1.17	0.85	1.02	1.39	0.89	0.32	0.22	0.20	0.00	1.15	1.23	0.84	0.77	0.86	1.10	0.87	0.77	0.81	0.82	0.49	000
OROUS	EFF.mg/I	0.61	0.65	0.62	0.82	0.89		0.99	0.89	0.86	0.78	0.80	0.73		0.68	0.63	0.72	08.0	0.71	0.61		0.55	0.64	1.18	1.00	0.69	0.73		0.92	0.89	0.71	0.64	77.0
PHOSPHO	INF,mg/I	2.88	3.04	3.31	4.71	4.72		4.56	6.05	3.86	3.87	4.83	4.79		1.63	1.91	2.81	2.92	7.37	3.94		2.96	7.25	4.88	4.28	4.48	4.64		5.26	5.93	5.62	1.87	V 2.V
	FLOW	4.273	5.186	4.030	3.646	4.227	3.594	3.543	3.477	3.619	3.052	4.258	3.675	4.238	3.976	3.892	3.597	3.711	3.546	3.916	3.262	3.327	3.603	3.060	3.919	3.603	3.470	3.067	4.250	3.542	3.176	3.208	3 600
	DATE	1	2	က	4	S)	9	7	œ	တ	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	52	26	27	28	29	30	31	AVERAGE
	DAY	⊢	ш	S	S	Σ	F	≥		Ш	တ	S	Σ	-	8	-	Щ	S	တ	Σ	-	8		4	တ	מ	Σ	- :	3	-	T 0	n	

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

FRANK A. Nerone, P.E. CERT. 4A 716-693-0001 716-693-8759 FAX

FLOW INF 3.763 18.4 3.763 18.4 4.304 18.4 4.304 18.4 4.012 18.4 4.002 18.4 4.461 18.4 4.461 18.4 4.461 18.4 5.678 19.4 3.503 18.7 4.356 18.4 3.571 18.4 3.571 18.4 3.870 17.1 3.815 17.8 4.048 19.1 4.048 19.1 4.048 19.1 4.051 18.5 4.689 17.8 4.689 17.8 4.469 17.8 4.469 17.8 4.469 17.8 4.469 17.8 4.469 17.8 4.689 17.8 4.689 17.8 4.689 17.8 4.689 17.8 4.689 17.4 4.689 17.8 4.689 17.8 4.689 17.4 4.689 17.4	EFF INF, MIN 18.4 7.1 22.7 7.1 22.9 7.3 22.9 7.2 22.9 7.1 22.9 7.1 22.0 7.1 22.1 7.1 22.8 7.1 22.8 7.1 22.8 7.1 22.0 7.1 22.0 7.1 22.0 7.1 22.0 7.1 22.0 7.1 22.0 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.2 7.3 22.3 7.3 7.3 7.3 <	1NF, MAX 7.4 7.3	EFF, MIN	FFF MAX	INF mill FFF mill	EFF ml/	INE man EE	FFF ma/l		
18.4 18.4 18.4 18.4 18.4 19.7 19.7 19.7 19.7 19.7 19.7 19.7 19.7		7.4	-			-]	NE may	EFF ma/l
18.4 18.4 18.4 18.4 18.4 19.7 19.7 19.1 19.1 19.1 19.1 19.1 19.1		7.3	7.1	7.2	23	<0.1			284	22
18.4 18.4 18.4 18.4 19.7 19.7 19.7 19.4 19.4 19.1 19.1 19.1 19.1 19.1 19.1		2	7.0	7.1	21.0	<0.1			216	2.0
18.4 18.4 18.4 19.7 19.7 19.7 19.7 19.4 19.1 19.1 19.1 19.1 19.1 19.1 19.1		7.4	6.9	7.1	21.0	<0.1			396	22
18.4 18.4 18.4 19.7 19.7 19.7 19.4 18.4 19.4 19.4 19.4 19.4 19.1 19.4 19.4 19		7.1	6.9	7.3	14.5	<0.1	250.8	1.8	244	1.2
18.4 18.4 19.4 19.7 19.4 19.4 19.4 19.4 19.4 19.4 19.4 19.4		7.3	6.9	7.0	23.0	<0.1	170.6	3.5	160	1.1
18.4 19.4 19.4 19.4 19.4 19.4 19.4 19.1 19.1		7.3	6.9	7.2	22.5	<0.1	145.9	2.3	168	13
18.4 19.7 19.7 19.7 19.7 19.7 19.7 19.7 19.7		7.3	6.9	7.1	24.0	<0.1	226.8	2.2	268	90
18.7 19.4 19.4 19.4 18.7 17.8 19.4 19.1 19.1 19.1 19.1 19.1 19.1 19.1		7.3	6.7	7.1	22.0	<0.1			236	16
19.7 19.7 19.7 18.4 18.4 18.4 19.1 19.1 19.1 19.1 19.1 19.1 19.1 19		7.4	6.9	7.3	22.0	<0.1			212	2.2
19.7 19.4 19.4 18.7 17.1 17.8 19.4 19.1 19.1 18.5 18.5 18.5 18.5 18.5 18.5 18.5 18		7.1	6.8	7.0	22.0	<0.1			232	13
19.4 19.4 18.4 18.4 19.4 19.4 19.1 19.1 18.5 18.5 18.5 18.5 18.5 18.5 18.5 18		7.4	6.8	7.0	23.0	<0.1	229.1	3.2	248	10
19.1 18.7 18.4 18.4 19.4 19.1 19.1 18.5 18.5 18.5 17.8 17.8 17.8 17.8 17.8 17.8	-	7.4	6.7	7.1	20.0	<0.1	137.3	2.4	192	0.4
18.7 18.4 18.4 17.1 19.4 19.4 19.1 18.5 18.5 17.8 17.8 17.8 17.8 17.8 17.8		7.4	6.8	7.5	24.0	<0.1	135.1	3.4	304	3.0
18.4 18.4 17.1 17.8 19.4 19.4 19.1 19.1 18.5 18.5 17.8 17.8 17.8		7.3	6.7	6.8	24.0	<0.1	1733	18	212	2.0
18.4 17.1 17.8 19.4 19.4 19.1 19.1 18.5 17.8 17.8 17.8		7.3	6.8	6.8	22.0	<0.1)	240	2.2
18.1 17.1 17.8 19.4 19.1 19.1 18.5 18.5 17.8 17.8 17.4		7.4	6.8	7.1	22.0	<0.1			264	2.0
17.1 17.8 18.4 19.1 19.1 18.5 18.5 17.8 17.8		7.3	6.7	7.0	23.0	<0.1			296	20
17.8 18.4 19.1 19.1 18.5 18.5 17.8 17.8	22.7 7.2	7.4	7.0	7.1	20.0	<0.1	149.1	14	404	10
18.4 19.4 19.1 19.1 18.5 18.5 17.8 17.8 17.8		7.3	6.9	7.2	24.0	<0.1	140.8	22	228	2.5
19.1 19.1 19.1 18.5 18.5 17.8 17.8 17.8	-	7.3	6.8	7.0	24.0	<0.1	199.3	1,4	224	12
19.4 19.1 18.1 18.1 17.8 17.8 17.8	24.1 7.3	7.5	7.0	7.2	22.0	<0.1	193.2	1.7	204	14
19.1 18.5 18.4 17.8 17.4 18.1		7.3	6.8	7.0	19.0	<0.1			248	3.6
19.1 18.5 18.4 17.8 17.4 18.1	23.1 7.2	7.3	6.7	7.0	22.0	<0.1			192	2.2
18.5 18.4 17.8 17.4 17.4		7.3	6.8	7.0	24.0	<0.1			316	14
18.1 17.8 17.4 17.4	23.1 7.0	7.4	6.9	7.1	21.0	<0.1	176.5	2.5	248	18
18.4 17.8 17.4 18.1	21.8 7.3	7.4	7.0	7.1	19.0	<0.1	183.7	3.5	202	1.6
17.8		7.4	7.1	7.2	27.0	<0.1	130.2	23	320	2.0
17.4	19.3 7.2	7.4	6.8	7.2	21.0	¢0.1	283.0	2.0	364	2.2
18.1		7.4	6.9	6.9	15.0	<0.1		i	264	2.0
	21.1 7.2	7.2	6.9	6.9	21.0	<0.1			148	2.0
i d	-									i
3 18.5	22.3 6.6	7.5	6.7	7.5	27.0	0.0	185.6	2.4	252.8	1.9
Monthly ave. a	ave. min	max	min	тах	тах	max	98.7%	88.8	99.2%	68.8

FRANK A. NERONE

COMMENTS	COMMENT						- Approximate the second secon																1949										interpretation can be a second of the second	
FCOLL	/ 100 ml				8		3	3				8		K	6				6.)	124	m)			m		3	3)			4.1	10.4
OUAL	AVE.ma/I	1.07	0.97	0.98	0.83	0.95	0.75	0.99	1.31	42.	1.21	1.47	1.35	0.92	0.95	0.93	111	1.10	0.82	26.0	0.86	1.10	0.93	1.19	0.97	1.41	1.18	1.09	134	1 23	153	3	1.53	
CHLORINE RESIDUAL	MAX.mg/I AVE.mg/I	1.20	1.25	1.32	1.03	1.33	0.81	1.08	1.42	1.12	1.33	2.08	1.57	0.95	2	1.00	122	1.20	0.83	1.14	1.65	1.38	1.10	1.58	1.19	1.58	1.33	1.39	144	1.39	1.66		2.08	
CHLOR	MIN,mg/I		0.60	0.67	0.67	0.48	0.70	0.86	1.15	0.95	1.03	1.11	1.15	0.90	0.90	0.90	0.92	1.02	0.80	0.78	0.24	0.76	0.79	0.71	0.62	1.26	1.00	0.77	1.17	1.08	1.44		0.24	
OROUS	EFF,mg/I	┼	0.57		0.46	0.50	0.65	99.0	0.68	0.83		1.17	08.0	0.80	0.92	1.01	0.82		0.64	0.69	0.71	0.69	0.90	0.88		0.82	0.89	0.90	0.55	0.21	0.23		0.72	25.6
PHOSPH	INF,mg/I	20.71	3.78		8.42	5.69	11.11	5.15	17.35	16.84		12.51	6.75	4.99	5.56	10.14	5.07		6.78	10.37	5.69	7.72	5.12	3.12		2.38	5.97	7.64	5.88	5.14	2.10		7.24	
	FLOW	-	3.743	4.304	3.751	4.012	4.202	4.002	4.512	4.469	4.481	5.678	4.668	3.836	3.503	4.336	4.107	3.571	3.870	3.815	4.218	3.694	3.443	3.555	4.048	4.071	4.253	7.608	4.689	4.469	4.769		4.248	
	DATE	-	2	က	4	5	9	7	8	o	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
	DAY	S	Σ	 -	3	-	LL (S	S	Σ	-	3		Щ	S	S	Σ	H	≥	⊢	ш	တ	တ	Σ	-	8	H	L.	S	တ	Σ			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

DATE FLOW NK EFF NF,MIN NF,MAX EFF,MIN EFF,MIN EFF,MIN NF,MIN EFF,MIN NF,MIN				TEMPERATURE	ATURE,C	На	Ha	Ha	H	SETTSO	SOI IDS 1HP	2	CBOD	0.0000	001100
1	DAY	DATE	FLOW	HN.	EFF	INF, MIN	INF, MAX	EFF, MIN	EFF. MAX	N L	EFF ml/	INF ma/I	FEE ma/l		EEE mail
2 4.104 19.5 21.4 7.0 8.0 7.1 7.2 21.00 <0.01 4 4.288 19.2 21.0 7.4 7.4 7.4 25.50 <0.01	- :		4.022		21.1	7.0	7.3	7.0	7.2		<0.4 40.4			Mail, ivii	7.0
3 4.321 19.2 21.0 7.4 7.4 7.1 7.4 25.50 0.01 6 4.4268 19.1 20.7 7.2 7.2 6.8 7.1 22.00 <0.1	8	2	4.104		21.4	7.0	8.0	7.1	7.2	2100	507	106	0 0	200	7.0
4 4,268 19,1 20,7 7,2 7,2 6.6 7,1 22,00 <0,1 5 8,144 18,4 20,2 7,2 7,2 6,6 7,1 22,00 <0,1		8	4.321		21.0	7.4	7.4	7.1	7.4	25.50	20,00	- 20°-	7.0	700	7.1
5 8,144 19,4 21,3 7,2 7,3 7,0 7,1 22.00 40,1 7 3,945 18,5 20,7 7,2 7,2 6,9 7,0 23.00 40,1 8 4,107 18,1 20,2 7,2 7,5 6,9 7,0 25.00 40,1 9 3,524 19,0 19,3 7,3 7,3 6,8 7,2 25.00 40,1 10 3,678 18,5 20,0 7,3 6,9 7,0 23.00 40,1 11 3,678 18,5 20,0 7,3 6,9 7,0 23.00 40,1 12 4,523 20,0 21,4 7,2 7,3 6,9 7,0 7,1 27.00 40,1 14 3,978 18,0 21,4 7,2 7,4 7,0 7,1 27.00 40,1 16 5,730 18,2 7,2 7,4 7,0 7,1 27.00	L	4	4.268		20.7	7.2	7.2	8.9	7.1	22.00	0,0	477 E	1,4	700	7.1
6 3.945 18.5 20.7 7.2 7.2 6.9 7.0 23.00 40.1 7 3.469 18.9 20.2 7.3 7.5 6.8 7.0 25.00 40.1 8 3.524 19.0 19.3 7.3 7.5 6.8 7.0 25.00 40.1 10 3.678 18.9 20.0 7.3 7.5 6.9 7.0 23.00 40.1 11 3.678 18.5 20.7 7.0 7.3 6.9 7.0 23.00 40.1 12 3.678 18.9 20.0 7.3 7.4 7.0 23.00 40.1 13 3.795 18.3 7.0 7.4 7.1 7.1 27.00 40.1 14 3.960 18.3 7.2 7.4 7.0 7.1 27.00 40.1 16 4.222 18.5 19.1 7.3 7.4 7.0 7.1 27.0 40.0	S	5	8.144		21.3	7.2	7.3	7.0	7.1	22.00	7	242.0	3,0	00	- 0
7 3.469 18.9 20.2 7.3 7.5 6.8 7.0 25.00 40.1 8 4.107 19.1 20.1 7.2 7.4 6.8 7.0 25.00 40.1 10 3.678 18.9 20.0 7.3 7.5 6.9 7.0 21.00 40.1 11 3.978 18.5 20.7 7.0 7.3 6.9 7.0 21.00 40.1 12 3.786 19.0 21.3 7.0 7.3 6.9 7.0 21.00 40.1 14 3.960 18.3 20.0 21.3 7.0 7.3 6.9 7.0 21.00 40.1 14 3.960 18.7 19.1 7.2 7.4 7.0 7.1 27.0 6.0 15 4.222 18.5 19.1 7.3 7.4 7.0 7.1 20.0 6.0 18 8.389 18.0 18.9 7.2 7.4 <t< td=""><td>S</td><td>9</td><td>3.945</td><td>18.5</td><td>20.7</td><td>7.2</td><td>7.2</td><td>6.9</td><td>7.0</td><td>23.00</td><td>500</td><td>717.0</td><td>2.6</td><td>302</td><td>0.0</td></t<>	S	9	3.945	18.5	20.7	7.2	7.2	6.9	7.0	23.00	500	717.0	2.6	302	0.0
8 4.107 19.1 20.1 7.2 7.4 6.8 7.2 25.00 -0.1 19 3.524 19.0 19.3 7.3 7.3 6.8 7.2 25.00 -0.1 10 3.678 18.5 20.0 7.3 7.3 6.9 7.0 23.00 -0.1 12 4.523 20.0 21.3 7.0 7.3 6.9 7.0 23.00 -0.1 13 3.765 19.0 21.4 7.2 7.3 6.9 7.1 27.00 -0.1 14 4.523 20.0 21.3 7.0 7.3 6.9 7.1 27.00 -0.1 15 4.222 18.0 21.4 7.2 7.3 6.9 7.1 27.00 -0.1 16 5.730 18.7 7.2 7.4 7.1 7.1 27.00 -0.1 17 4.439 18.2 18.2 7.2 7.4 7.0 7.1	Σ	7	3.469	18.9	20.2	7.3	7.5	8 9	7.0	25.00				7/1	0.7
9 3,524 19.0 19.3 7.3 7.3 6.8 7.2 26.00 40.1 10 3,678 18.9 20.0 7.3 7.5 6.9 7.0 23.00 40.1 11 3,678 18.9 20.0 7.3 7.6 7.0 21.00 40.1 12 4,523 20.0 21.3 7.0 7.3 6.9 7.0 21.00 40.1 14 3,960 18.3 20.2 7.3 7.4 7.1 27.00 40.1 15 4,222 18.5 19.1 7.2 7.4 7.0 7.1 27.0 40.1 16 5,730 18.7 7.2 7.4 7.0 7.1 27.0 40.1 16 5,730 18.2 7.2 7.4 6.9 7.1 27.0 40.1 18 8.389 18.0 18.9 7.2 7.4 6.9 7.1 20.0 40.1 <td< td=""><td><u> </u>-</td><td>80</td><td>4.107</td><td>19.1</td><td>20.1</td><td>7.2</td><td>7.4</td><td>8 9</td><td>7.2</td><td>25.00</td><td></td><td></td><td></td><td>107</td><td>0,0</td></td<>	<u> </u> -	80	4.107	19.1	20.1	7.2	7.4	8 9	7.2	25.00				107	0,0
10 3678 18.9 20.0 7.3 7.5 6.9 7.0 25.00 C.1 1.2 3.978 18.5 20.7 7.0 7.3 6.9 7.0 25.00 C.1 1.2 3.978 18.5 20.7 7.0 7.3 6.9 7.0 25.00 C.1 1.3 3.785 19.0 21.4 7.2 7.3 6.9 7.1 27.0 25.00 C.1 1.4 3.960 18.3 20.2 7.3 7.4 7.0 7.1 27.0 C.1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1	≥	6	3.524		19.3	7.3	7.3	8 9	7.2	28.00		0 707	,	20,	0.5
11 3.978 18.5 20.7 7.0 7.3 6.9 7.0 23.00 c0.1 12 4.523 20.0 21.3 7.0 7.3 6.9 7.0 21.00 c0.1 13 3.795 18.0 21.4 7.2 7.3 7.4 7.1 27.00 c0.1 14 3.960 18.3 20.2 7.3 7.4 7.1 27.00 c0.1 15 4.222 18.5 19.1 7.3 7.4 7.0 7.2 20.00 c0.1 17 4.439 18.2 19.2 7.2 7.4 6.9 7.1 26.00 c0.1 18 8.389 18.0 18.9 7.2 7.4 6.9 7.1 26.00 c0.1 19 6.056 77.9 18.9 7.2 7.4 6.9 7.1 19.00 c0.1 20 5.032 17.5 18.5 7.2 7.4 6.9 7.1 19.00 c0.1 21 4.259 77.5 18.5 7.0 7.3 6.9 7.0 17.00 c0.1 22 4.348 77.5 18.5 7.0 7.3 6.9 7.0 17.00 c0.1 23 3.765 17.1 19.1 7.3 7.4 6.9 7.0 11.00 c0.1 24 4.906 17.0 18.9 7.2 7.4 6.9 7.0 11.00 c0.1 25 5.881 7.3 18.8 7.0 7.4 6.9 7.0 11.00 c0.1 26 4.906 17.0 18.0 7.1 7.4 6.9 7.0 11.00 c0.1 27 4.224 16.9 18.2 7.4 7.5 6.9 7.0 11.00 c0.1 28 4.646 16.8 18.1 7.1 7.4 6.9 7.0 15.00 c0.1 29 4.050 18.9 7.1 7.4 7.5 7.0 15.00 c0.1 29 4.050 18.9 7.2 7.4 7.5 7.0 15.00 c0.1 30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 c0.1 31 3.886 16.7 17.2 7.2 7.4 7.5 7.0 19.50 c0.1 31 3.886 16.7 17.2 7.2 7.4 7.7 7.1 22.00 c0.1 31 3.886 16.7 17.2 7.2 7.4 7.7 7.1 22.00 c0.1 31 3.886 16.7 17.2 7.2 7.4 7.7 7.1 22.00 c0.1	<u>-</u>	10	3.678		20.0	7.3	7.5	0.6	7.7	22.00	70.7	0.400	4.1	192	0.6
12 4,523 20.0 21.3 7.0 7.3 6.9 7.7 21.00 c0.1 1.4 23.96 19.0 21.4 7.2 7.3 7.0 7.1 27.00 c0.1 1.4 3.960 18.3 20.2 7.3 7.4 7.1 7.1 27.00 c0.1 1.5 4.39 18.2 19.1 7.2 7.4 7.0 7.1 27.00 c0.1 1.5 7.30 18.2 19.1 7.2 7.4 7.0 7.1 27.00 c0.1 1.5 6.9 18.2 19.2 7.2 7.4 6.9 7.1 26.00 c0.1 1.5 6.05 17.9 18.9 7.2 7.4 6.9 7.1 24.00 c0.1 1.5 6.05 17.9 18.9 7.2 7.4 6.9 7.1 19.00 c0.1 1.5 6.05 17.9 18.9 7.2 7.4 6.9 7.1 19.00 c0.1 1.5 6.0 5.03 17.5 18.2 7.2 7.4 6.9 7.1 19.00 c0.1 1.5 6.0 5.03 17.5 18.2 7.2 7.4 6.9 7.1 19.00 c0.1 1.5 6.0 5.0 1.5 6.0	щ	11	3.978		20.7	7.0	7.3	0 0	7.0	23.00	7.0.0	2.812	3.3	228	1.0
13 3.795 19.0 21.4 7.2 7.3 7.1 7.1 27.00 <0.1 14 3.960 18.3 20.2 7.3 7.4 7.1 7.3 28.00 <0.1	S	12	4.523		213	7.0	7.3	0.0	7 1	21.00	<0.1	209.5	1.6	232	0.8
14 3.960 12.5 7.3 7.4 7.1 7.1 27.00 <0.1	တ	13	3 795		21.7	2.7	5.7	1 0		27.00	<0.1	231.4	5.1	364	1.1
15 4.200 16.3 7.4 7.1 7.3 28.00 <0.1 16 5.730 18.5 19.1 7.2 7.4 7.0 7.2 20.00 <0.1	Σ	17	2 060		4.1.4	7.1	۲.3	0.7	7.1	27.00	<0.1			292	0.6
16 4.224 19.1 7.3 7.4 7.0 7.2 20.00 <0.1 16 4.736 18.7 19.6 7.2 7.4 7.0 7.1 26.00 <0.1	-	t r	3.900	20.0	20.7	7.3	7.4	7.1	7.3	28.00	<0.1			184	0.8
10 2,730 18.7 19.6 7.2 7.4 7.0 7.1 26.00 <0.1 18 4439 18.2 19.2 7.2 7.4 6.9 7.1 24.00 <0.1 19 6.055 17.9 18.9 7.2 7.3 6.9 7.1 19.00 <0.1 20 5.032 17.5 18.2 7.2 7.3 6.9 7.2 16.00 <0.1 21 4.259 17.4 18.5 7.0 7.3 6.9 7.2 16.00 <0.1 22 4.348 17.5 18.7 7.1 7.4 7.0 7.3 11.00 <0.1 24 3.874 17.2 18.6 7.4 7.5 6.9 7.0 11.00 <0.1 25 5.881 17.3 18.8 7.0 7.4 6.9 7.0 11.00 <0.1 26 4.906 17.0 18.0 7.1 7.4 6.9 7.0 11.00 <0.1 27 4.224 16.9 18.2 6.9 7.0 15.00 <0.1 28 4.646 16.8 18.1 7.1 7.4 6.9 7.0 15.00 <0.1 29 4.050 16.9 18.4 7.4 7.5 7.0 15.00 <0.1 30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3.886 16.7 17.2 7.2 7.4 7.5 7.4 7.5 7.0 7.1 7.4 7.5 7.0 7.1 30 3.968 16.7 17.2 7.2 7.4 7.5 7.5 7.4 7.5 7	W	2 4	4.222	10.5	19.1	7.3	7.4	7.0	7.2	20.00	<0.1			308	0.8
18 8.389 18.2 19.2 7.2 7.4 6.9 7.1 24.00 <0.1 18 8.389 18.0 18.9 7.2 7.4 6.9 7.1 19.00 <0.1	}	1,	5.730	18.7	19.6	7.2	7.4	7.0	7.1	26.00	<0.1	192.6	3.2	348	0.5
18 8.389 18.0 18.9 7.2 7.4 6.9 7.1 19.00 <0.1 19 6.055 17.9 18.9 7.2 7.3 6.9 7.0 17.00 <0.1 20 5.032 17.5 18.2 7.2 7.3 6.9 7.2 16.00 <0.1 21 4.259 17.4 18.5 7.0 7.3 6.7 6.9 12.50 <0.1 22 4.348 17.5 18.7 7.1 7.4 7.0 7.3 11.00 <0.1 23 3.765 17.1 19.1 7.3 7.4 6.9 7.0 11.00 <0.1 24 3.874 17.2 18.6 7.4 7.5 6.9 7.0 11.00 <0.1 25 5.881 17.3 18.8 7.0 7.4 6.9 7.0 15.00 <0.1 26 4.906 17.0 18.0 7.1 7.4 6.9 7.0 15.00 <0.1 27 4.224 16.9 18.1 7.1 7.4 6.9 7.0 15.00 <0.1 28 4.646 16.8 18.1 7.1 7.4 6.8 7.0 15.00 <0.1 29 4.050 16.9 18.4 7.4 7.5 7.0 7.0 19.50 <0.1 30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3.886 16.7 17.2 7.2 7.4 7.1	- L		4.439	18.2	19.2	7.2	7.4	6.9	7.1	24.00	<0.1	254.8	3.9	316	1.2
19 6,055 17.9 18.9 7.2 7.3 6.9 7.0 17.00 <0.1 20 5,032 17.5 18.2 7.2 7.3 6.9 7.2 16.00 <0.1 21 4,259 17.4 18.5 7.0 7.3 6.7 6.9 12.50 <0.1 22 4,348 17.5 18.7 7.1 7.4 7.0 7.3 11.00 <0.1 23 3,765 17.1 19.1 7.3 7.4 6.9 7.0 11.00 <0.1 24 3,874 17.2 18.6 7.4 7.5 6.9 7.0 15.00 <0.1 25 5,881 17.3 18.8 7.0 7.4 6.9 7.0 15.00 <0.1 26 4,906 17.0 18.0 7.1 7.4 6.9 7.0 15.00 <0.1 27 4,224 16.9 18.2 6.9 7.4 6.9 7.0 16.00 <0.1 28 4,646 16.8 18.1 7.1 7.4 6.8 7.0 15.00 <0.1 29 4,050 16.9 18.4 7.4 7.5 7.0 7.1 22.00 <0.1 30 3,968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3,886 16.7 17.2 7.2 7.4 7.1 7.1 0.00 <0.1 AVERAGE 4,565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 30 4,050 6,04 4.050	د اد	0 0	8.389	18.0	18.9	7.2	7.4	6.9	7.1	19.00	<0.1	108.6	10.7	172	i 4
20 5.032 17.5 18.2 7.2 7.3 6.9 7.2 16.00 <0.1 21 4.259 17.4 18.5 7.0 7.3 6.7 6.9 12.50 <0.1	0 0	2 6	6.055	17.9	18.9	7.2	7.3	6.9	7.0	17.00	<0.1	70.1	36	360	2.4
21 4,259 17.4 18.5 7.0 7.3 6.7 6.9 12.50 <0.1 22 4,348 17.5 18.7 7.1 7.4 7.0 7.3 11.00 <0.1	0 2	2 2	5.032	17.5	18.2	7.2	7.3	6.9	7.2	16.00	<0.1			360	- α
22 4.348 17.5 18.7 7.1 7.4 7.0 7.3 11.00 <0.1 23 3.765 17.1 19.1 7.3 7.4 6.9 7.0 11.00 <0.1	≥	7.7	4.259	17.4	18.5	7.0	7.3	6.7	6.9	12.50	\$0.4 \$0.4			200	2 0
23 3.765 17.1 19.1 7.3 7.4 6.9 7.0 11.00 <0.1 24 3.874 17.2 18.6 7.4 7.5 6.9 7.0 11.00 <0.1	-	22	4.348	17.5	18.7	7.1	7.4	7.0	73	11.00	40.3			17.	2.0
24 3.874 17.2 18.6 7.4 7.5 6.9 7.0 15.00 <0.1 25 5.881 17.3 18.8 7.0 7.4 6.9 7.0 11.00 <0.1	\$	23	3.765	17.1	19.1	7.3	7.4	6.9	7.0	1100	<0.50 J	1520	000	101	2.7
25 5.881 17.3 18.8 7.0 7.4 6.9 7.0 11.00 <0.1 26 4.906 17.0 18.0 7.1 7.4 6.9 7.0 11.00 <0.1	- -	24	3.874	17.2	18.6	7.4	7.5	6.9	7.0	15.00	5	223.0	2.0	2 878	2.7
26 4.906 17.0 18.0 7.1 7.4 6.9 7.1 16.00 <0.1 27 4.224 16.9 18.2 6.9 7.4 6.9 7.0 16.00 <0.1	_	25	5.881	17.3	18.8	7.0	7.4	6.9	7.0	11.00	\$ 0.1	150.4	010	212	7.7
2/1 4,224 16.9 18.2 6.9 7.4 6.9 7.0 16.00 <0.1 28 4,646 16.8 18.1 7.1 7.4 6.8 7.0 15.00 <0.1	S) o	26	4.906	17.0	18.0	7.1	7.4	6.9	7.1	16.00	\$0.1 1	106.6	24.7	212	2.4
28 4.646 16.8 18.1 7.1 7.4 6.8 7.0 15.00 <0.1 29 4.050 16.9 18.4 7.4 7.5 7.0 7.0 19.50 <0.1 30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3.886 16.7 17.2 7.2 7.4 7.1 7.1 0.00 <0.1 AVERAGE 4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0	n :	2/	4.224	16.9	18.2	6.9	7.4	6.9	7.0	16.00	<0.1		1	167	- i
29 4.050 16.9 18.4 7.4 7.5 7.0 7.0 19.50 <0.1 30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3.886 16.7 17.2 7.2 7.4 7.1 7.1 0.00 <0.1 AVERAGE 4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 Monthly ave, ave, min may min may min	∑ ⊦	28	4.646	16.8	18.1	7.1	7.4	6.8	7.0	15.00	0			208	2.0
30 3.968 17.2 18.1 7.4 7.5 7.0 7.1 22.00 <0.1 31 3.886 16.7 17.2 7.2 7.4 7.1 7.1 0.00 <0.1 AVERAGE 4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 Monthly ave, ave, min may min may min	- :	29	4.050	16.9	18.4		7.5	7.0	7.0	19.50	<0.1			176	0.0
31 3.886 16.7 17.2 7.2 7.4 7.1 0.00 <0.1 AVERAGE 4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 Monthly ave, ave, min max min max	≥ +	30	3.968		18.1	7.4	7.5	7.0	7.1	22.00	\$0.1	2063	27	148	0.10
4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 Monthly ave. ave. min may	-	31	3.886		17.2	7.2	7.4	7.1	7.1	0.00	<0.1	188.0	20.6	212	5 6
4.565 18.2 19.5 6.9 8.0 6.7 7.4 28.0 0.0 Monthly ave. ave. min may min may		10.00												1	2
ave, ave min max min mov		AVERAGE		18.2	19.5	6.9	8.0	6.7	7.4	28.0	0.0	176.7	8 5	247 6	1.4
THE LIE WAS THE WAY THE			Monthly	ave.	ave.	min	max	mim	max	max	max	46 7%	234.4	00 40/	52.7

COMMENTS	COMMENTS																															Trades and the second s				
ECOLI		/ 100 mi		3			3				8		33	33				3		K	8				3		3	119							4.1	10.2
DUAL	AVE mail	4VE, mg/1	7.53	45.	42.	0.95	0.98	1.16	1.52	1.11	1.55	1.56	1.52	0.83	0.60	0.73	0.51	1.45	0.95	1.08	1.52	1.15	0.80	131	1.31	1.38	1.10	0.51	1.39	1.57	1.25	1.40	1.37		1.57	
CHLORINE RESIDUAL	MAX mail	אר אישוויטים ארביוווקיו	1.45	7,40	1.18	1.10	1.13	1.31	1.80	1.26	1.64	1.58	1.80	1.31	0.72	0.81	0.95	1.85	0.98	1.10	1.75	120	1 12	148	1.52	1.57	1.23	0.99	1.57	1.98	1.51	1.61	1.92		1.98	
CHLOF	MIN ma/I	4 4 7 7	1.17	5 5	0.02	0.84	0.72	1.08	1.30	0.95	1.50	1.55	1.20	0.47	0.53	0.66	0.17	0.88	0.92	1.06	1.23	1.10	0.74	1.18	1.10	1.25	1.01	0.16	1.28	1.31	0.99	1.07	2,		0.16	
OROUS	FFF ma/I	j.	78.0	1000	60.0	0.88	0.94	0.90	96.0		0.97	0.95	0.83	0.76	0.66	0.87		1.15	0.90	0.59	0.53	0.55	0.25		0.51	0.71	0.84	1.33	0.73	0.81		1.18	1.03		0.80	30.7
PHOSPH	INF ma/I	-1	437	20.0	7.01	64.7	1.99	4.44	6.16		3.90	6.35	3.39	6.63	4.25	6.44		5.19	6.39	3.15	4.48	4.13	2.07		3.23	4.17	4.60	4.21	4.29	4.91		4.95	9.86		4.76	
	FLOW	4 022	4 104	1 321	70.7	4.200	8.144	3.945	3.469	4.107	3.524	3.678	3.978	4.523	3.795	3.960	4.222	5.730	4.439	8.389	6.055	5.032	4.259	4.348	3.765	3.874	5.881	4.906	4.224	4.646	4.050	3.968	3.886		4.565	
	DATE	-	2	(7)		t L	0	ဖ	7	80	o.	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	70401	AVERAGE	
	DAY	L	×	F	· Lu	_ (0	S)	Σ	⊢	≯	⊢	Щ	S	S	Σ	⊢	3	 -	Щ	S	S	Σ	⊢	*	-	11	တ	S	۶		>	- 			-

,-	_
TY SEWER DISTRICT #1	Apr-03
NIAGARA COUNTY SEWI	SPDES # NY-0027979

	_					-1	_				1	1	,-	1	1	1	-1	-)-			т·		, -	1	т	_	ı			Г	_	1	-	_
иļ	200	FEF ma/	ָ מ מ	0.0	2.0	1 ς 1 α	2.7	2.7	200	2.8	46	3.8	8.8	5.4	2.8	4.0	0.9	22	3.2	3.4	12	3.3	1.7	1.8	3.8	2.6	2.0	3.0	3.6	4.2	5.8	2.2	C	5.5
Verone, P.	3 0313	INF ma/I		54 24	3 2	64	4	40	40	40	36	4	40	160	40	32	72	124	36	28	12	90	44	92	176	40	40	56	98	84	108	52		03.0
FRANK A. Nerone, P.E. CERT. 4A	2	EFF.ma/I	D .	2,00	15.6	11.4	86				16.7	7.5	22.8	7.3				30.2	14.8	12.0	5.7				4.6	7.4	10.5	6.6				9.8	5	6.770
	מטמט	INF.ma/I	1	82.0	89.7	819	67.3				73.3	57.8	72.2	134.9				85.4	88.3	88.2	83.2				120.5	87.5	105.1	90.9				108.9	0 00	00.00
716-693-0001 716-693-8759 FAX	SOI INS 1HB	EFF,mI/I	, CV	500	\$0.1 \$0.1	40.1	×0.1	×0.1	\$0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	c	20.0
,- ,-	SETTSOI	H, H	0.50	1.50	1.50	1.40	0.50	0.70	1.50	0.40	0.20	0.20	0.10	14.00	0.10	0.20	0.30	11.00	0.50	0.50	0.30	2.00	12.00	3.50	8.00	1.00	1.00	3.00	1.50	1.70	4.00	1.50	14.0	75.6
N YORK	Hu	X	7.2	7.1	7.2	7.3	7.0	7.3	7.1	7.2	7.3	7.1	7.1	7.1	7.1	7.0	7.3	7.2	7.3	7.2	7.2	7.3	7.3	7.4	7.2	7.5	7.2	7.5	5.7	7.7		7.3	77	may
7348 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	Ha	Z	7.0	6.9	6.8	7.1	6.9	7.0	6.9	6.8	7.1	7.1	6.8	6.9	6.9	7.0	6.7	7.1	7.2	7.2	7.2	7.2	7.2	7.2	7.2	0.7	1.1	7.7	- 1	(.3	7:1	7.2	6.7	nin.
NIAGARA I	Hd	INF, MAX	7.3	7.3	7.3	7.3	7.2	7.1	7.1	7.5	1.4	7.4	(3	7.4	7.4	(.3	7.3	7.4	7.4	7.4	7.3	7.3	7.3	(.3	4.7	5.7	5,	4.7	5.1	۲.۵		5.7	7.5	тах
_	Hd	INF, MIN	7.2	7.0	7.0	7.2	7.0	6.9	6.7	6.8	6.3	4.7	0.0	7.7	7.3	7.7	7.1	7.2	7.3	7.2	(.2	7.2	(.1	7.7	5) 1	7.7	S. C.	7.5	5.7	7.7	1 0	5.7	6.7	min
Apr-03	ATURE,C	EFF	0	10.1	10.3	9.8	9.4	6.3	9.9	9.4	4.6	4.6	2.6	0.5	10.1	4.0.1	71.3	11.4	10.9	11.0	7.7.	13.1	13.4	6.7	14.6	5.5	12.7	127	13.7	10.2	0.0	0.	11.0	ave,
	TEMPERATURE	IN.	9.8	9.9	10.1	10.0	9.8	9.4			7.00	S. O.	0.00	000	0 0	2000	10.4	10.6	10.4	10.6	0.01	10.8			1.0	, a	o	10.1	10.2	10.6	77.0	2	10.0	ave.
r-0027979	H	FLOW	9.864	9.316	8.602	9.455	10.882	12.802	13.033	11.222	10.002	10.757	10.101	11 010	10 300	0.00	9.030	8.170	9.284	7.893	7.001	7 200	7.436	7 224	7.063	6 882	6 671	6.701	6.699	6 630	6312	71.00	9.187	Monthly
SPDES # NY-0027979 Apr-03		DATE		2	20	4 r	0 0	0 1	_ 0	οσ	5	7 -	12	1 6	2 4	τ̈́	2 4	17	7 0	0 0	2 00	24	22	23	24	25	26	27	28	29	30		AVERAGE	
		JAY	- :	≥	- -	L 0	0 0	2	<u></u> ⊢	- ≥		- 11	. V	V.	Þ	 -	- >	\$ 	- - L	_ 0.	U	> ≥	-	×	ļ.	ш	S	S	Σ	 	≥			

COMMENTS																																		
F.COLI	/ 100 ml		ю		C.	3 (7)				7	-	4	124				e.)	C	2	C	0			2		,	1400	2			2)	7.0	23.3
IDUAL	AVE,mg/I	0.40	0.88	0.95	66.0	66.0	0.89	0.93	0.63	0.03	0.40	0.60	0.42	0 29	0.18	0.42	0.37	0.80	0.73	7.0	- 0	40.0	10.0	0.00	0.28	0.46	0.40	0.34	0.28	0.24	17.0	3.0	116	2
CHLORINE RESIDUAL	MIN,mg/I MAX,mg/I AVE,mg/I	0.63	1.21	1.23	1.32	1.14	1.15	1.14	0.82	0.64	0.59	0.85	0.61	0.50	0.42	0.47	0.48	1.08	0.95	1.45	0.87	0.74	0.60	0.50	0.54	0.52	0.43	0.38	0.74	0.35	4.03	3.	1.45	
CHLO	MIN,mg/I	0.14	0.25	0.64	0.77	0.88	0.67	0.75	0.52	0.56	0.23	0.41	0.24	0.08	0.00	0.33	0.27	0.39	0.49	0.61	0.32	000	0.35	0.33	0.00	0.41	0.35	0.28	0.34	0.13	080	000	0.00	
	EFF,mg/I		0.31	0.30	0.37	0.47	0.38	0.35		0.39	0.54	0.90	0.81	0.47	0.54		0.80	0.91	0.80	0.74	0.70	0.74		0.54	0.49	0.71	0.91	0.77	0.71		0.55	3	0.59	46.2
PHOSPH	INF,mg/I		1.60	2.64	1.80	2.20	2.00	2.08		1.56	1.80	1.92	4.72	1.32	1.44		4.60	1.52	1.52	0.80	5.08	6.44		4.88	2.24	3.12	2.72	2.44	4.04		2.48		2.54	
	FLOW	9.864	9.316	8.602	9.455	10.882	12.802	. 13.033	11.222	10.862	12.452	10.757	14.922	11.919	10.309	9:636	9.170	8.284	7.993	7.631	7.409	7.389	7.436	7.321	7.063	6.882	6.671	6.701	6.699	6.630	6.312		9.187	
	DATE		2	က	4	S.	9	7	8	6	10	7	. 12	13	44	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
	DAY	-	M		_	S	S	Σ		3	<u> - </u>	<u>.</u>	S	တ ြ	Σ		X	-	ı.	S	S	Σ	-	>	ı-	4	S	S	≥	-	×			

	-				_													- 	_		-T		·	_						_	1	,	т		, ,	-1	_
щį	!	SOLIDS	EFF,mg/	0.4	3.8	3.8	2.8	2.2	3.0	3.4	3.8	4.4	2.8	2.8	2.2	4.6	5.4	4.2	28	3.4	2.0	26	3.2	4.2	2.2	4.2	8.0	5.2	3.0	5.0	6.2	3.2	3.0	2.0		3.7	277.2
Nerone, P.		S ASDS	INF,mg/I	20	72	912	4	68	52	32	44	188	160	292	124	132	112	168	192	192	232	192	316	256	192	228	260	. 184	232	264	196	260	484	120		201.5	98.2%
FRANK A. Nerone, P.E. CERT. 4A	2	ייייייייייייייייייייייייייייייייייייייי	17. mg//	12.0	8./	0.0				21.6	11.4	12.3	11.6				10.0	10.4	4.7	9.0				16.2	3.0	7.0	5.6				15.4	10.2	3.9	3.0		9.7	724.8
		ואוב שבייון	11/L 111/L	0.00	92.8	7.607				80.4	74.6		206.9				147.4	142.2	200.8	174.9				187.5	155.7	178.6	134.7			,	188.4	153.6	200.7	131.7	0	130.0	93.8%
716-693-0001 716-693-8759 FAX	oli ine 4ub	FEE mil	1 2	- 3		- 3	V0.1	<0.1	V0.1	<0.1	\$0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0.1	Q.1	<0.1	V0.1	<0.1	<0.1	0.1	<0.1	<0.1	<0.1		0.0	max
	SETT SOI	2 5	2 50	0000	7000	3.0	0.00	5.00	0.50	1.50	0.50	14.00	15.00	20.00	12.00	11.00	11.00	15.00	21.00	20.00	25.00	22.00	26.00	17.00	26.00	28.00	29.00	26.00	32.00	28.00	18.00	20.00	19.00	12.00	32.0	32.0	шах
N YORK	Hu	ΔX	7.2	7.7	5.7	7.7	t (1	5.1	5, 5	7.7	۲./	6.3	7.2	(.2	6.9	7.0	7.1	7.0	7.1	7.2	7.2	7.0	7.2	7.2	1.1	7.7	7.7	7.7	7.7	3.7	7.2	7.7	7.2	7.1	7	2 2	шах
RTY DRIVE FALLS,NE	H	Z	-	7.1	7.1	7.4	7.7	7.7	7.7	7.7	1 0	0.7	0.7	7.7	χ. Ι Ω	0.	7.1	6.9	7.0	7.1	7.7	0.7	7.1	7.7	[.]		1 0	7.7	- 1	7.1	[:]	1.7	1.1	1.1	88	i E	
7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK	Ha	INF, MAX	7.4	7.4	7.4	7.4	7.5	5.7	1.7	7.5	7.5	7.7	7.7	5.7	7.7	5.7	[.]	6.7	7.7	7.7	1.7	7.7	7.4	5.7	4.7	1.4	1.1	7.3	5.7	5.7	5.7	5.7	5.7	4./	7.5	Max	וומץ
-	Ha	Z		7.1	7.3	7.3	7.3	2.7	7.2	2. 4	0.0	0.7	0.7	0.7	10.7	7.0	- 0	α α	1.0	0.7	0.0	0.0	7.3	5.7	7.3	5.7	7.2	7.1	7.4	7.7	0.7	1.7	7.7	7:/	6.6	min	
May-03	TURE,C	EFF	11.4	11.5	10.7	11.1	10.8	111	114	α,	12.1	120	12.0	117		 	0.7	. C.	17.8	12.0	12.7	10.1	- 17 - 17 - 17	- - -	117	120	12.2	12.2	12.7	13.0	12.0	100,	120	2	12.0	ave.	
	TEMPERATURE	INI H	11.4	11.5	10.6	10.8	1			ľ			124		. [1	5 2			5 5	110	2 7	. . .	110	12.0	12.2	12.6	12.5	12.3	12.5	12.8	123	12.5	2	11.8	ave.	
Y-0027979		FLOW	8.018	9.709	8.851	7.989	7.908	10.517	8.923	7.979	7.733	7,214	8.928	9.663	10 831	9 655	8 649	9 852	11 104	9.375	8 578	8 360	11 252	9.306	8.453	9.965	10.371	8.884	8.367	8.379	7.853	7 958	8 689		9.010	Monthly	
SPDES # NY-0027979 May-03		DATE	-	2	က	4	ιĊ	မ	7	8	6	10	11	12	13	14	13	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		AVERAGE		
:		DAY	<u>-</u> ,	u.	တ	တ	∑	ı	8	 	止	S	တ	Σ	ŀ⊢	≥	 	L	S	S	Σ	 	3	 -	ட	S	S	Σ	_	Μ	⊢	L	S				

COMMENTS																																		The state of the s	
F.COLI	/ 100 ml		3600	3				Œ		560	3)				3	24	7	-			3	2	1020	3				6	0	867	8		21.4	41.0
JUAL	AVE.mg/I	0.51	0.23	0.92	0.87	0.51	0.86	0.77	0.81	0.51	0.55	0.48	0.71	0.87	0.71	0.69	0.78	0.77	0.61	180	- U	0,00	0.00	0.37	0.94	0.73	0.86	0.51	5.5	0.54	0.61	0.79		0.94	
CHLORINE RESIDUAL	MAX.mg/I	0.74	0.48	1.02	0.93	1.13	1.06	1.45	1.10	0.80	0.78	0.72	1.20	0.92	0.90	0.76	0.92	0.81	0.63	160	0.25	0.84	0.78	0.46	0.98	0.75	0.88	0.83	0.94	0.81	1.03	1.15		1.45	
CHLOR	MIN,ma/I		0.05	0.82	0.77	0.00	0.65	0.28	0.48	0.20	0.12	0.18	0.36	0.82	0.51	0.63	0.57	0.72	0.58	0.67	0.01	0.44	0.46	0.15	0.91	0.72	0.83	0.00	0.30	0.38	0.34	0.35		0.00	
OROUS	EFF,mg/I	0.96	0.67	0.39	0.51	0.62		0.68	0.81	0.93	1.09	0.91	0.71		0.52	0.52	0.44	0.58	0.43	0.52		0.83	0.83	1.01	1.29	1.00	1.06		1.24	0.91	0.72	0.34		0.77	57.7
PHOSPH	INF,mg/I	1	2.72	15.76	1.06	3.28		1.76	3.76	3.92	5.52	6.88	3.96		2.76	9.84	4.60	6.20	3.08	3.64		4.72	4.00	3.60	4.12	5.80	4.28		3.20	6.64	11.68	5.88		5.05	
	FLOW		9.709	8.851	7.989	7.908	10.517	8.923	7.979	7.733	7.214	8.928	9.663	10.831	9.655	8.649	9.852	11.104	9.375	8.578	8.369	11.252	9.306	8.453	9.965	10.371	8.884	8.367	8.379	7.853	7.958	8.689		9.010	
	DATE	-	2	က	4	2	9	7	8	රා	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	70,471,4	AVERAGE	
	DAY	;	L1.	တ	တ	Σ	-	8	F	L	S	S	≥	-	>	 -	ц.	S	S	Σ	F	Μ	F	4	ဟ	<i>σ</i>	ΣĮ	- :	8		4	တ			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

FRANK A. Nerone, P.E. CERT, 4A 716-693-8759 FAX 716-693-0001

INF,mg/I EFF,mg/ 176 4.4 SUSP SOLIDS 0 1 2.8 2.0 1.5 7. 8. 2.2 2.2 2.0 3.8 2.5 4.2 1.2 0. 20 0.4 1.3 2.0 1.2 7 Ξ 0.7 99.0% 190.4 92 144 176 176 196 196 276 276 276 276 276 192 276 192 192 192 192 160 160 284 232 200 128 212 116 140 2 49 48 INF,mg/I EFF,mg/I 280.1 3.8 3.0 18.2 3.2 3.8 3.2 3.0 3.3 3.0 4.4 CBOD 203.0 230.2 178.7 152.8 210.5 135.3 97.7% 219.0 201.2 134.0 159.9 200.8 201.8 178.7 189.1 185 SETT SOLIDS, 1HR INF,ml/I EFF,ml/I <u>^0.1</u> max 0.1 \$0.1 1 <u>~0.1</u> 0.0 0.0 <0.1 0.1 0.1 <u>^0</u> 6 9. 000 ò ô 0 0 8 0 0 0. 0. 0.7 0 ô 8 19.00 11.00 16.00 17.00 17.00 25.00 20.00 14.00 17.00 16.00 11.00 14.50 13.00 15.00 17.00 16.00 18.00 15.00 21.00 20.00 18.00 9.00 8.60 20.00 15.00 14.00 19.00 9.00 25.0 max EFF, MAX Пах Hd 7.3 7.3 EFF, MIN 7.0 H. 7.0 6.9 INF, MAX max 7.5 7.4 7.2 7.3 7.3 7.4 6.5 7.3 7.3 7.0 7.0 6.5 min. 7.1 7.1 7.0 TEMPERATURE,C 14.5 14.3 13.2 14.3 14.0 14.2 14.4 14.4 15.0 15.8 15.0 16.0 12.5 13.4 14.0 15.0 16.2 15.2 16.5 15.0 12.1 14.1 ave. 12.6 13.4 13.5 14.0 14.0 14.3 14.0 14.8 4.9 14.9 14.5 15.9 13.7 13.6 14.6 14.8 15.4 16.8 16.9 16.7 15.3 14.5 14.1 14.7 15.1 14.7 ave, 9.659 7.909 9.369 8.199 7.579 8.649 11.239 9.999 7.959 7.359 7.159 6.639 6.689 6.779 6.269 7.815 10,459 8.059 6.989 6.599 6.359 5.990 5.870 Monthly FLOW AVERAGE DATE 800 224667 0 21 $\alpha | \omega$ 4 DAY ഗ ≥ ဟ ≥ 上の ≥ ≥ Щ တ တ ≥ ≥ ш S o ≥ ≥ LL ဟ ഗ∣∑

FRANK A. NERONE

118.7

COMMENTS																																			
F.COLI	/ 100 ml				3		15	6				16	2	ľ	2 "					3		က	3				83		с.	0 0	?			43	12.0
DUAL	AVE,mg/I	0.79	0.87	0.41	0.45	0.68	0.68	0.48	0.39	090	0.55	0.72	0.75	0.64	080	02.0	0.73	70.0	0.0	0.90	0.68	0.63	0.34	0.64	0.37	0.73	0.77	0.65	0.56	030	0.00	700	45.0	0.90	
CHLORINE RESIDUAL	MAX,mg/I AVE,mg/I	1.00	0.94	0.50	1.05	0.81	0.87	0.68	0.67	0.88	0.72	0.88	0.96	0.95	0.89	0.84	5 0	2000	1 2	0.83	0.80	0.87	0.36	0.79	0.55	0.95	0.95	0.73	0.70	0.56	0.49	0 55	6.55	1.05	
CHLOF	MIN,mg/I	0.58	0.76	0.26	0.00	0.44	0.37	0.30	0.20	0.41	0.40	0.42	0.53	0.44	0.74	0.75	0.73	2 20	0.00	0.07	0.59	0.41	0.32	0.41	0.15	0.60	0.63	0.57	0.45	0.25	0.38	000	3	0.00	
OROUS	EFF,mg/I	0.43	0.39		0.56	0.44	0.34	0.38	0.37	0.36		0.43	0.49	0.41	0.40	0.42	0.53		0 57	40.0	0.33	0.69	0.82	0.89	0.84		1.09	1.11	1.04	0.89	0.94	0.94	5	0.57	37.7
PHOSPH	INF,mg/I	5.20	2.40		3.08	6.16	4.64	4.08	4.16	4.88		4.00	3.12	3.40	3.96	2.52	4.86		268	7.50	4.30	0.10	6.76	5.24	4.52		4.32	4.04	4.08	3.40	3.40	3.60		4.16	
	FLOW	12.107	9.659	8.249	7.909	9.369	8,199	7.599	7.579	10.459	8.649	8.249	8.059	11.239	9.999	8.569	7.959	7.359	7 159	080 8	0.303	0.038	6.689	6.779	6.599	6.359	6.269	6.270	5.990	5.990	5.640	5.870		7.815	
	DATE	-	2	က	4	വ	9 1	/	80	6	10	11	12	13	14	1	16	17	18	10	200	. 07	17	77	23	24	25	26	27	28	29	30		AVERAGE	
	DAY	מ	ΣĮ	-	≥		т (y)	ഗ	Σ	-	8	 -	ᄔ	S)	တ	M	⊢	M			- 0	0	מ	≥ ,	-	>		14	Ŋ	S	Σ			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

IDS	EFF,mg/I	0.3	1.0	0.8	18.4	15	19	2.6	6.2	9.2	9.0	12.0	9.8	6.8	2.4	7.2	5.6	5.6	6.8	5.6	9.6	4.8	5.2	20.0	12.2	6.4	3.2	2.0	0.8	1.9	1.1		0.0
SUSP SOLIDS	5	1	272	328	-	-	-		212			-		_				·						_			216	220	220	352	228	7 000	7.867
Ω.	EFF,mg/I	-	5.2				3.8	3.4	3.9	5.1				5.0	8.7	4.1	14.5				11.9	10.3	7.2	17.6				3.5	3.0	13.1	4.2	-	7.0
CBOD	INF,mg/I	153.9	191.7				213.6	184.2	148.8	2002				119.9	182.4	173.6	121.2				96.7	120.9	135.6	121.2				134.2	137.9	130.1	122.7	447.0	0.14.
SOLIDS,1HR	EFF,ml/I	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	\$0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0	0.0
SELL SO	INF,mI/I	30	28.0	24.0	30.0	16.0	29.0	26.0	21.0	28.0	28.0	15.0	17.0	18.0	27.0	26.0	24.0	17.0	25.0	6.0	19.0	20.0	20.0	16.0	11.0	14.0	13.0	13.0	22.0	23.0	23.0	30.0	
	ž	(.1	7.1	7.0	7.1	7.2	7.2	7.1	7.1	7.1	7.1	7.1	1.7	(.1	7.2	7.2	7.2	7.1	(.1	7.7	7.7	7.4	7.0	7.7	7.7	7.2	5.7	6.3	7.3	7.2	7.1	7.4	
nd L	EFF, WIN	0.7	0.7	0.7	7.1	7.1	7.1	7.0	6.9	7.0	0.7	1 0.7	1.0	0.7	7.1	0.7	1.7	10.8	1.0	1.0	1.7	7.2	7.0	7.0	7.7	7.7	7.1	7.7	[.]	7.1	7.1	6.9	
DII MAN	IINF, IVIAN	υ., r	U.)	1.5	9./	7.6	9./	7.5	7.6	7.5	1.4	0.7	1.1	5.7 T	C.7	U. 1	1.0	4.7	1.4	7.7	7.7	7.7	7.5	5.7	7.3	C: 7	5.7	4.7	7.3	4.7	(.5	7.6	max
INE MIN	17	1.4	1.4	4.7	7.5	7.3	6.7	4.7	7.4	7.4	1.4	4.7	5.7	7.7	7.7	0.7	1.1	7.3	7.1	7.7	7.7	7.0	S. /	7.7	1.7	7.4	7.7	0.7	7.0	7.7	7.,	6.9	min
2								. [18.3	0.00	0.00	17.5	17.4	47.4	18.7	18.7	157	14.9	ת ע	10.0 10.0 10.0	16.0	16.0	13.0	72.0	43.0	13.5	13.3	200	0.10	7,00		16.3	ave.
INF	17.1	10 T	2 2 2	20.0	70.0	10.7	70.7	7.0	16.0	180	18.4	15.7	15.8	77.6	15.6	15.2	14.9	14.4	15.1	14.7	14.8	14.4	13.4	13.5	13.6	13.9	13.8	13.3	12.7	127	1.0	15.2	ave.
FLow	3.898	4 357	3 977	3 946	707 /	7.161	E 337	100.0	4 929	5 759	6.507	4.668	4.928	5.368	5.357	5.003	7.980	9.125	6.261	5.882	5.271	9.654	13.171	9.450	8.214	7.309	5.065	6.339	6.302	6 750		6.192	Monthly
DATE	-	2	8	4	ירני	9	7	- α	0 0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
DAY	Ш	တ	S	Σ	-	X		·	(0)	တ	Σ	F	×	 -	ш	ဟ	ဟ	Σ	F	×	⊢	L	တ	တ	Σ	⊢	≯	⊢	ш	S			

C	Ų
\subset	כ
7	i >
C)
z	7
_	

OTIVEMBACO	COMMENTS																																	
FCOLL	/ 100 ml	33) m)			0)	С.	o er	5			C.)	c	۳ c	>				3		က	2700			·	0	r) (20	5.1	37.2
DUAI	AVE ma/I	2.32	121	1 20	1.26	130	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	128	1.43	2 03	0.55	0.59	0.64	1.74	2.03	1 97	173	0 08	7.00	1.51	1.73		1.15	1.00	1.05	1.77	30	00.7	787	0.20	78.0	0.04	2.32	
CHLORINE RESIDUAL	MAX.mg/I	2.75	1.67	1.54	1.66	1.70	191	1.48	1.57	2.60	0.68	0.65	1.78	1.80	3.05	2 33	1.78	1 40	7 12	00.1	1.00	1.1.1	1.43	1.09	1.62	8.	1.0.1	0.73	1.06	0.87	000	0.90	3.05	
CHLO	MIN.mg/I		0.98	0.92	0.82	1.00	135	1.00	1.18	1.41	0.46	0.50	0.06	1.63	1,44	162	1.65	0.68	1 20	1.60	20.7	00.0	0.87	0.90	0.00	00.	20.0	0.35	0.22	0.64	0.76	2	0.00	
OROUS	EFF,mg/I	1.19	1.31	1.29	1.16		1.02	1.10	1.58	1.65	0.86	0.92		0.89	1.32	1.17	1.03	0.97	0.78		70.0	0.04	7.00	0.00	0.70	0.03	0.07	0.36	0.42	0.18	0.27	11:0	0.89	43.8
PHOSPHO	INF,mg/I	7.02	7.29	5.53	5.77		4.36	6.31	25.70	4.01	6.66	5.26		5.53	4.48	3.70	3.74	5.19	3 90	1	207			4.23	ł	2 92	3.78	2.85	4.60	1.79	2.22		5.06	
	FLOW	3.898	4.357	3.977	3.946	4.727	5.213	5.334	5.022	4.929	5.759	6.507	4.668	4.928	5.368	5.357	5.003	7.980	9.125	6.261	5 882	5 271	0 657	42 474	9.171	8 214	7.309	5.065	. 6.339	6.302	6.750		6.192	
	DATE	-	2	3	4	5	9	7	∞	0	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		AVERAGE	
	DAY	ш	တ	တ	≥	⊢	≯		ഥ	တ	တ	≥	-	>	-	ட	တ	တ	Σ	F	>	-	LL	. U	S	Σ	F	M		ഥ	တ			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Dec-02

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-0001 FRANK A. Nerone, P.E. 716-693-8759 FAX CERT. 4A

EI OW	I EIVIPERA I UKE	A LUKE,C	pH INIT TATE	PH	_		SETT SO	OLIDS,1HR	CB	СВОР	SUSP SOLIDS	OLIDS
1	12.4	4.0 T	NE, MIN	INF, MAX	Z	EFF, MAX	INF,mI/I	EFF,mI/I	INF,mg/I	EFF,mg/I	INF,mg/I	EFF,mg/I
1	17.7	12.5	7.3	7.4	7.2	7.2	18.00	<0.1			164	12
- 1	13.2	12.6	7.4	7.4	7.1	7.2	24.50	<0.1			280	27
- 1	13.1	13.3	7.3	7.4	7.2	7.3	29.00	<0.1			460	12
5.440	13.0	13.2	7.2	7.5	7.1	7.2	9.00	<0.1	138.4	2.0	176	15
0.0 100 100 100 100 100 100 100 100 100	13.4	14.1	7.2	7.4	7.1	7.2	13.00	<0.1	202.1	14.0	272	13
0.00	5.0	14.5	(.3	7.4	7.2	7.5	16.00	<0.1	134.7	1.0	248	14
	13.4	14.4	7.3	7.4	7.1	7.2	24.00	<0.1	208.4	5.2	340	14
2.280	13.4	13.8	7.1	7.3	7.0	7.2	14.00	<0.1			212	12
4.010	13.4	13.5	7.2	7.4	7.0	7.3	10.00	<0.1			200	, c
4.044	13.3	13.9	7.2	7.2	7.0	7.4	16.50	<0.1			180	2 -
4.53/	13.3	14.1	7.2	7.3	7.0	7.2	20.00	<0.1	168,4	2.3	216	2 0
1.17.	13.3	14.4	7.2	7.3	7.0	7.2	16.00	<0.1	160.9	3.0	172	2 0
0.007	12.9	14.1	7.1	7.3	7.0	7.1	21.00	<0.1	172.8	6.3	256	0.0
7 0	11.9	13.3	7.1	7.5	6.9	7.3	27.00	<0.1	197.2	8.3	428	3 8
12.010	11.5	12.5	7.2	7.2	7.0	7.1	18.00	<0.1			236	9 6
11.560	11.6	12.3	7.2	7.5	7.0	7.1	13.00	<0.1			108	2.0
8.400	11./	12.0	6.9	7.4	7.1	7.2	20.00	<0.1			100	2.2
0.023).L	12.1	7.4	7.4	7.2	7.3	19.00	<0.1	224.8	7.2	168	2.4
47 020	ρ	12.3	7.4	7.5	7.3	7.4	17,00	<0.1	138.8	5.3	120	2.0
0 8	D 0	11.6	7.3	7.4	7.3	7.3	12.00	<0.1	185.4	24.0	160	3.0
007.7	10.0	10.9	7.1	7.4	7.0	7.1	10.00	<0.1	131.0	3.7	28	2.0
10.043	- 7	11.2	7.3	7.4	7.2.	7.3	14.00	<0.1	1		228	1
7 708	7.1.7	11.2	6.3	(.3	7.1	7.4	14.00	<0.1			184	12.
7.130 F.718		11.4	6.6	7.3	7.1	7.2	14.00	<0.1			188	2.0
0.40	7. L	0.1	7.7	4.7	6.9	7.5	17.00	<0.1	169.2	12.0	164	2.0
2 5	0 7	4.1	0.7	7.7	7.2	7.3	23.00	<0.1	229.1	5.0	164	0.3
7.00.1 F 86.1	7.7	5.17	0.7	7.3	6.8	7.1	14.00	<0.1	164.8	4.2	164	1.0
0.00	- 7		7.0	7.0	6.9	7.1	21.50	<0.1	157.4	8.9	140	0.3
1 40.0	o. :	12.2	7.1	7.4	6.9	7.2	13.00	<0.1			136	0.3
0 5	ρ.		7.0	7.1	6.8	7.2	11.00	<0.1			156	10
14.234	11.3	10.9	7.0	7.0	7.0	7.1	0.00	<0.1			340	18
7.968	12.2	12 B	9	7.7		1						
>	0)16	2:0	6.0	, ,	0.0	ç.)	29.0	0.0	175.4	8.4	207.9	1.6
	5	ave.	UIIII	max	E	Шах	max	max	95 2%	562 G	/00 00	1253

COMMENTS				The second secon														The state of the s			The state of the s													American Company of the Company of t	
F.COLI	/ 100 ml		-		3		3	0				60		8	o (m			C	2		0	2 6	0			33		3	m					3.0	3.0
DUAL	AVE,mg/I	0.64	0.64	0.74	0.74	0.75	0.52	0.43	0.63	0.80	0.91	0.85	0.95	1.08	1 42	133	120	0.87	0.07	78.0	20.7	1.00	9.5	0.86	0.61	0.58	0.63	0.52	0.39	0.53	0.53	0.82	70.0	1.50	
CHLORINE RESIDUAL	MAX,mg/I	0.81	0.77	0.98	0.80	0.83	09.0	0.55	1.05	0.88	1.10	1.10	1.06	1.23	1.67	141	1.25	1 23	1 12	103	22.7	1.75	105	102	0.91	0.67	0.75	0.60	0.49	0.57	0.64	1.52		1.74	
CHLOF	MIN,mg/I MAX,mg/I AVE,mg/I	0.40	0.40	0.60	0.64	09.0	0.45	0.29	0.06	0.64	0.73	0.55	0.80	0.82	1.10	1.27	1.15	0.40	0.43	0.20	1.25	0 92	0.73	0.70	0.45	0.46	0.56	0.45	0.34	0.49	0.41	0.20		90.0	
OROUS	EFF,mg/I		0.49		0.27	0.20	0.19	0.21	0.18	0.31		0.32	0.25	0.29	0.31	0.62	0.23		0.22	0.20	0.43	0.18	0.20	0.21		0.29	0.24	0.41	0.40	0.40	0.46			0.31	21.7
PHOSPHO	INF,mg/I	1.13	4.25		6.24	2.65	4.13	6.31	1.99	3.16		4.68	3.74	3.74	5.89	5.54	1.68		3.08	2.42	2.50	2.03	2.03	4.25		3.63	6.63	18.72	4.09	4.21	4.64			4.36	
	FLOW	5.690	5.734	5.030	5.228	5.014	5.095	5.199	5.280	4.616	4.844	4.537	7.211	8.687	14.592	12.610	11.560	8.400	10.823	9.327	17.238	12.786	8.643	10.780	7.798	5.418	6.348	5.901	5.861	6.341	6.188	14.234		7.968	
	DATE	-	. 2	င	4	3	9	. 7.	8	o.	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		AVERAGE	
	DAY	တ	Σ	 -	>	<u> </u>		တ	တ	≥		M	-	щ	တ	S	Σ	-	W	F	ш	တ	S	Σ	Ь	8		L-	S	S	∑	-			

NIAGARA COUNTY SEWER DISTRICT #1 SPDES # NY-0027979 Feb-03

7346 LIBERTY DRIVE NIAGARA FALLS,NEW YORK

716-693-8759 FAX CERT. 4A

SOLIDS	FEE ma/I	Sil.	0,	7.4	3.4	3.8	4.6	3.4	2.6	3.2	2.0	2.0	3.0	3.4	5.0	3.4	2.0	16	0.6	1.0	7.4	3.4	1,4	3.2	3.2	6.2	4.4	5.2	6.2	15.0		3.9	220.0
SUI IOS ASIIS	INF ma/I	7	000	144	136	216	72	92	88	80	324	352	208	120	196	236	200	340	304	368	328	260	192	184	436	48	92	48	99	9		189.6	/00 00
QO	EFF.ma/I	1/14	ř				8.3	9.5	8.0	8.1				8.6	5.1	3.4	2.8				4.8	3.0	10.3	13.8				20.2	11.9	16.2		9.7	EE7 2
CBOD	INF.ma/I		1.00.1				79.3	92.3	83.3	104.6				144.9	140.4	315.5	282.4				214.1	253.3	163.8	167.7				130.3	74.4	84.4		144.7	02 20/
SOLIDS,1HR	EFF,mI/I	AD 4	¥ 0>	,	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		0.0	70.11
SETT SOI	INF,mI/I	τÜ	rc.	0 0	0.0	10.0	3.0	4.0	2.0	4.0	21.0	33.0	12.0	4.0	8.0	14.0	20.0	22.0	20.0	25.0	19.0	16.0	13.0	9.0	31.0	0.8	0.5	1.0	0.2	0.2		33.0	Ag A
hф	EFF, MAX	7.2	7.3	7.3	7.5	7.7	7.1	7.1	7.3	7.4	7.3	7.3	7.2	7.2	7.2	7.1	7.1	7.2	7.2	7.3	7.0	7.0	7.4	7.1	7.1	7.7	7.7	7.2	7.2.	7.2	1	4.1	XECT
μd	EFF, MIN	7.0	7.1	7.1	- 1	0.7	0.7	0.7	1.7	7.7	7.2	7.7	7.7	0.7	/.1	0.7	6.9	7.0	7.1	7.0	6.9	6.8	7.1	6.8	10.0	0.0	0.0	(.)	۲.٦	0.7	0 0	0.0	Ë
Н	INF, MAX	7.2	7.3	7.4	1.7	7.7	1.0	7.5	1.0	1.0	(.5	4.7	5.7	5.7	5.7	7.7	7.7	7.2	6.3	7.3	7.1	7.0	7.4	7.7	7.7	7.7	7.7	(.0	(.3	4.7	7.6	0.1	max
Hd	INF, MIN	7.0	7.1	7.1	- α	10.0	7.0	7.0	7.7	7.7	7.7	7.1	7.7	7.0	100	0.0	0.8	1.0	0.7	0.)	6.0	6.8	6.0	0 0	2 0	0 0	7.0	1.1	- 1	0.	9 9	2.	Ē
ATURE,C	EFF	11.4	11.3	11.8	10.2	7.0	0.0	0.0	2.0	0.0	4.6	0.0	0.0	5.00	9.7	3.7	9.7	3,00	0.0	9.4	7.01	7.0.7	50.0	0.0	0 0	α	0 0	000	- u		7 6		ave.
IEMPERATURE	- N	7.11	11.4	11.2	10.4	70	α	10.7	0	10.0	10.0	10.3	10.3	10.0	10.2	10.2	5.0	10.0	10.4	10.3	10.0	10.0	100	5.00	9.6	2.6	800	0	10.0	2	10.3	0/10	α ν.α.
1	TLOW	200.0	5.126	6.599	12.625	10 688	9379	8 297	7 712	6 784	606.9	6.114	6.688	5 970	5 608	7 181	4 561	4 683	7 808	7.000	4.003	7 408	6 866	13.620	10.214	8.040	8.007	7.970	7,274		7.191	Monthly	1
חדאת	177	- 0	7	3	4	5	Θ	7	æ	O	10	7-1	12	13	14	15	16	17	78	19	20	24	22	23	24	25	26	27	28		AVERAGE		
אַעַּר	c v	0	0	≥	-	≥	-	1	S	Ø	Σ	_	≥	F	ш	S	S	Σ	-	X	 -	ш	S	S	Σ	F	M	<u> </u>	止				

STINEMANDO	COMMENTS																																	
F C011	/ 100 ml	20.11	2			•	3		C	2 6	ם					c	2)	77						6.) (r.				("	,		2	000	3.0
DUAI	AVF ma/I	8 8 9	0.00	0.78	0,.0	0.81	0.73	0.68	0.54	0.66	0.00	74	0.67	0.02	0.34	10.0	0.00	0.83	1.04	0.66	0.66	0.54	0.44	0.34	0.32	0.32	20.0	98.0	20.00	77.0	27.0	0.42	707	10.
CHLORINE RESIDUAL	MIN.mg/ MAX.mg/ AVF mg/I	0 80	5 6	25.0	0.70	1.04	0.89	0.70	0.72	0.71	0.78	0.84	0.72	0.60	0.53	0.70	2 7	0 .	1.65	0.70	0.73	0.70	0.47	0.42	0.44	0.34	0.37	0.48	080	120	23.0	00	1.65	2
CHLOF	MIN.ma/I	0.57	27.0	2 0	0.00	0.48	0.63	0.66	0.42	0.61	0.43	0.68	0.50	0.41	0.20	0.41	- 1	0.70	0.73	0.60	0.62	0.44	0.40	0.29	0.26	0.31	0.32	0.24	0.20	0.35	0.30	2	0.20	
IOROUS	EFF,mg/I	0.38	0.00	0.00	-		0.27	0.31	0.26	0.21	0.18	0.29		0.47	0.46	0.34	34	0.0 Ha	0.00	0.34		0.70	0.22	0.14	0.24	0.35	0.22		0.28	0.50	0.80		0.36	20.3
PHOSPH	INF,mg/I	6.32	3.62	3 47			1.60	1.87	1.99	2.50	5.85	12.36		2.92	4.21	4.88	7.88	7.58	7.00	7.45		6.12	6.04	3.19	1.99	12.16	1.09		0.66	1.40	1.13		4.52	
	FLOW	5.552	5.126	6.599	10 BOE	12.025	10.688	9.379	8.297	7.712	6.784	6.909	6.114	6.688	5.970	5.608	5 181	4 561		4.683	5.808	4.653	5.006	5.406	6.866	13.620	10.214	8.040	8.007	7.970	7.274		7.191	
	DATE	-	2	8		† L	n	9	7	8	6	10	11	12	13	14	15	18	1,		20	19	20	21	22	23	24	25	26	27	28		AVERAGE	
	DAY	ഗ	ഗ	Σ	 	187	\$ F	1	L	တ	တ	Σ	⊢	8	F	ш.	ഗ	S	M	N/	- :	>		ш	တ	ഗ	Σ	I	3	-	11-	,		

7346 LIBERTY DRIVE

CERT. 4A 716-693-8759 FAX 716-693-0001

760.6 INF,mg/I EFF,mg/ 18.8 14.4 8.5 8.5 7.0 5.6 8.8 12.4 3.6 5.0 SUSP SOLIDS 2.6 3.0 2.8 3.0 5.2 6.6 6.4 3.2 8.4 4.8 5.2 7.0 4,4 4.2 FRANK A. Nerone, P.E. 96.2% 185.0 132 116 88 100 100 100 80 80 80 88 2712 92 204 416 416 784 76 560 40 264 808 808 00 88 00 584 INF,mg/I EFF,mg/I 1412.5 14.5 12.6 10.0 19.6 26.4 16.2 19.1 25.2 12.4 16.6 14.6 12.2 10.7 7.7 14.1 13.7 14.4 CBOD 86.5% 160.3 107.3 112.2 107.0 167.0 163.4 188.0 110.8 124.9 137.4 106.8 96.0 85.2 96.1 91.8 66.0 81.7 SETT SOLIDS, 1HR EFF,mI/I шах 0.0 0.1 6.6 \$ 0.1 \$ 0.1 \$0.1 <0.1 0. 0. 0.1 \$ 0.1 \$ 0.1 <0.1 6. 0.7 0.1 **c**0.1 0.7 0.1 0.1 0 0 ô. 0, 0.0 ô ô. ô 000 INF,m(/ 15.00 10.00 12.00 11.00 12.00 20.00 15.00 15.00 11.00 30.00 30.0 Пах 0.20 15.00 3.50 0.50 0.50 0.40 3.50 3.00 2.00 4.50 4.00 1.50 1.00 0.50 0.20 EFF, MAX NIAGARA FALLS,NEW YORK пах 7.3 7.4 7.2 7.2 7.2 7.2 7. EFF, MIN 6.8 Ë 6.8 7.0 6.9 7.0 7.0 7.0 7.0 INF, MAX тах 7.6 7.4 INF. MIN Ë 7.4 7.2 6.8 7.3 7.2 6.7 6.7 7.1 7.1 Mar-03 TEMPERATURE,C 15.4 10.5 8.8 9.4 ave. 8.69 10.1 8.3 8.3 9. 9. 8.5 8.1 9.1 ю Э 9.6 0 0 8 7.3 7.6 8.7 9.1 10.0 10.0 10.3 9.9 9.4 9.5 8.8 8.8 9.0 9.3 ave. 10.1 10.1 9.7 9.8 9.7 9.5 9.0 7.4 8.4 9.3 9.3 9.7 SPDES # NY-0027979 8.748 9.845 10.024 22.383 23.017 29.858 20.023 20.548 6.579 20.226 12.450 12,850 8.942 8.124 14.625 11.429 17.356 13.664 12.964 10.169 10.869 6.923 7.317 9.811 20,387 10.347 Monthly FLOW AVERAGE DATE 96/2 4 က်က ∞ DAY ທ≥ ≥ ഗ ທ∣≥ ≥ ட $\omega \omega \geq$ ≥ S S ≥ ≥ Ω, ທ≥

CTIVENATOR	COMINENTS																																			
FCOL	/ 100 ml	σ	,			36	3 6		,				55		C	28	04		-		760		25	3417						ΛF	CYV	P		:		40.0
DUAI	AVE.mg/I	0.45	0.45	0.37	0.27	0.35	0.35	0.31	0.45	0.48	0.92	0.89	0.70	0.44	0.72	0.72	200	5 6	0.80	70.0	0.54	0.93	0.67	0.97	0.96	0.74	0.46	0.63	0.47	0.49	0.40	0.47	F L	0.58	0.07	16.0
CHLORINE RESIDITAL	MAX,mg/I	0.58	0.46	0.42	0.32	0.54	0.48	0.34	0.50	0.59	1.22	1.45	1.22	0.47	1 20	0.62	100	3.5	1.0.1	0.00	0.87	0.95	0.74	1.09	1.09	1.05	0.56	0.76	0.55	0.60	0.45	0.55	0.00	0.67	1 15	?
CHLOF	MIN,mg/I		0.45	0.34	0.17	0.20	0.12	0.28	0.41	0.42	0.77	0.42	0.24	0.38	0.35	0.39	0.62	20.0	0.78		0.19	0.91	0.60	0.86	0.78	0.36	0.34	0.49	0.40	0.40	0.35	0.34	0.47	74.0	0 42	1
OROUS	EFF,mg/I	0.45	0.44	0.47		0.60	0.80	0.66	0.72	0.80	0.48		0.56	0.43	0.31	0.23	0.30	0.78	2	777	74.0	0.36	0.35	0.21	0.22	0.19		0.28	0.09	0.21	0.22	0.12	0.48	2	0.39	41.8
PHOSPH	g/l	1.01	2.76	1.01		1.99	1.68	1.44	1.83	2.44	2.16		3.60	6.56	2.76	5.00	7.76	6.52	70	172	7.12	78.70	75.20	1.48	1.12	2.12		2.60	1.60	1.72	1.96	1.20	4 04	-	4.89	
	FLOW	6.923	8.942	9.017	6.579	8.748	5.910	7.317	8.124	14.625	11.429	9.811	10.869	9.845	7.316	10.024	22.383	23.017	29.858	20.023	20.02	20.040	20.307	20.226	17.356	13.664	12.450	12.964	9.337	10.347	10.169	10.628	9.515		12.850	
	DATE	-	2	e	4	5	9	7	8	O	10	-	12	13	14	. 15	16	17	18	19	20	24	- 20	77	52	75 25	200	27	77	28	29	30	31		AVERAGE	
	DAY	<i>y</i>	so :	ΣΙ	-	8	- 1	L	S	<i>လ</i> :	ΣΗ	-	8	-	-	S	တ	≥	 - 	*	 -	L	. 0	0	2	<u> </u>	- /4/	\$ -	- 1	L	တ	so :	≥			

Appendix E Phosphorus Summary (Demonstration Project Sampling Results)

DECEMBER 04 FILTER DATA

Ļ	Average	9.17	0.43	0.26	427	9.9	1.9	178.9			
	12/16	5.96	0.46	0.31	296	7.2	1.0	132.0	<3		
	12/15	1.67	0.41	<.24	140	7.2	1.4	89.1	<3		
	12/14	-	0.42		188	10.4	2.4	NO S	ET UP		
	12/13	7.5	0.40	<.24	344	10.8	2.6	NO SE	ET UP		
	12/12	19.69	0,36	<.24	856	18.0	2.3	NO SE	ET UP		
	12/11	3.97	0.52	0.30	152	10.8	1.2	126.3	. <3		
	12/10	16.21	0.44	0.25	1012	4.8	2.2	>368	<3		
						:					
	Month/Day	Influent	Filter Feed	Effluent	Influent	Filter Feed	Effluent	Influent	Effluent		
	<u>DATE</u>	P	HOSPHORU	<u>JS</u>	<u>sus</u>	PENDED SC	BOD				

For information on other NYSERDA reports, contact:

New York State Energy Research and Development Authority 17 Columbia Circle Albany, New York 12203-6399

> toll free: 1 (866) NYSERDA local: (518) 862-1090 fax: (518) 862-1091

> > info@nyserda.org www.nyserda.org

PRIMARY EFFLUENT FILTRATION

FINAL REPORT 05-08

STATE OF NEW YORK GEORGE E. PATAKI, GOVERNOR

NEW YORK STATE ENERGY RESEARCH AND DEVELOPMENT AUTHORITY VINCENT A. DEIORIO, ESQ., CHAIRMAN PETER R. SMITH, PRESIDENT

